

# MHD Modeling of CHI on NSTX

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# Overview

- Grad-Shafranov equilibrium modeling.
  - Grad-Shafranov model has flows!
  - Helicity and energy balance.
- Resistive steady state.
  - Unlike high- $S$  Ohmic discharges, resistive steady state gives significantly different answer from Grad-Shafranov equilibrium modeling.
  - Reason: plasma flow scales with externally imposed voltage, not parallel resistivity.
  - Consequence: plasma inertia and viscous forces induce  $\mathbf{j}_{\perp}$ . Small  $\mathbf{j}_{\perp}$  brings strong poloidal localization of large parallel current on a flux surface.
- Transient CHI for secondary current drive.
  - 2D forced reconnection.
  - Ramp down of 3D nonlinearly saturated state.

## Open field line Grad-Shafranov Equi.

- Magnetic coordinates for open field lines,

$$\mathbf{B} = \nabla\psi \times \nabla\theta + \nabla\varphi \times \nabla\chi(\psi, t) = G(\chi)\nabla\varphi + \nabla\varphi \times \nabla\chi.$$

At electrode surfaces,  $\mathbf{B} \cdot \mathbf{n} > 0, \theta = 0$ ;  $\mathbf{B} \cdot \mathbf{n} < 0, \theta = 2\pi$ .

- Grad-Shafranov equation is closed by specifying the parallel current from resistive Ohm's law,

$$\frac{dG}{d\psi} = \frac{\mathcal{V}(\psi)}{q(\psi)\mathcal{R}(\psi)}; \quad \mathcal{R}(\psi) \equiv \int_0^{2\pi} \frac{\eta B^2}{\mathbf{B} \cdot \nabla\varphi} d\theta$$

- Helicity and energy balance ( $\nabla p = 0$ )

$$\begin{aligned} \mathcal{V}(\psi) &= -4\pi^2 q(\psi) \eta_{||} (G + \iota I) k_n; \\ \mathcal{V}(\psi) \frac{dG}{d\psi} &= 4\pi^2 \eta_{||} (G + \iota I) k_n^2. \end{aligned}$$

Net parallel current  $k_n = -dG/d\chi$ .

$G$  and  $I$  are poloidal and toroidal plasma current.

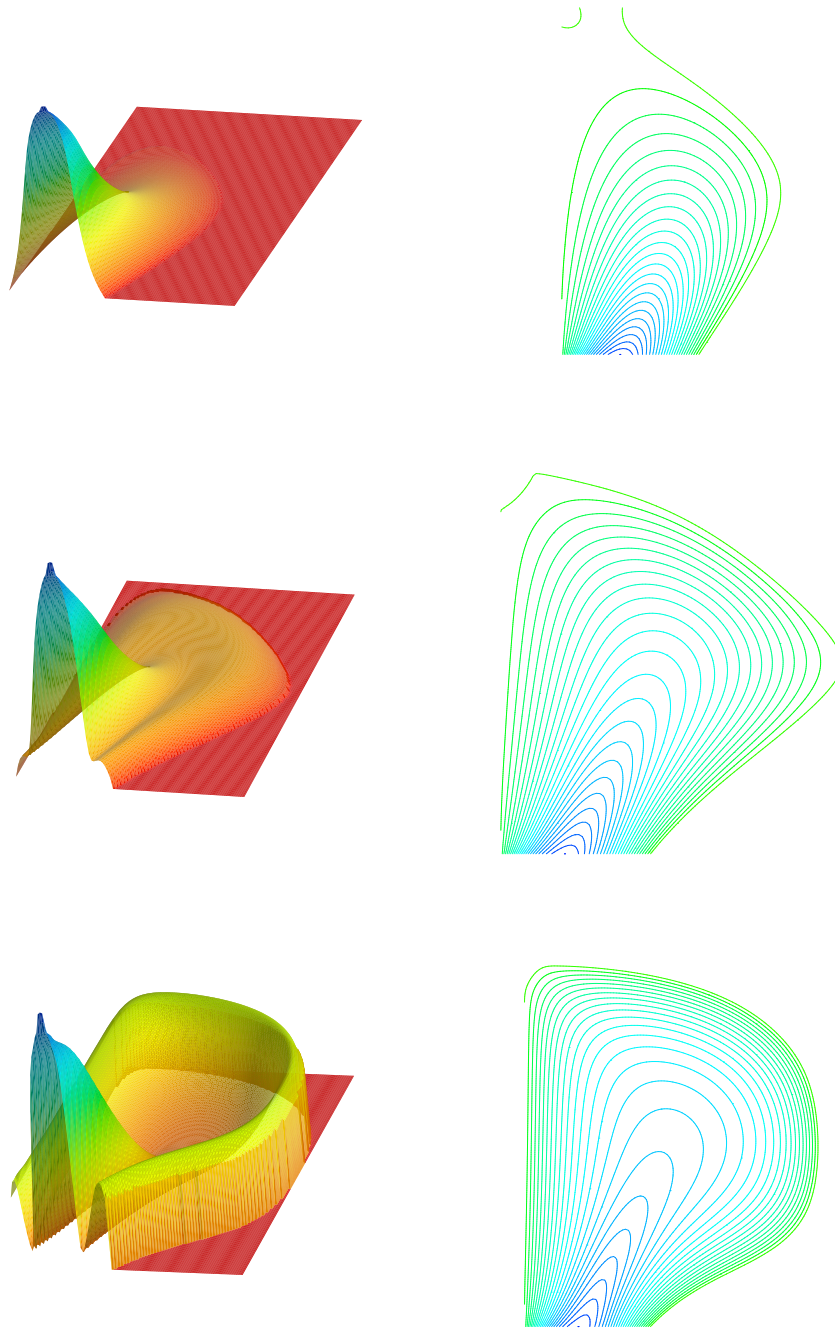


Figure 1: Surface plot of  $RJ_\varphi$  and contour plot of  $\psi$  (top  $\mathcal{V} = -1$ ; middle  $\mathcal{V} = -2$ ; bottom  $\mathcal{V} = -4$ .)

