



# Breeding Potential and Blanket / Materials Testing Strategy for FNSF

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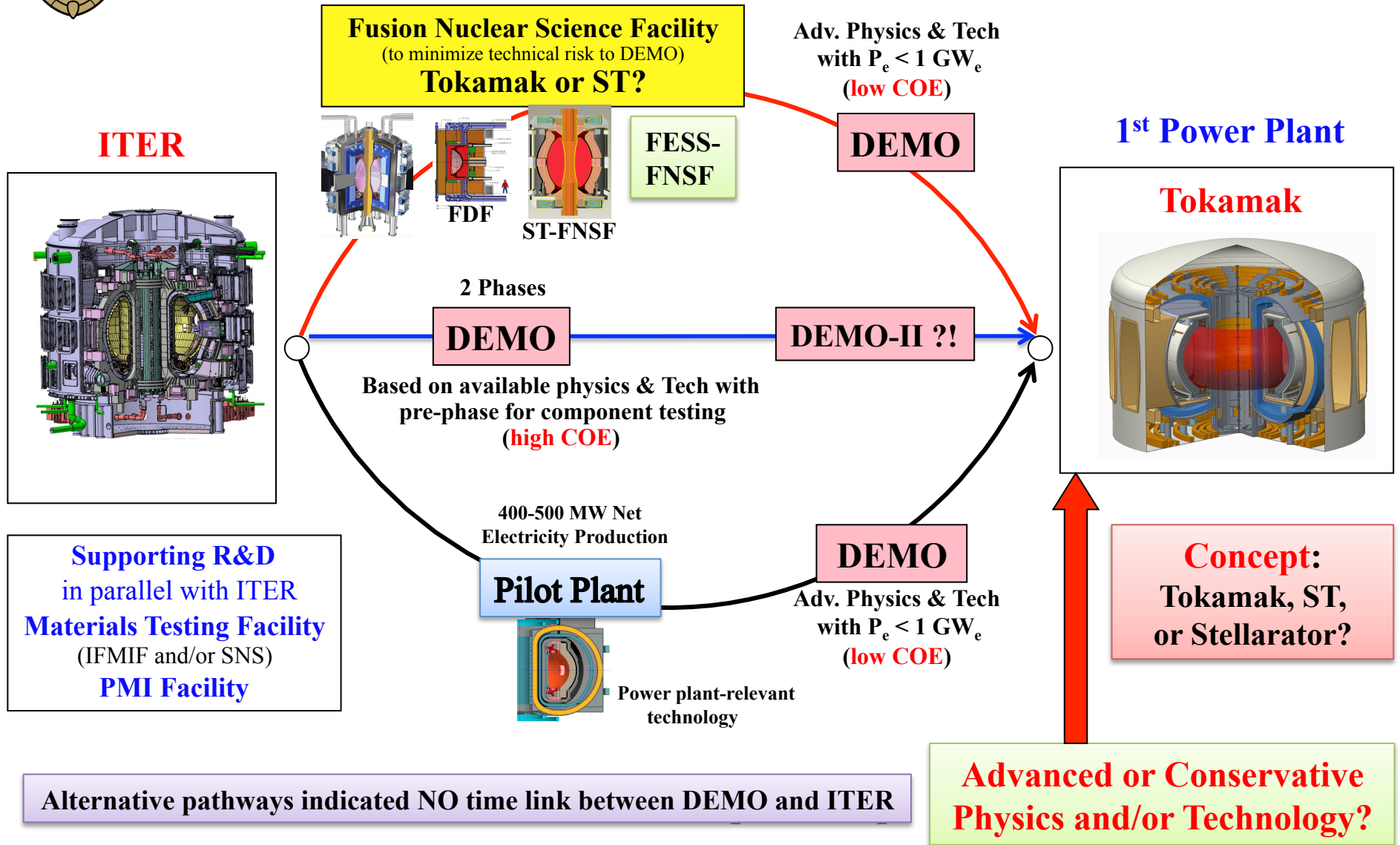
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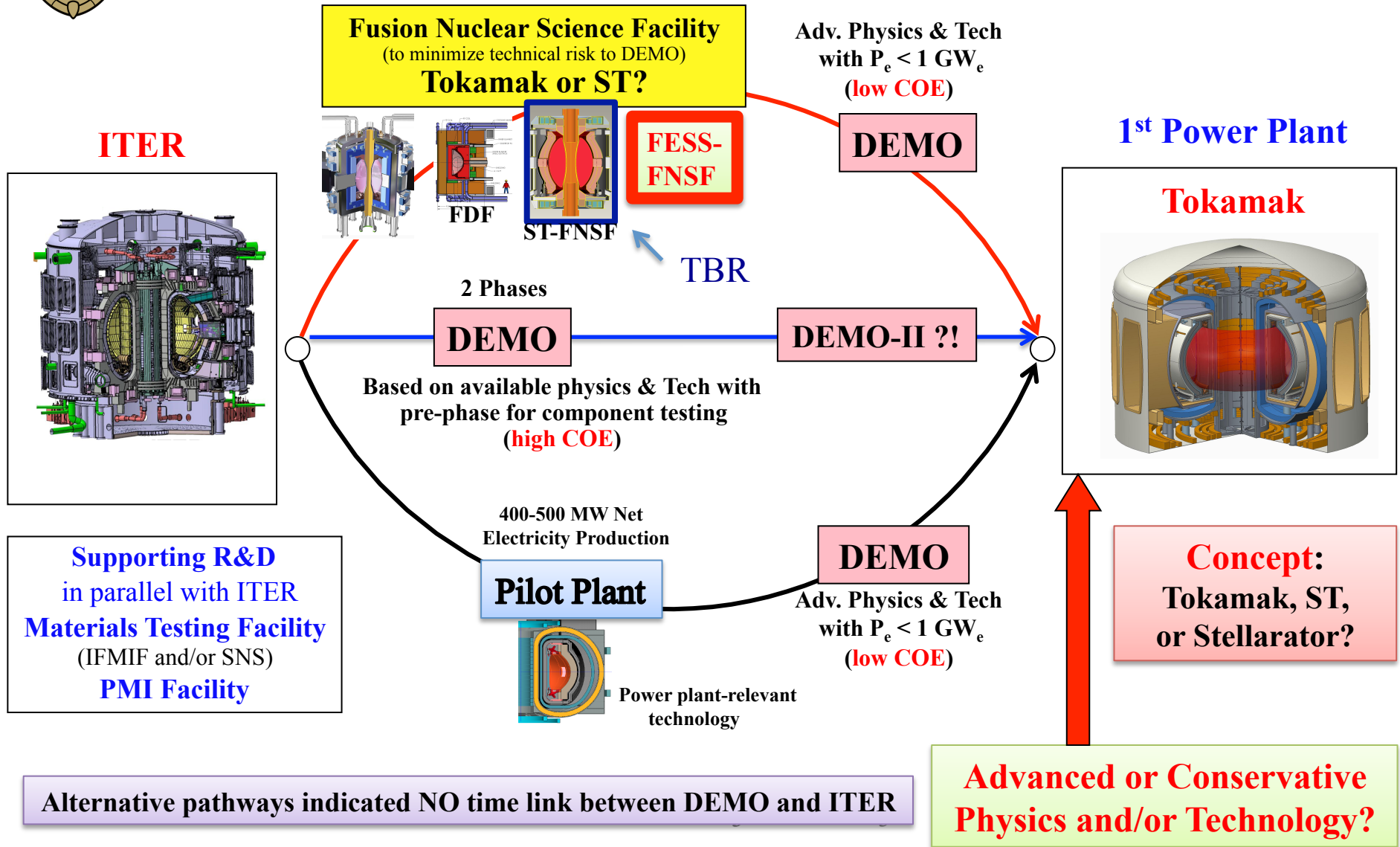
# Pathways to Fusion Energy

