



Electron density gradients from linear D_{α} camera

M. R. Tournianski, P. G. Carolan, E. R. Arends, G. F. Counsell

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**EURATOM - UKAEA Fusion Association
Culham Science Centre
Abingdon, Oxfordshire, OX14 3DB, UK**

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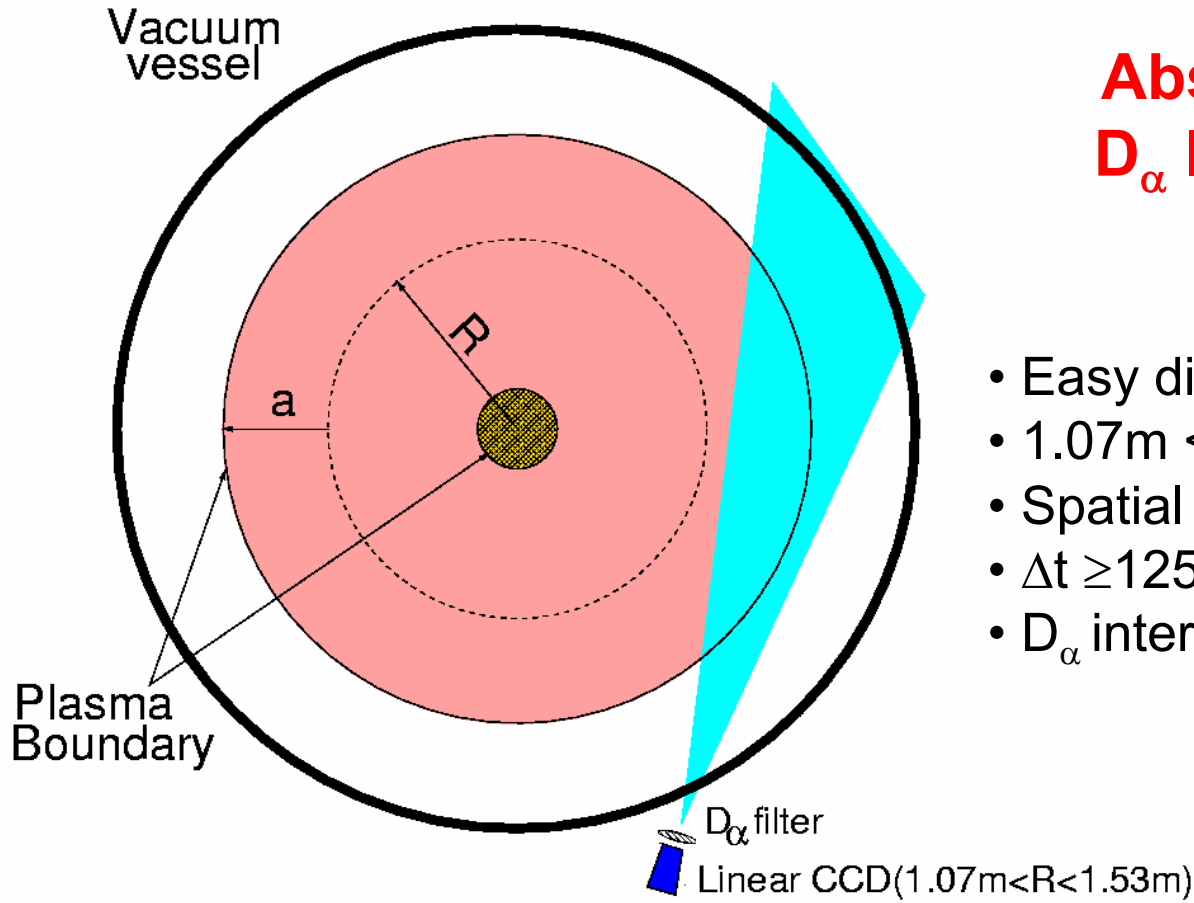
Contents

- Instrumentation
- Motivation
- Analytic model and computer simulation
- Experimental results
- Conclusions

Instrumentation

Absolutely calibrated D_{α} linear CCD camera (256 elements):