## Interpretation and reconstruction

- Quasi-neutral modification of  $\Phi$  is included in G-S model,

$$\Phi(\chi, \theta) = \mathcal{V}(\chi) \frac{\int_0^\theta \frac{\eta B^2}{\mathbf{B} \cdot \nabla \varphi} d\theta}{\int_0^{2\pi} \frac{\eta B^2}{\mathbf{B} \cdot \nabla \varphi} d\theta}.$$

In MHD, that implies a self-consistent  $\mathbf{B} \times \nabla \Phi$  flow.

- In Ohmic discharges,  
high  $T_e \rightarrow$  large  $S \rightarrow$  small  $\mathcal{M}_g$ .
- In CHI discharges,  
 $\mathbf{v} = \mathbf{B} \times \nabla \Phi / B^2$  independent of  $S$ , vanishing  $\rho \rightarrow$  small  $\mathcal{M}_g$ .
- Due to the operational density limit in CHI, G-S model is a fragile limit for CHI.
- Reconstruction from experiments: EFIT, MFIT, ESC, TSC.

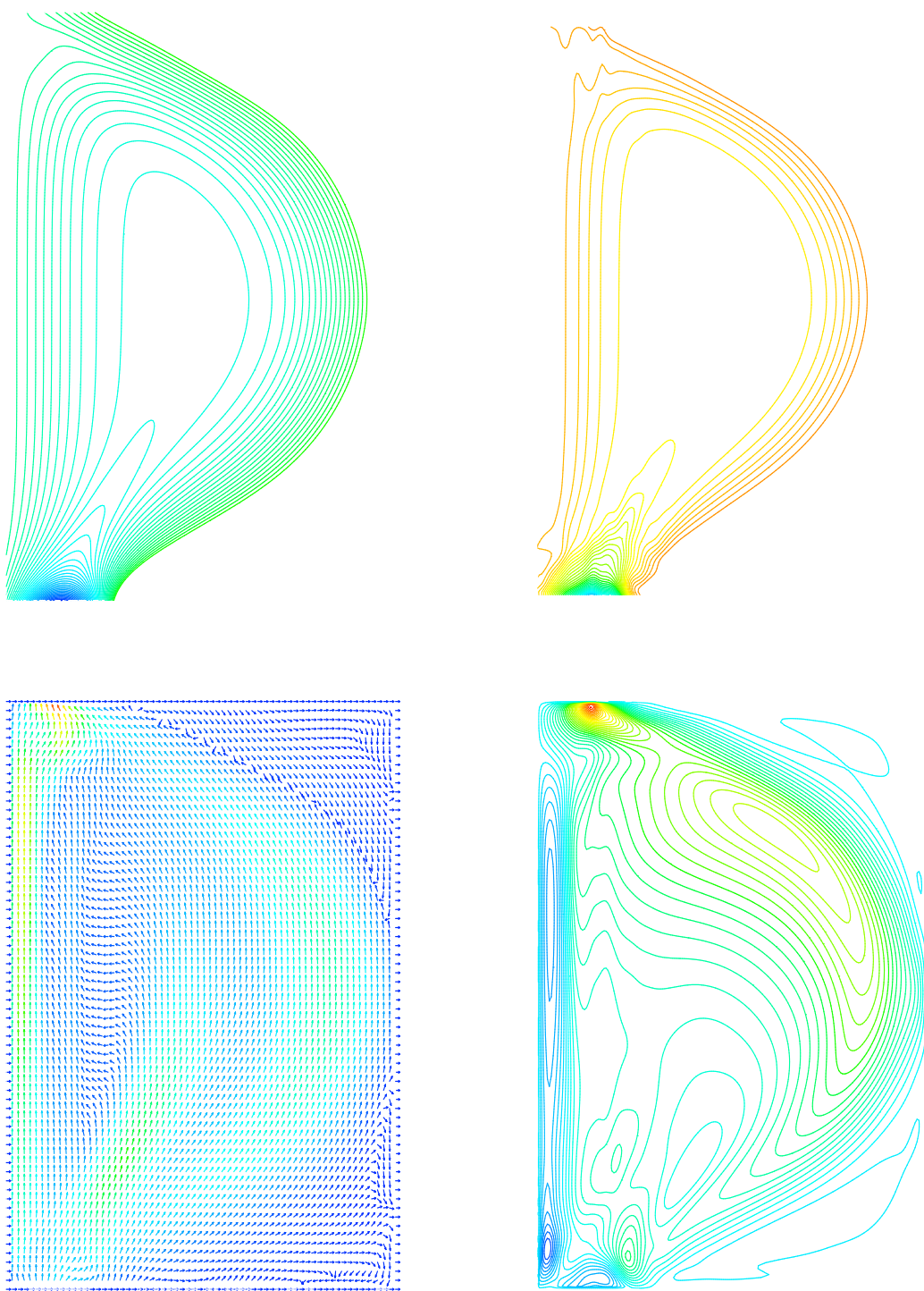


Figure 2: Top left: poloidal flux  $\psi$ ; top right:  $RB_\phi$ ;  
Bottom left: poloidal flow; Bottom right:  $v_\phi$ .