(Which Pathway offers Lowest Risk?)





# This Talk Focuses on **FESS-FNSF** (DOE funded project; under development)





# Outline

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- FESS-FNSF **radiation environment**.
- **Novel testing strategy** to develop and **qualify DCLL blankets and materials** for DEMO and power plants.
- FNSF **breeding** potential.

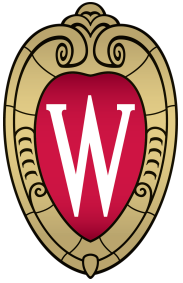
# **Radiation Environment**



# FNSF Operating Schedule\*

Fuel Cycle	He/H	D-D	D-T		D-T	D-T	D-T	More?
	Plasma physics		Low Fluence Fusion Nuclear Break-in			High Fluence Fusion Nuclear Operation		
<b>Phase</b>	<b>1</b>	<b>2</b>	<b>3</b>	<b>4</b>	<b>5</b>	<b>6</b>	<b>7</b>	
Phase Time (y)	1.5	1 2	1 3	1 5	1 5	1 7	7	
FNSF Operating Time (y)	1.5	3.5	6.5	11.5	16.5	23.5	30.5	
$N_w^{peak}$ , MW/m <sup>2</sup>		~0.009	1.5	1.5	1.5	1.5	1.5	
Plasma on-time per year (days)	10-25% (37-91)	10-50% (37-183)	10-15% (37-55)	25% (91)	35% (128)	35% (128)	35% (128)	
FPY			0.3 – 0.45	1.25	1.75	2.45	2.45	
Peak EOL Fluence (MWy/m <sup>2</sup> )			0.45-0.68	1.88	2.63	3.68	3.68	
Cumulative EOL Fluence			0.68	2.56	5.19	8.87	12.55	
Plasma duty cycle (days on/days off)		0.33-0.95 1/2 – 10/0.5	0.33 1/2	0.67 2/1	0.91 5/0.5	0.95 10/0.5	0.95 10/0.5	
Operation / Maintenance per year (days)			111-165/254-200	137 / 228	141 / 224	135 / 230	135/230	
Peak dpa			4.5-6.8	18.8	26.3	36.8	36.8	
Cumulative dpa			6.8	25.6	51.9	88.7	125.5	
Total # of plasma cycles			111-165	230	130	91	91	

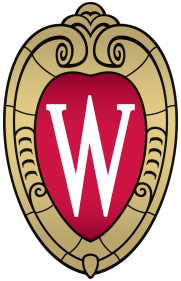
\* C.E. Kessel et al., The Fusion Nuclear Science Facility (FNSF), the Critical Step in the Pathway to Fusion Energy, presented at 21<sup>st</sup> TOFE-2014.