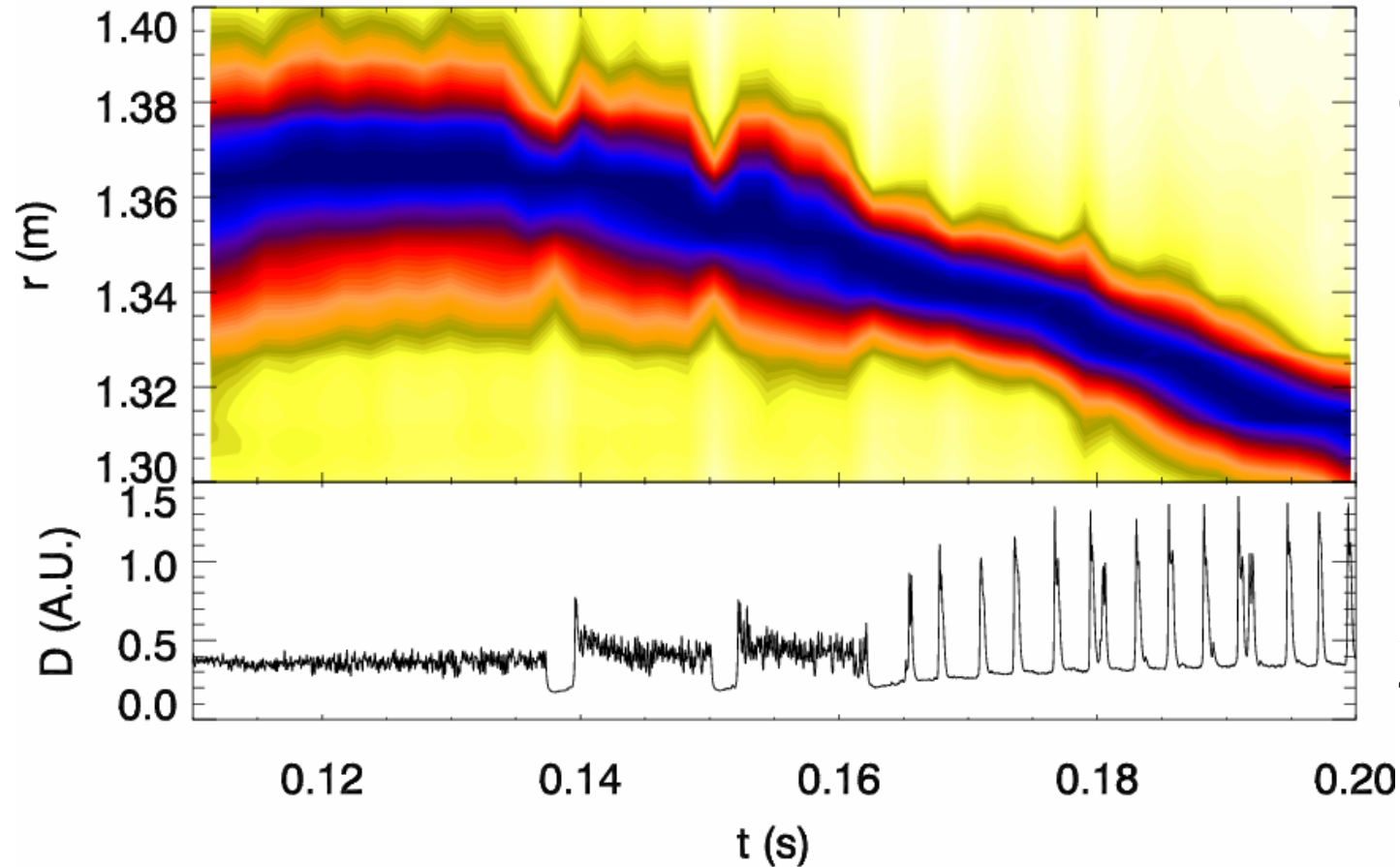
- Easy diagnostic access
- $1.07\text{m} < R < 1.53\text{m}$ (Outboard)
- Spatial resolution $\Delta R \sim 2\text{mm}$
- $\Delta t \geq 125\mu\text{s}$ (read out speed)
- D_{α} interference filter





Experimental observations

MAST #4168

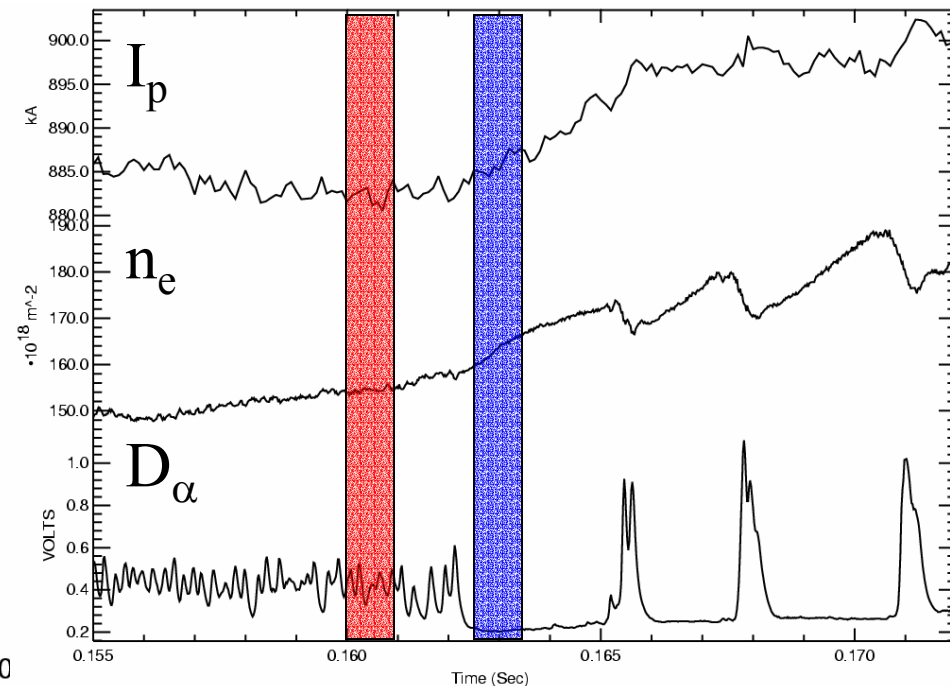
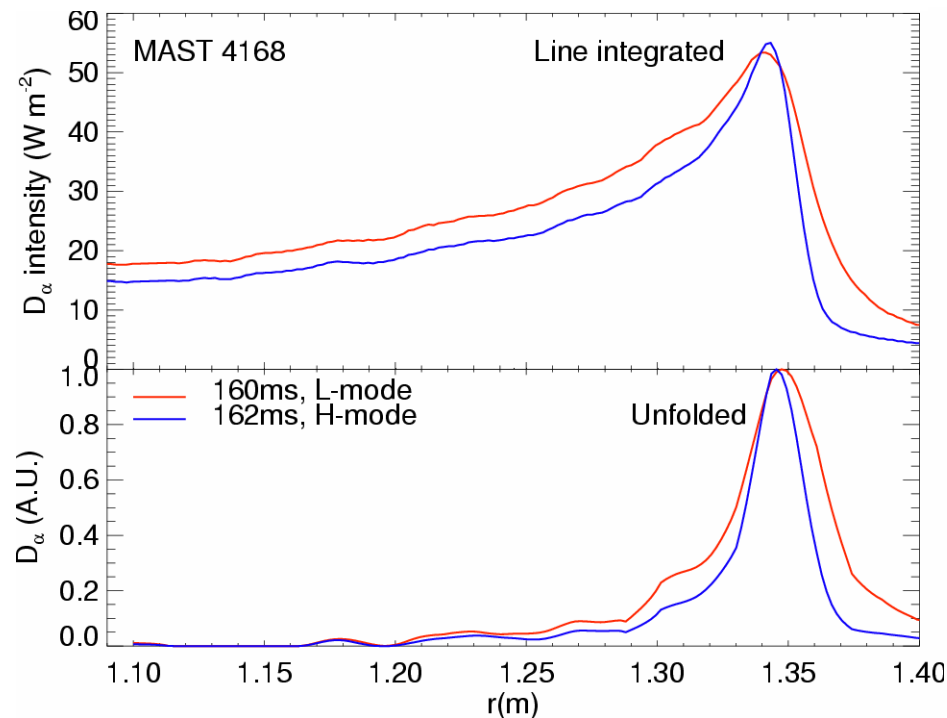