## Resistive Steady State: $\mathbf{j}_\perp$

- $\mathbf{j}_\perp$  is required for force balance with plasma inertia and viscous force,

$$\mathbf{j} \times \mathbf{B} = \mathbf{F}; \quad \mathbf{F} = \rho \mathbf{v} \cdot \nabla \mathbf{v} - \rho \nu \nabla^2 \mathbf{v}.$$

- Largest  $\mathbf{j}_\perp$  occurs around the absorber and injector with electrode gap  $d$ ,

$$j_\perp \sim \mathcal{M}_g^2 B/d, \quad \mathcal{M}_g \equiv \frac{v_{\mathbf{E} \times \mathbf{B}}}{v_A} = g \frac{\rho^{1/2} \mathcal{V}}{dB^2}.$$

Magnetic Mach number  $\mathcal{M}_g$  depends on a geometric factor  $g \sim 1 - \mathbf{E} \cdot \mathbf{B}/EB$ .

- At the injector, poloidal field is designed to be maximumly aligned with  $\mathbf{E}$  for high efficiency in driving the parallel current ( $g \rightarrow 0$ ). Opposite is true at the absorber ( $g \rightarrow 1$ ).

## Resistive Steady State: $j_{\parallel}$

- Parallel current is the one affected most by flows,

$$k_{\parallel} \equiv \mathbf{j} \cdot \mathbf{B} / jB = k_n(\psi) + k_{ps}(\psi, \theta) + k_{\alpha\psi}(\psi, \theta).$$

- Net parallel current  $k_n(\psi)$  is not affected by  $\mathbf{j}_{\perp}$  or

$$\mathbf{F} = F_{\psi}(\psi, \theta)\nabla\psi + F_{\alpha}(\psi, \theta)\nabla\alpha.$$

Clebsch coordinates  $\alpha \equiv \theta - \iota\varphi, \xi \equiv \theta + \iota\varphi$ .

- Pfirsch-Schlüter current is driven by  $F_{\psi}$ ,

$$k_{ps} = \frac{2g_{\alpha\xi}}{qJ_m B^2} F_{\psi} - \frac{qJ_m}{2} F_{\psi}.$$

- $k_{\alpha\psi}$  current is driven by  $F_{\alpha}$ ,

$$k_{\alpha\psi} = -\frac{2g_{\psi\xi}}{qJ_m B^2} F_{\alpha} + \int_0^{\theta} \frac{\partial}{\partial\psi} (qJ_m F_{\alpha}) d\theta'.$$



## Small $k_{\perp} \rightarrow$ large $k_{\parallel}$

- Normalized perpendicular current and magnetic field

$$k_{\perp}^{\alpha} \equiv \frac{\mathbf{j}_{\perp} \cdot \nabla \alpha}{\sqrt{g^{\alpha\alpha}} B} = \frac{F_{\psi}}{\sqrt{g^{\alpha\alpha}} B} \quad ; \quad k_{\perp}^{\psi} \equiv \frac{\mathbf{j}_{\perp} \cdot \nabla \psi}{\sqrt{g^{\psi\psi}} B} = -\frac{F_{\alpha}}{\sqrt{g^{\psi\psi}} B}.$$

$$b_{\alpha} = \mathbf{B} \cdot \frac{\partial \mathbf{x}}{\partial \alpha} / B \sqrt{g_{\alpha\alpha}} \quad ; \quad b_{\psi} = \mathbf{B} \cdot \frac{\partial \mathbf{x}}{\partial \psi} / B \sqrt{g_{\psi\psi}}.$$

- Pfirsch-Schlüter current  $\sim q^2 k_{\perp}^{\alpha}$

$$k_{ps} = b_{\alpha} \sqrt{g_{\alpha\alpha} g^{\alpha\alpha}} k_{\perp}^{\alpha} - \frac{1}{2} q J_m \sqrt{g^{\alpha\alpha}} B k_{\perp}^{\alpha}$$

- $k_{\alpha\psi}$  current  $\sim \frac{\partial}{\partial \psi} (q J_m B \sqrt{g^{\psi\psi}}) k_{\perp}^{\psi}$ .

$$k_{\alpha\psi} = b_{\psi} \sqrt{g_{\psi\psi} g^{\psi\psi}} k_{\perp}^{\psi} - \int_0^{\theta} \frac{\partial}{\partial \psi} (q J_m \sqrt{g^{\psi\psi}} B k_{\perp}^{\psi}) d\theta'$$

- Strong parallel current is localized poloidally around injector where local  $B_{\theta}$  is small on a high  $q$  field line, and around absorber where local  $B_{\theta}$  is strong on a high  $q$  field line near the X point.