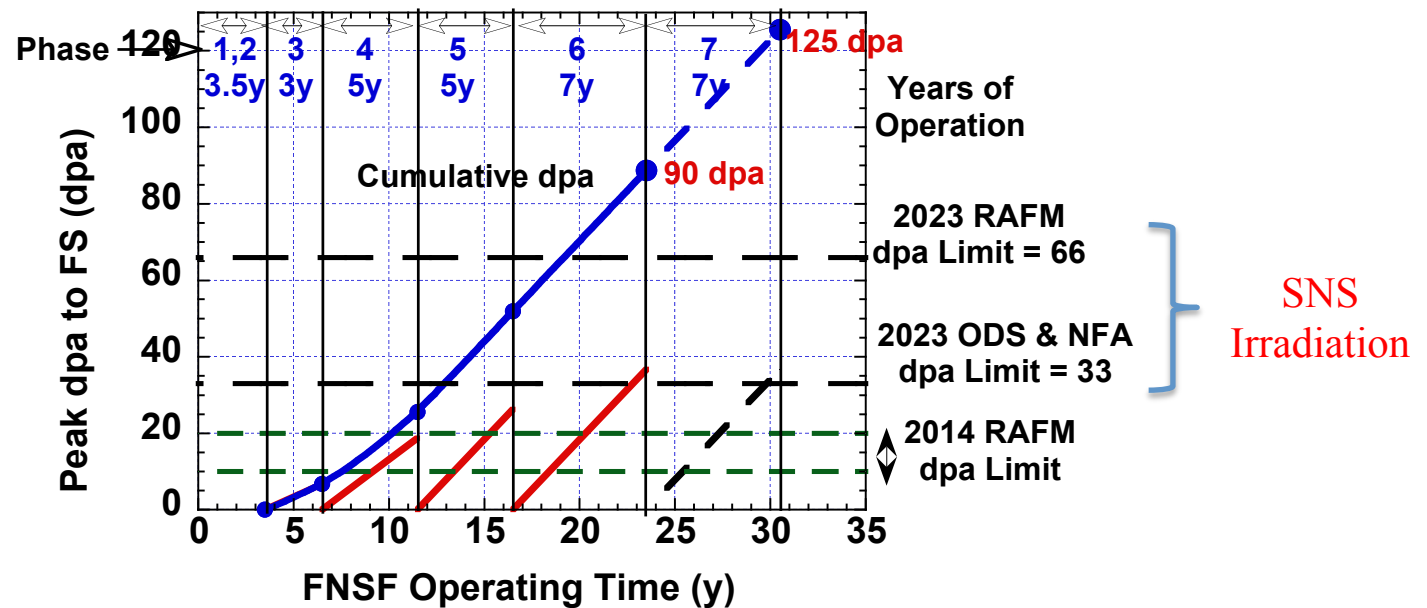
# FNSF Assumptions

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- Tokamak concept.
- 8 ports: 4 TBMs, 1 MTM, and 3 H/CD ports on OB side.
- 10 dpa/FPY per MW/m<sup>2</sup>.
- 10-20 dpa **present** limit for RAFM FS.
- Possibility of pre-FNSF irradiation in SNS (@ 5.5 dpa/FPY) could yield:
  - 66 dpa in 12 y for RAFM FS
  - 33 dpa in 6 y for ODS-FS
  - 33 dpa in 6 y for Nano-Structured Ferritic Alloys (NFA).



# Radiation Damage and Lifetime of RAFM Structure (OB midplane)

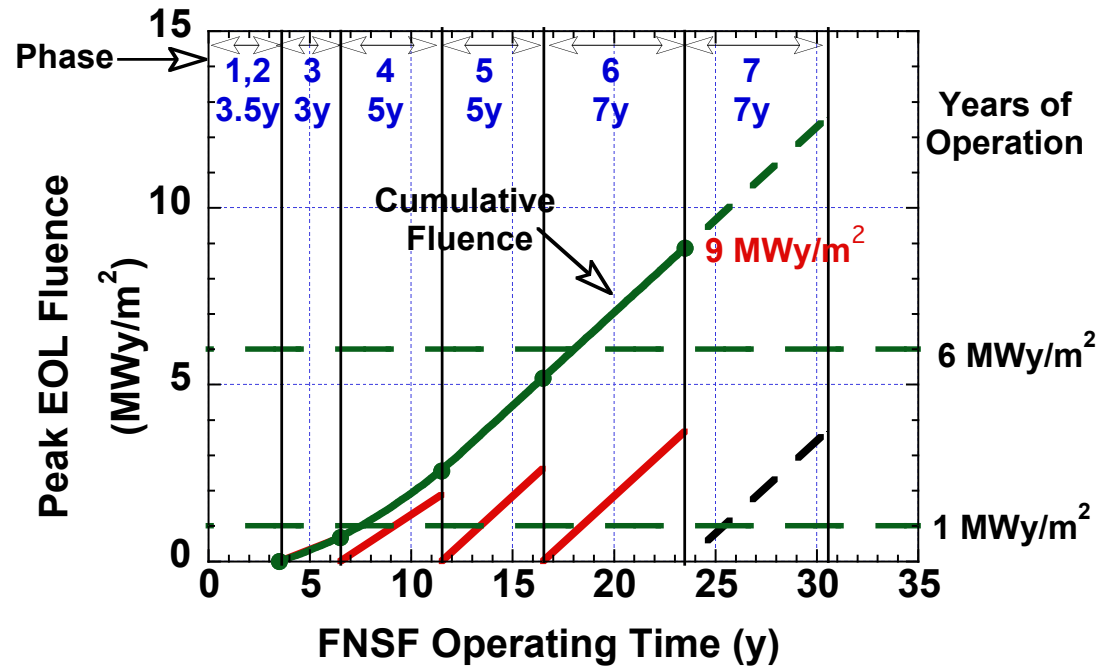


- Structural material replacement may coincide with end of Phase.
- Testing modules (TBM and MTM) could remain in place to achieve high fluence (66 dpa for RAFM FS, 33 dpa for ODS-FS, and 33 dpa for NFA).
- **Cumulative dpa could reach 90-125 dpa max @ OB midplane.**
- What other failure mechanism could limit RAFM structure lifetime?
- How long should TBM/MTM operate to provide meaningful testing? EOL fluence?





# End-of-Life Fluence for Testing (OB midplane)



- Should TBM EOL fluence coincide with end of phase (0.7 – 3.7 MWy/m<sup>2</sup> for 6 – 37 dpa)?
- EOL fluence could reach 9 – 12 MWy/m<sup>2</sup> for 90 -125 dpa @ OB midplane.
- What is the ultimate **fluence goal** for meaningful testing?
  - 1 MWy/m<sup>2</sup> (for reliable operation; ~0.7 FPY)?
  - 6 MWy/m<sup>2</sup> (for operating over long time of exposure; ~4 FPY)?