Contour graph
of unfolded D_{α} emission
(MAST #4168, 656nm)

Neutral density extraction
using TS on START/MAST
M. R. Tournianski et al.,
Nuclear Fusion
41(1) 77-89 (2001)

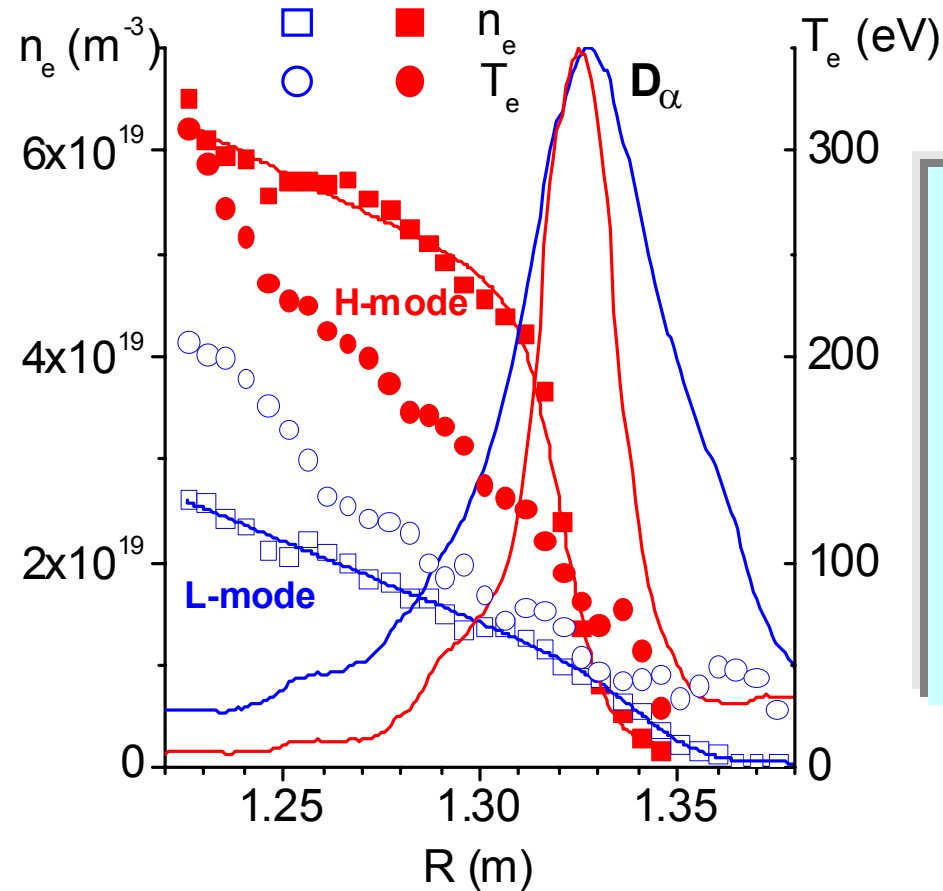
Unfolding the line-of-sight integrated intensities

- Assume toroidal symmetry
- “Singular Value Decomposition”
- Radial smearing/finite CCD element size included



D_α emissivity narrows during L-H transition

D_α narrowing



- n_e profile accounts for D_α narrowing
- $T_e > 30\text{eV}$ in D_α range
- D_α peak at transport barrier
- Modified TANH least square fit position