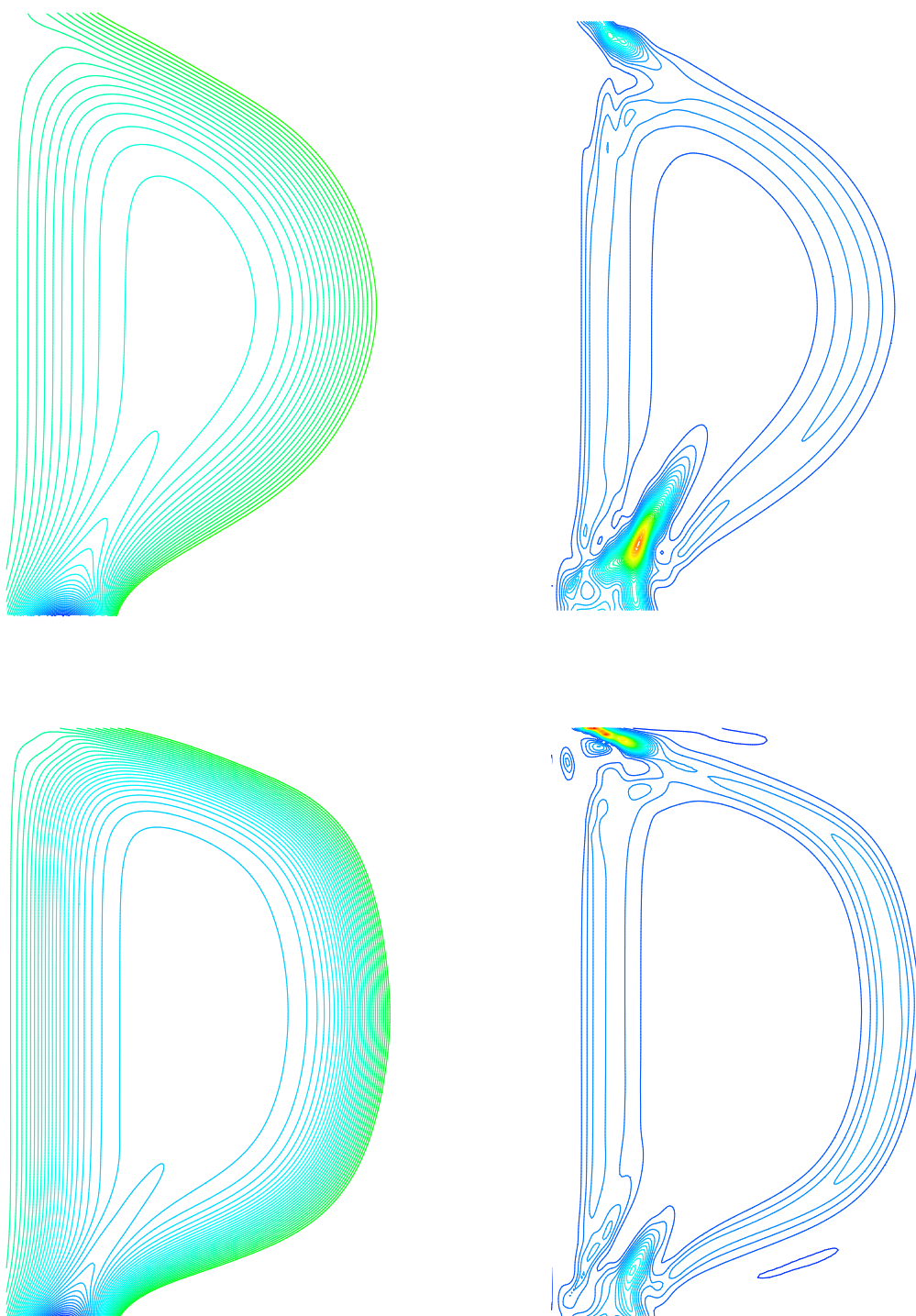


Figure 3: Left: poloidal flux  $\psi$ ; right:  $k_{\parallel}$ . Bottom run has twice the voltage as the top run. In both cases,  $k_{\parallel} \gg k_{\perp}$ .

## Transient CHI for secondary current drive

- Non-inductive startup is attractive for NSTX and future ST devices.
- CHI prepares the initial plasma and field. Secondary current drive provides profile control and sustainment.
- Secondary current drive (Ohmic, beam, rf wave) all require a plasma core with adequate confinement (closed flux surfaces).
- Steady state CHI plasma with good core confinement remains an issue of debate, but transient CHI plasma can easily satisfy the requirement.

## 2D or 3D?

- Transient axisymmetric CHI plasma: forced 2D reconnection to form large volume of axisymmetric plasmoid.
  - pinching off the injector flux or modulating the voltage.
  - downside:  $q$  profile is opposite of eventual ST profile, more work for secondary drive.
- Transient 3D CHI plasma: ramp-down a nonlinearly saturated high- $\nu$  3D plasma.
  - saturated  $n = 0$  component has substantial current penetration into the core.
  - fast decay of  $n > 0$  modes leaves  $n = 0$  with ST-like  $q$  profile.
  - room for  $q$  profile optimization during the CHI phase.

