CFD Simulations and HHF Testing of Lithium-cooled Refractory Heatsinks

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Outline

- Lithium-cooled refractories P.S. fabrication
- LM Heat transfer in closed tubes and one-sided heating – understanding conductive fluids
- CFD modeling of smooth tubes and finned devices
- HHF testing setup using LIMITS and EBTS
- Conclusions



Objectives of modeling and experiment

- Support PPI's phase-II SBIR project
- Compare smooth tubes to tubes with fin enhancements (turbulence & extended surface area)
- Effect of film boundary on convective heat transfer
- Evaluate flow parameters: ΔP , v_{in} , T_{in} , mixing
- Lithium reactions with plasma sprayed refractory walls
- Thermal cycling effects on actively cooled refractories



SBIR/STTR partners make significant contributions to PFC research.

Plasma Processes, Inc.

- Constructed of plasma sprayed Molybdenum, Tungsten, and W-Ni-Fe Alloy
 - Refractory metals plasma sprayed over graphite mandrel
 - Graphite is then chemically etched away
- Advantages
 - Simplified machining for internal fins

Complete

- Disadvantages
 - Porous walls
 - Higher impurity content
 - Fin aspect ratio limitations

VPS Formed

Internal Fin







Lithium coolant has some advantages.

advantages

- Low pressure
- High temperature
- High conductivity
- Lithium is required for tritium breeding

disadvantages

- Pure lithium is molten between 454K and 1620K
- Lithium reacts with air, H20, Cu, etc...



Only refractory heatsinks can operate at very high temperatures and are compatible with liquid lithium coolant.

- Mo, W and W-Ni-Fe plasma sprayed heatsinks (Plasma Processes, Inc. – phase-II SBIR)
- Smooth tubes and helical fins (pitch: 1 rev/7.4 cm)
- Applications: FW/blanket smooth



Description	of Spray	Formed	Refractory	Metal	Heat Sinks
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ID Number	Material	Bore Configuration	Bore Major ID	Bore Minor ID	Number of Fins
V2000-20	W-Ni-Fe	Smooth	~12.7mm	N/A	N/A
V2000-23B	W-Ni-Fe	Finned	9mm	7mm	8
V2000-3C	Molybdenum	Smooth	~12.7mm	N/A	N/A
V2000-24	Molybdenum	Finned	9mm	7mm	8
V2002-12D	Tungsten	Finned	9mm	6.7mm	8



finned

Computational Fluid Dynamics Finite Volume Modeling Process

- Plan geometry with x,y,z symmetry
- Construct regions (manual CAD-type labor)
- Mesh regions into finite volumes (optimize)
- Add boundary conditions (walls, inlets, etc)
- Specify initial conditions & solution parameters
- Execute STORM solver (seek steady state)
 - Conservation of mass, momentum, energy
- Graphically interpret results with FIELDVIEW



Analysis uses temperature dependent properties for heatsink and coolant (user coding)

 $\frac{d\rho H/dt + d(\rho u_i H)/dx_i}{C} = \frac{d/dx_i [k/C_p dH/dx_i] + dp/dt + u_i dp/dx_i + \Phi + Q}{Lithium kth} + Q$



Axial Finned Model







- Thermal conductivity of lithium and molybdenum is not significantly different.
 - Molybdenum: 106 [w/(m*K)]
 - Lithium: 43
- Boundary layer disruption does not significantly affect overall heat transfer for lithium cooling.
- Further modeling will be needed to determine if the conductive effects of thick walls help transfer heat to the bottom of the lithium column.



Approach to Steady State Conduction 3D View, 5 MW/m2, 0.1 m/s, Axial Finned Laminar





Effect of Film not as important for LM as water.



FIG. 9-3. Martinelli's solutions for the temperature gradients in pipe flow.

- Our helical fin R_e ranges from 821 to 82150 (0.1 to 10 m/s)
- Pr = .0047 @ 200 C
- Convection contribution is same order of magnitude as conduction: Bi~Nu<10, Pr<.01
- For water, convection is more than 2 orders higher, Bi>10, Nu~1000s, Pr~.34 (x100)

$$R_{e} = D_{e} V \rho / \mu$$

$$Pr = C_{p} \mu / k$$

$$Bi = hL_{c} / k_{s}$$

$$Nu = hL_{c} / k_{f}$$



Axial fins of this geometry decrease heat transfer!



•With constant inlet velocity, less lithium flows through finned model due to the volume of the fins.



Laminar conditions are easy to model.





Transient is controlled by conduction in the wall.





Helical Finned Model





5 MW/m² heating to s.s. with 0.1 m/s flow.





Finned refractories have negative impact on heat transfer compared to smooth tubes.





Code has heatflux problem on elements with coplanar sides. Only affects surface elements in helical model at j,k boundary.





Temperature gradient is only in outer 2 mm of lithium at 4 m/s.





Lithium temperature is highest in low velocity grooves, with little mixing even at the exit.

exit temperatures 4 m/s







core velocity 4 m/s





Highly turbulent flows are difficult to initiate.





Fins significantly increase pressure drop.



Experimental Setup (Top View): LIquid Metal Integration Test System (LIMITS)





Refractories are instrumented with 4 type-K thermocouples.





Coolant Channel Mounted in LIMITS Vacuum Chamber





LIMITS at SNL's Plasma Materials Test Facility

Test support: J. McDonald, T. Lutz, K. Troncosa, F. Bauer





Conclusions

- Enhancing convection through the fin-effect is not beneficial for liquid metals compared to water in this example.
- Better heat transfer at higher velocities is too costly in pressure drop.
- High temperature, low pressure lithium applications using refractories require thin-walled, smooth tubing (or thin face plates on the heat flux side).
- Cracking in thin-walled refractories will be a problem.
- LIMITS will provide experimental data to benchmark CFD calculations
- Fins in refractory metals is a good demonstration of plasma spray fabrication; however, it may be more useful for helium than LM.
- Closer coordination between PFC institutions and SBIR/STTR companies can identify design issues early in a project. PFCs require a comprehensive treatment of materials, fabrication, heat transfer and PMI issues.