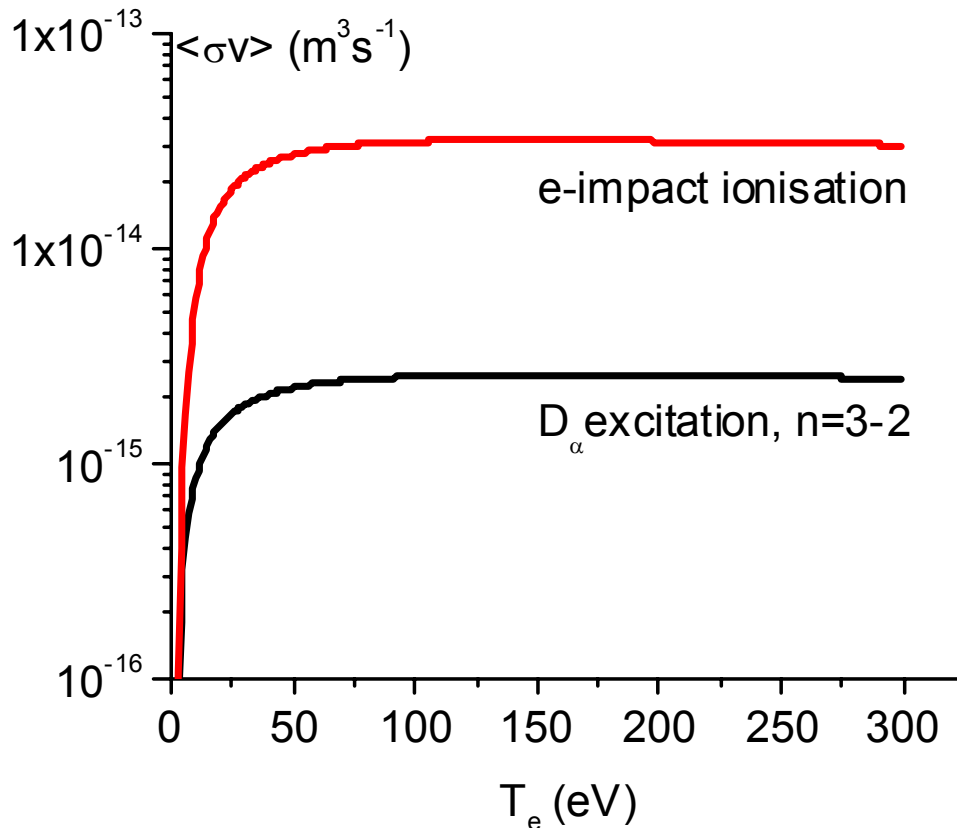
Motivation

Edge electron density profiles are important for H-mode studies

- To exploit physics of Hydrogen excitation
- Simple method to monitor edge density
- Limited TS time repetition rate
- Qualitative technique , 300 point TS system as yardstick
- Naturally limited in D_{α} range (transport barrier position)

Analytic model to understand main trends

Atomic physics helps !!!



$$D_{\alpha} = n_e n_o \langle \sigma v \rangle_{ex}$$

- $T_e > 40\text{eV}$ in D_{α} range in MAST/START (probes)
- $\langle \sigma v \rangle_{ex,ion}$ varies $\sim 15\%$,
 $T_e = 30\text{eV} - 300\text{eV}$ ($T_e > 13.6\text{eV}$)
- D_{α} narrowing due to T_e is much less important



Simple model for D_α emissivity (analytical)

$$D_\alpha = n_e n_o \langle \sigma v \rangle_{ex}$$

- Linear approximation for n_e
- $\langle \sigma v \rangle_{ion} \sim \text{const}$, $T_e > 40\text{eV}$

$$\left. \begin{array}{l} n_e = \frac{dn_e}{dr} \cdot r \\ \langle \sigma v \rangle_{ion} \sim \text{const} \end{array} \right\} n_o - ?$$

Basic n_o from particle continuity

$$\frac{\partial n_o}{\partial t} + \vec{\nabla} \cdot \vec{\Gamma}_0 = -S$$

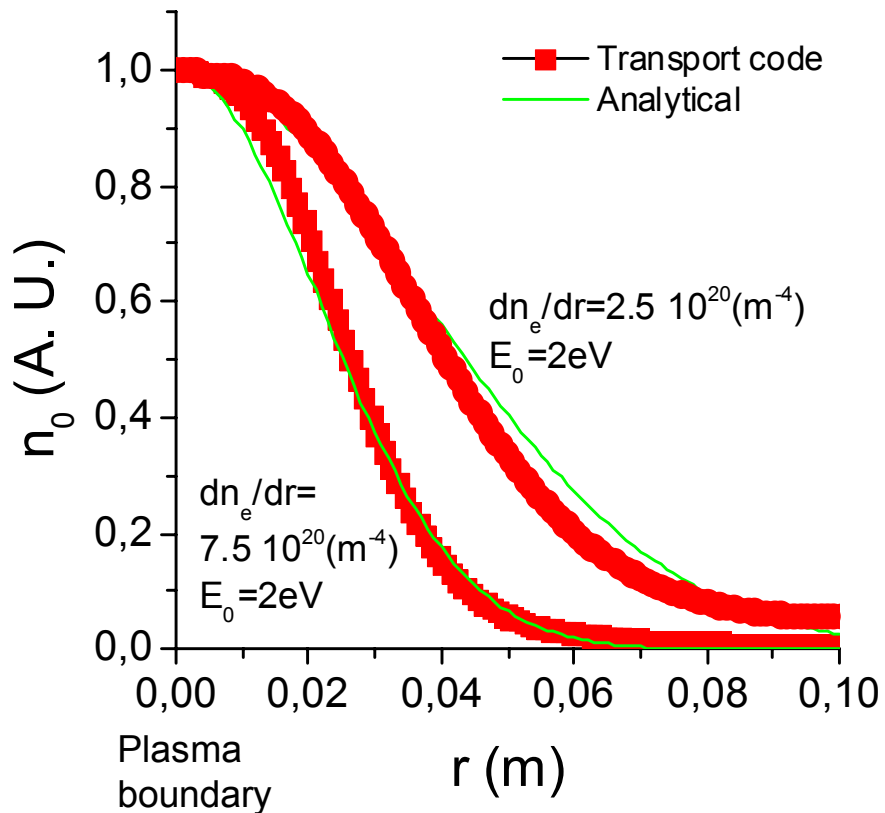
$$\vec{\Gamma}_0 = \vec{V}_0 \cdot n_o$$

$$\vec{V}_0 \cdot \vec{\nabla} n_o + n_e n_o \langle \sigma v \rangle_{ion} = 0$$