# Comparison numerical experiments

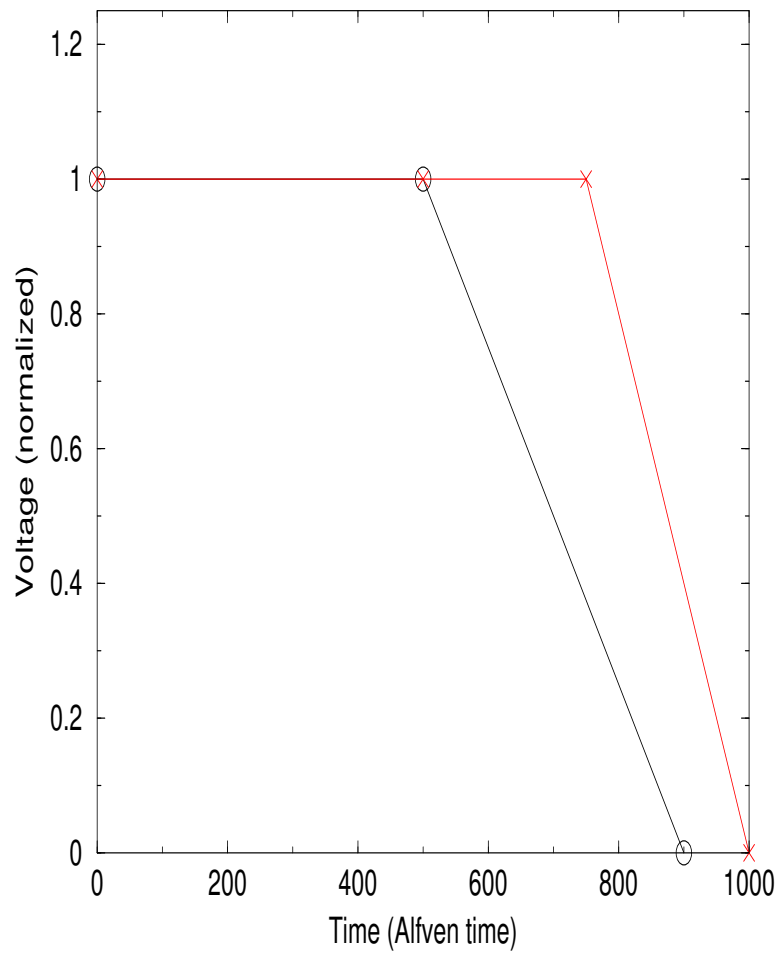


Figure 4: Two sequence of MHD calculations

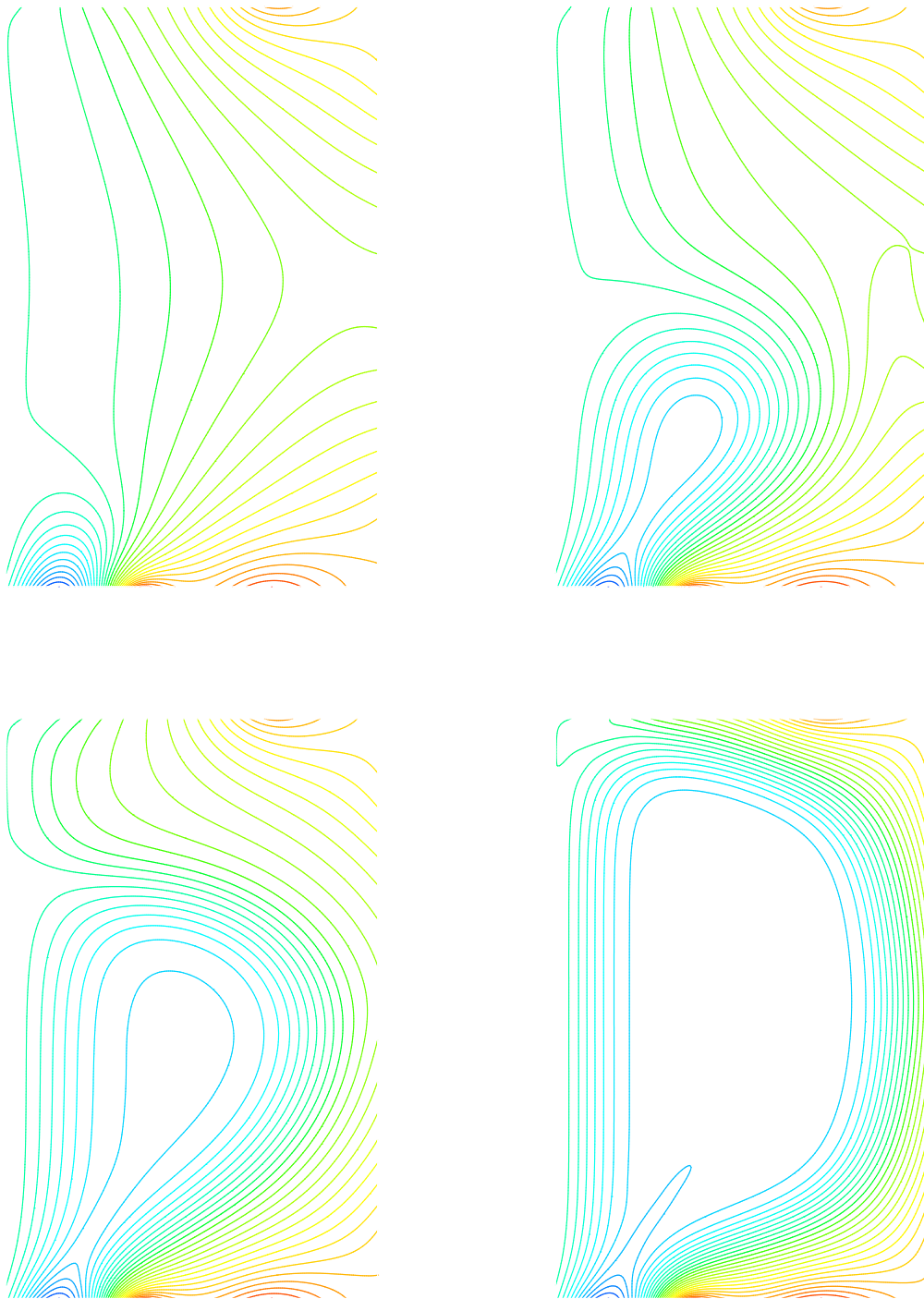


Figure 5: Axisymmetric ramp up to resistive steady state: poloidal Flux  $\chi$  over time.