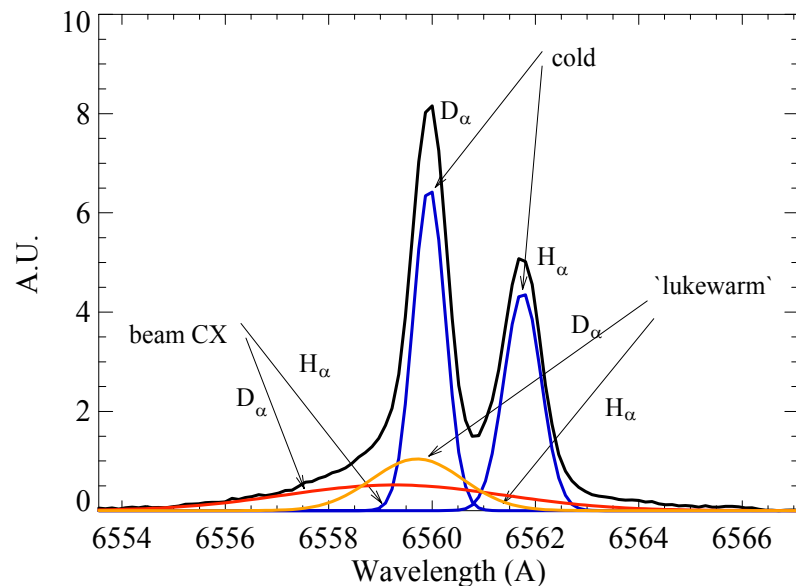
V_0 - is neutral influx velocity

$$n_o = n_o(0) \exp\left(-\frac{\langle \sigma v \rangle_{ion}}{2V_0} \frac{dn_e}{dr} r^2\right)$$

Edge neutral density



- n_0 analytical profiles compared with 1D Monte-Carlo neutral transport code
- Estimates of neutral influx velocity from D_α Doppler edge measurements ($\sim 1eV$)





D_α emissivity (analytical)

$$\left. \begin{array}{l} n_e = \frac{dn_e}{dr} \cdot r \\ \langle \sigma v \rangle_{ion}, \langle \sigma v \rangle_{ex} \sim const \end{array} \right\} \Delta_\alpha \text{ of } D_\alpha - ?$$

$$D_\alpha = \frac{dn_e}{dr} n_e r \cdot n_o(0) \exp\left(-\frac{\langle \sigma v \rangle_{ion}}{2V_0} \frac{dn_e}{dr} r^2\right) \langle \sigma v \rangle_{ex}$$

Radial position
at D_α -max

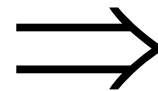
$$\frac{dD_\alpha}{dr} \Rightarrow r_\alpha = \sqrt{\frac{V_0}{\langle \sigma v \rangle_{ion} dn_e/dr}}$$

FWHM D_α emissivity (analytical)

$$D_\alpha(r_\Delta) = \frac{D_\alpha(r_\alpha)}{2} \rightarrow r_\Delta \text{ positions at } D_\alpha \text{ half max}$$

$$\xi \exp\left(-\frac{\xi^2}{2}\right) = \frac{1}{2} \exp\left(-\frac{1}{2}\right) \quad \text{where} \quad \left\{ \begin{array}{l} \xi - \text{dimensionless} \\ \xi = \sqrt{\frac{\langle \sigma v \rangle_{ion}}{V_0} \frac{dn_e}{dr}} \cdot r_\Delta \end{array} \right.$$

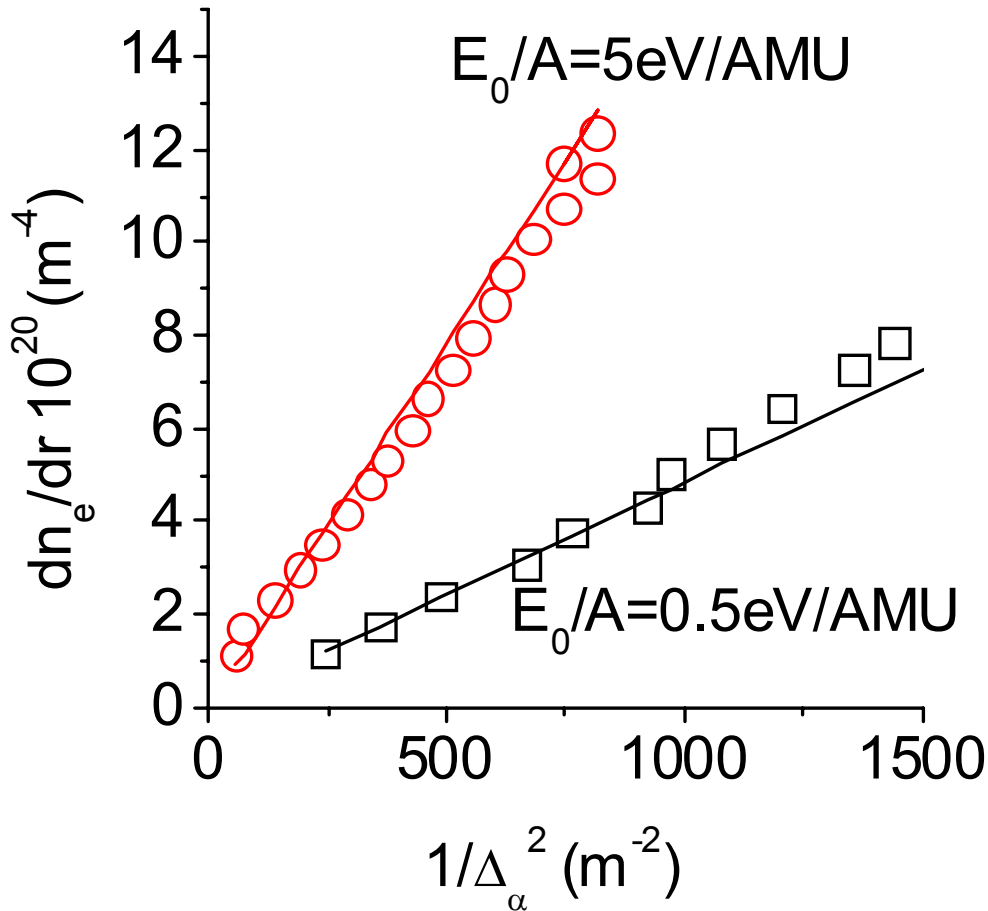
$$\Delta_\alpha \approx 1.62 \sqrt{\frac{V_0}{\langle \sigma v \rangle_{ion} \frac{dn_e}{dr}}}$$



$$\frac{dn_e}{dr} \approx \frac{V_0}{\langle \sigma v \rangle_{ion}} \left(\frac{1.62}{\Delta_\alpha} \right)^2$$

n_e gradient, dn_e/dr , is proportional to V_0/Δ_α^2

Modelling FWHM D_α

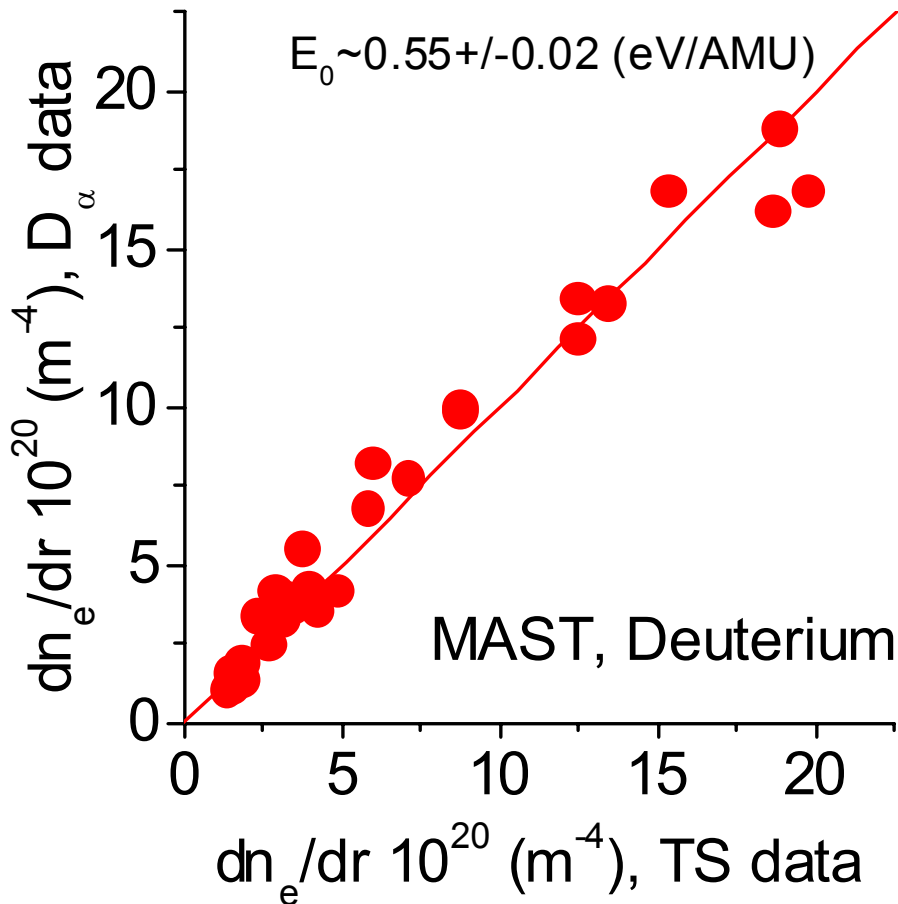


- Neutral transport code
- $\langle \sigma v \rangle_{\text{ex,ion}}$ - from ADAS
- Various influx velocities
- Solid line - analytical model

n_e gradient almost proportional to $1/\Delta_{\text{FWHM}}^2$

$$\frac{dn_e}{dr} \propto \frac{V_0}{\Delta^2}$$

TS cross-correlation



- Taken at TS time
- Modified TANH fit
- dynamic range ~ 15
- $1.3 \cdot 10^{20} \text{ m}^{-4} < dn_e/dr < 2 \cdot 10^{21} \text{ m}^{-4}$
- $E_0 \sim 0.55 \pm 0.02$ eV/AMU
- Initial error estimates

MAST data show almost linear dependence of n_e gradient on $1/\Delta^2_\alpha$



Source of Errors

Inversion makes accountability complicated

- inaccurate calibration
- other emission lines
- H impurity

10% H \rightarrow Δ_{α} (3%), dn_e/dr (5%)

“Monte Carlo” technique

- Noise errors

ideal spectra + Poisson (photon/statistical noise)
+ Normal (read-out noise)