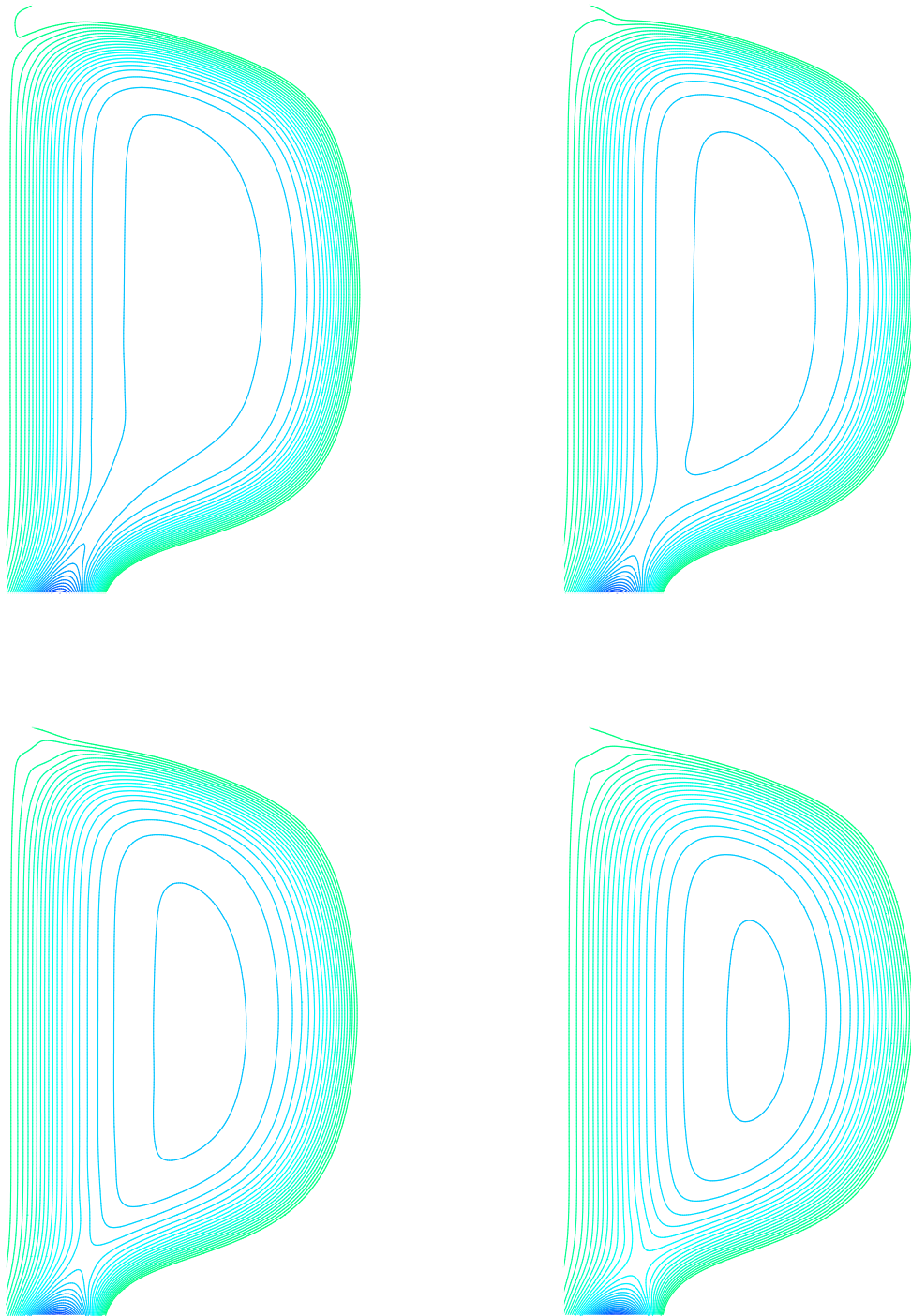


Figure 6: Axisymmetric ramp down: poloidal Flux  $\chi$  over time. (forced 2D reconnection by voltage modulation)