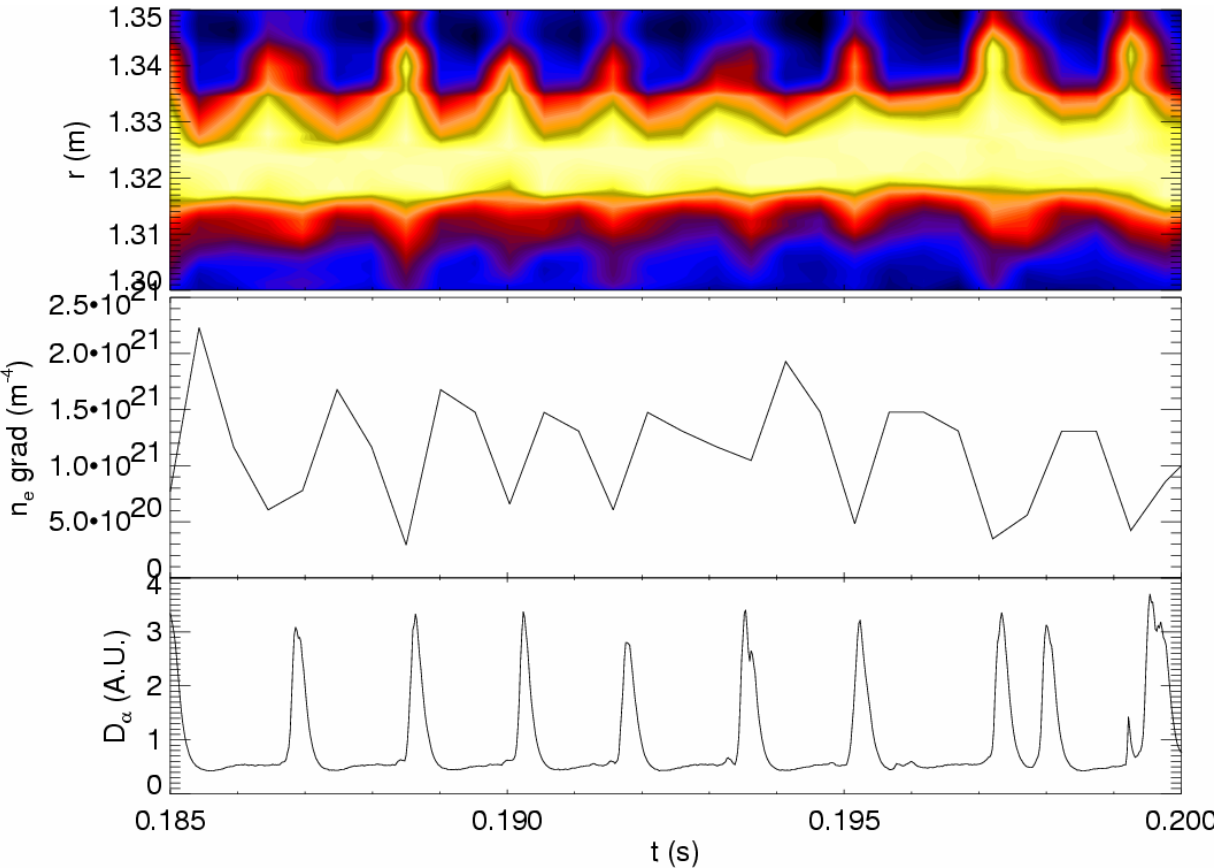
Δ_{α} (5%) \rightarrow dn_e/dr (10%)

- Systematic errors (10%)