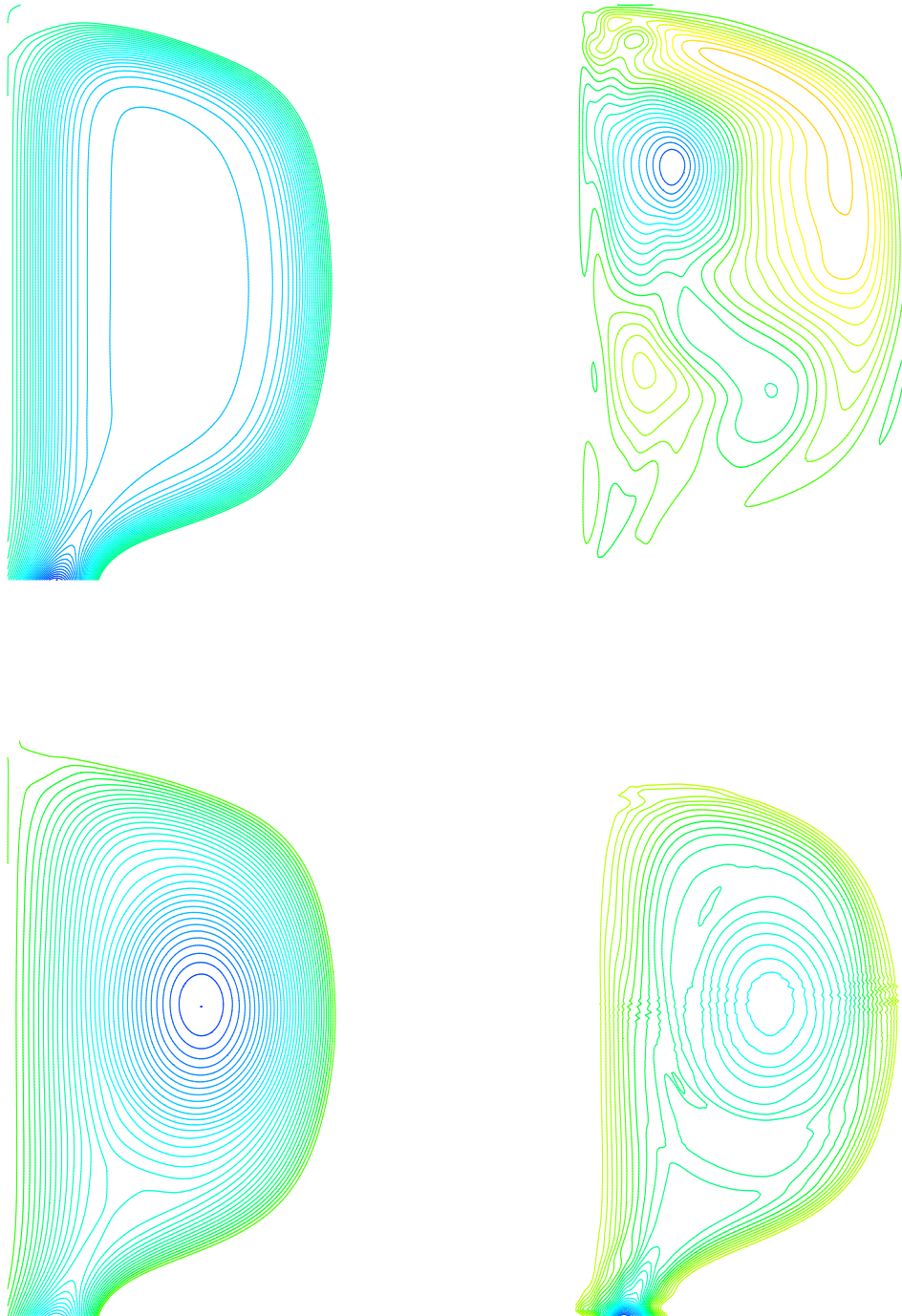


Figure 7: Kink instability and its nonlinear saturation<sub>15</sub>



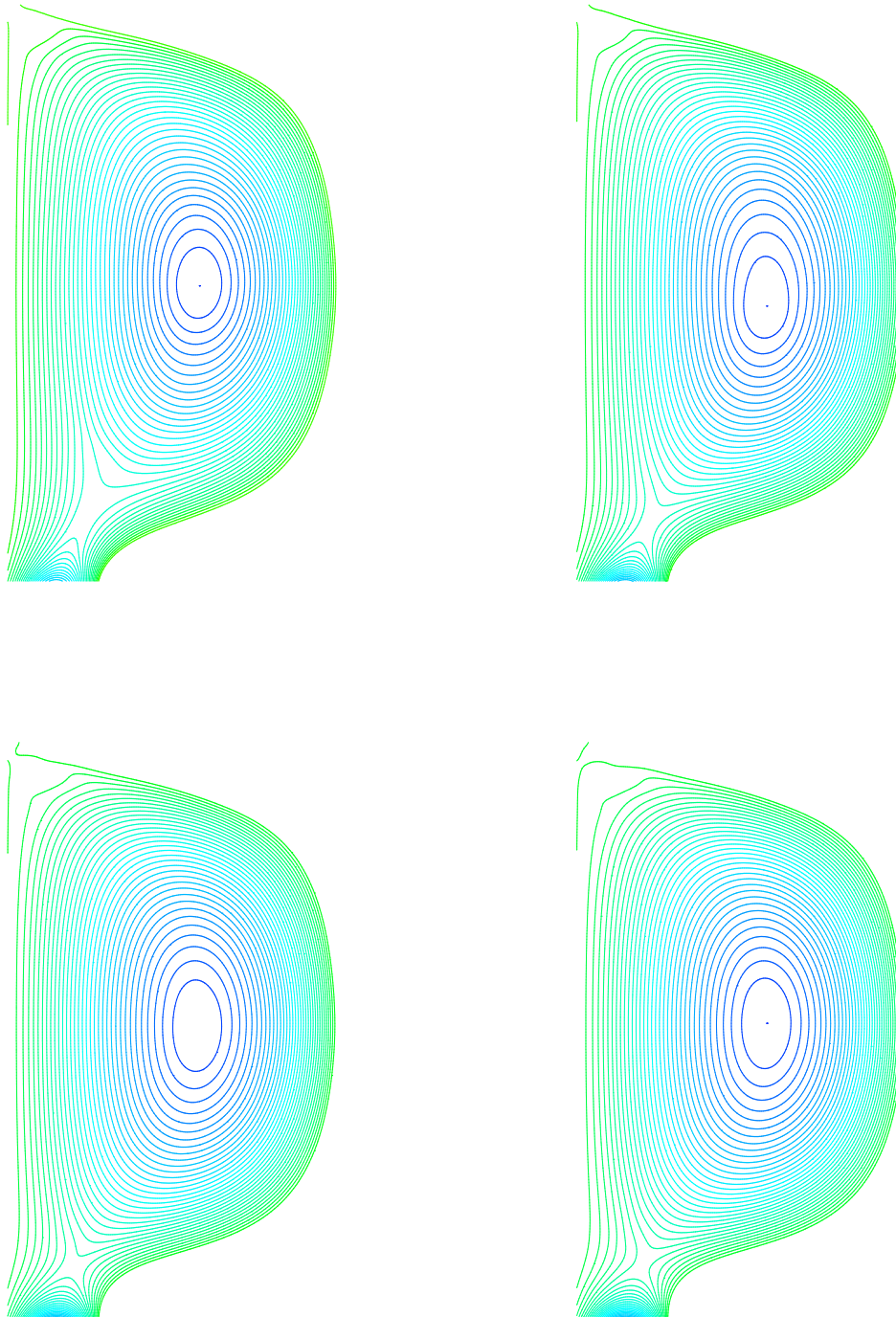


Figure 8: Ramp down of the nonlinearly saturated state

## Freely decaying CHI plasma

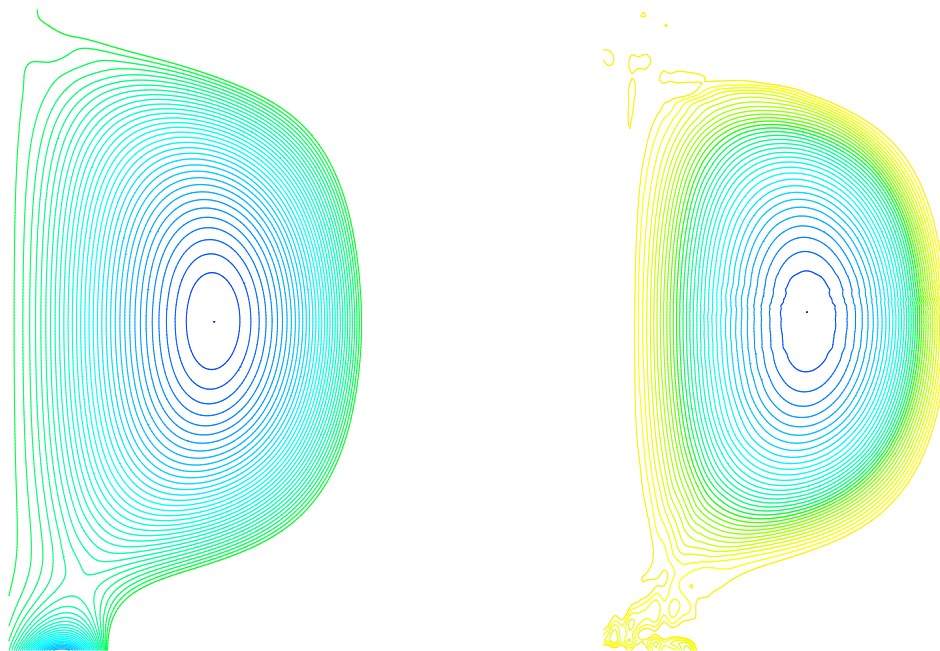


Figure 9: Freely decay CHI plasma (vanishing voltage),  $n=0$   $\chi$  (left) and  $RB_\varphi$  (right).

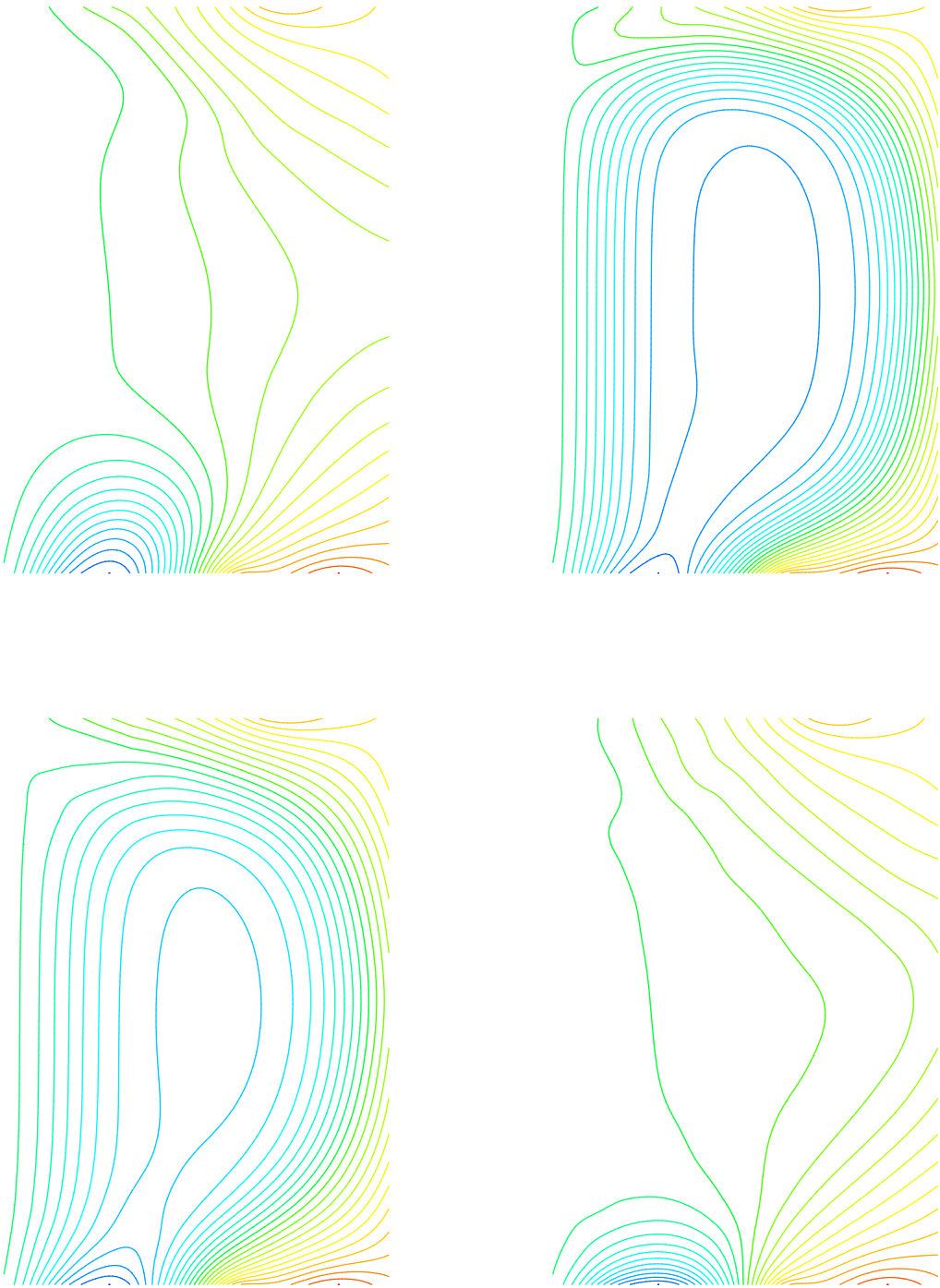


Figure 10: Ramp down could cause discharge termination. Freedom in PF shaping flux design. Top: Ramp-up; Down: Ramp-down