H-mode studies

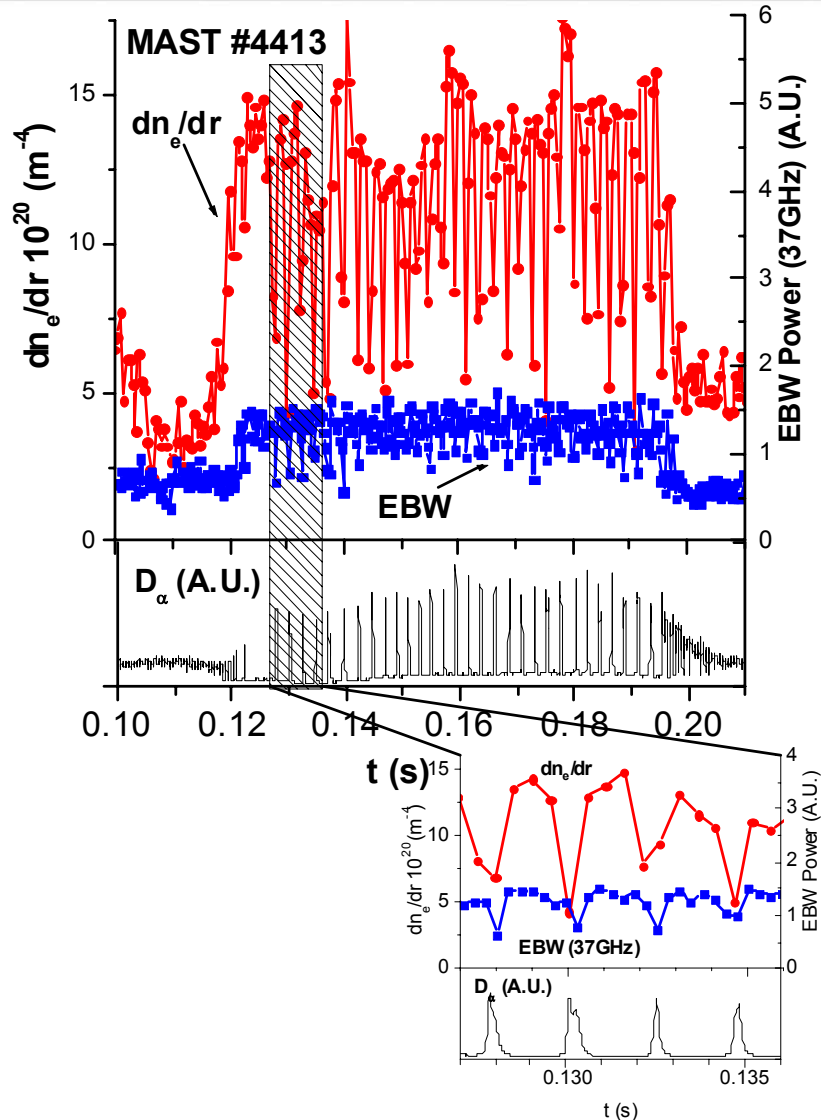


MAST #4415



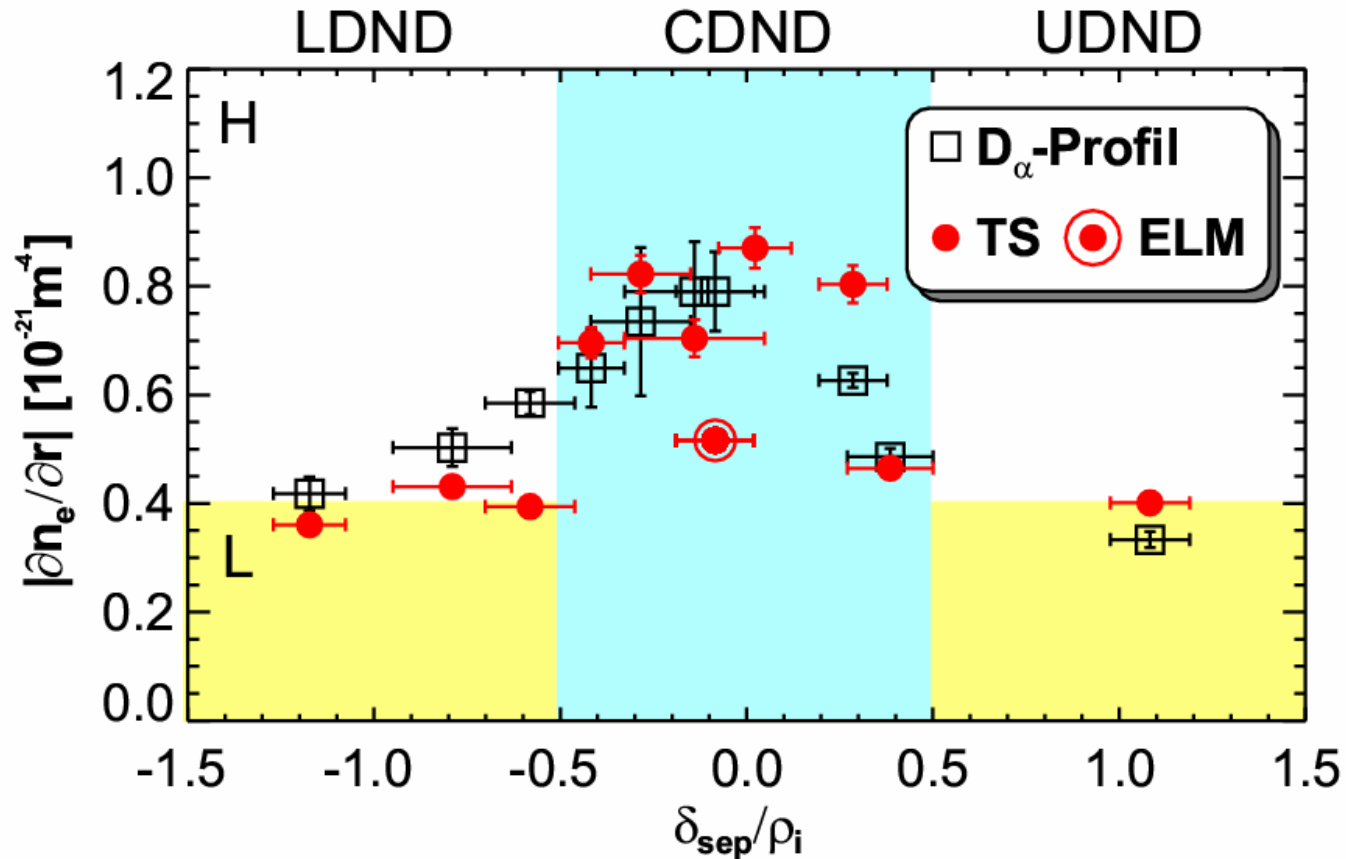
MAST data show rise
 n_e gradient during
inter ELM period

EBW correlates well with n_e gradient



- n_e gradient increases during ELM-free period
- EBW emission correlates well with n_e gradient changes

H-mode study



Magnetic configuration study in MAST H-mode plasmas



Conclusions

Method

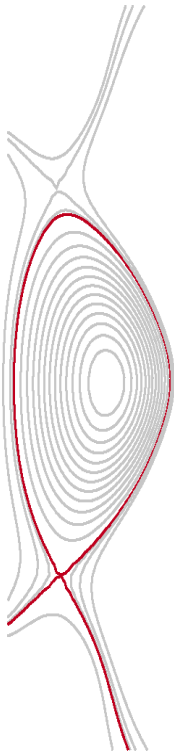
- simple, exploiting atomic physics, no extra cost
- higher repetition rate than TS
- n_e gradient is an importance for H-mode studies
- extracting neutral influx energy
- cross calibration of diagnostics

Anticipated development

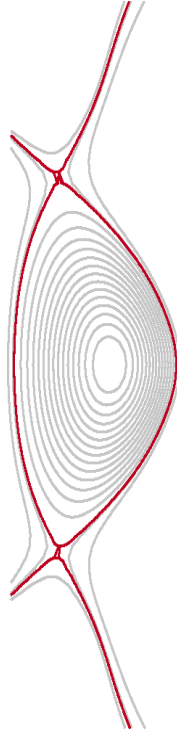
- real time plasma control for plasma feedback
 - Pick-up coils remote from plasma
 - Quasi continuous (ITER)
- use fast camera, - x-point region, total particle influx
- monitoring D_α , D_β and D_γ emissions to yield edge n_e and T_e

Magnetic configuration study

L-SND



CDN



U-SND