# **Blanket Testing Strategy**



# Blanket Testing, Development, and Qualification

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- **Goal:** Qualify preferred US blanket concept (DCLL) for DEMO (and power plants) through testing, developing, and enhancing performance during each phase of FNSF operation.
- **Novel Strategy** that reaches beyond traditional testing mission of ITER: Four generations of DCLL blanket concept tested first in test blanket modules (TBM with limited dimensions), and then converted (assuming +ve results) into full sector for qualification before use in DEMO (and power plants).
- **Requirements:**
  - TBMs located at outboard (OB) midplane (where neutron flux peaks)
  - Surrounding DCLL blanket utilized for tritium breeding, qualification, and reliability growth testing.
- **Staged blanket testing:** During operation, TBM serves as “forerunner” and develops more advanced blanket technologies for GEN-II, III, and IV DCLL blanket systems.
- **Combined results** from TBMs and blanket systems are essential to build high confidence and lower risk for successful operation of advanced blankets in DEMO (and power plants).

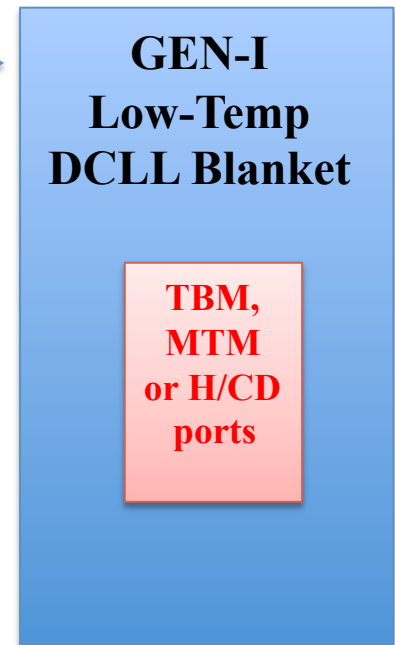




# GEN-I DCLL Blanket Installed at Beginning of FNSF Operation

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- To breed tritium, **low-temperature, robust, and highly reliable blanket** installed at beginning of FNSF operation and covers entire space surrounding 4 TBMs, 1 MTM, and 3 H/CD ports.
- To assure high reliability, **sufficient margins to absolute limits** (maximum structure temperatures, inter-phase temperatures to coolant, and mechanical stresses) should all be considered in designing GEN-I blanket coupled **with extensive pre-FNSF R&D blanket program** \*.



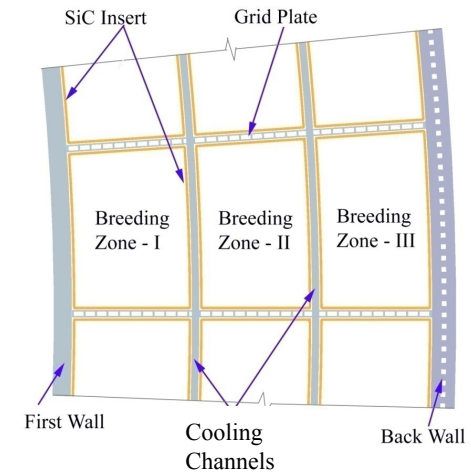
\* S. Smolentsev et al., R&D Needs and Progress Measurement for Liquid Metal Blankets and Systems on the Pathway from Present Experimental Facilities to FNSF, presented at 21<sup>st</sup> TOFE-2014.



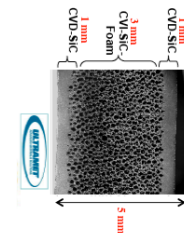
# Proposed Low-Temperature GEN-I DCLL Blanket

- Operates with moderate coolant temperature (e.g., FS temperature of 400-500°C and LiPb and He inlet/outlet temperature of 350/450°C).
- Requires FCI to serve as electric insulator to control MHD pressure drop. (Since operating temperature is not too high, FCI does not serve as thermal insulator).
- Temperature in FW and blanket structure as uniform as possible to minimize thermal stresses.
- Since SiC FCI may not be developed and qualified before operating FNSF, sandwich-like FCI made of FS/alumina/FS multilayer could be employed for GEN-I blanket.

## Typical DCLL Blanket Layout



### SiC FCI



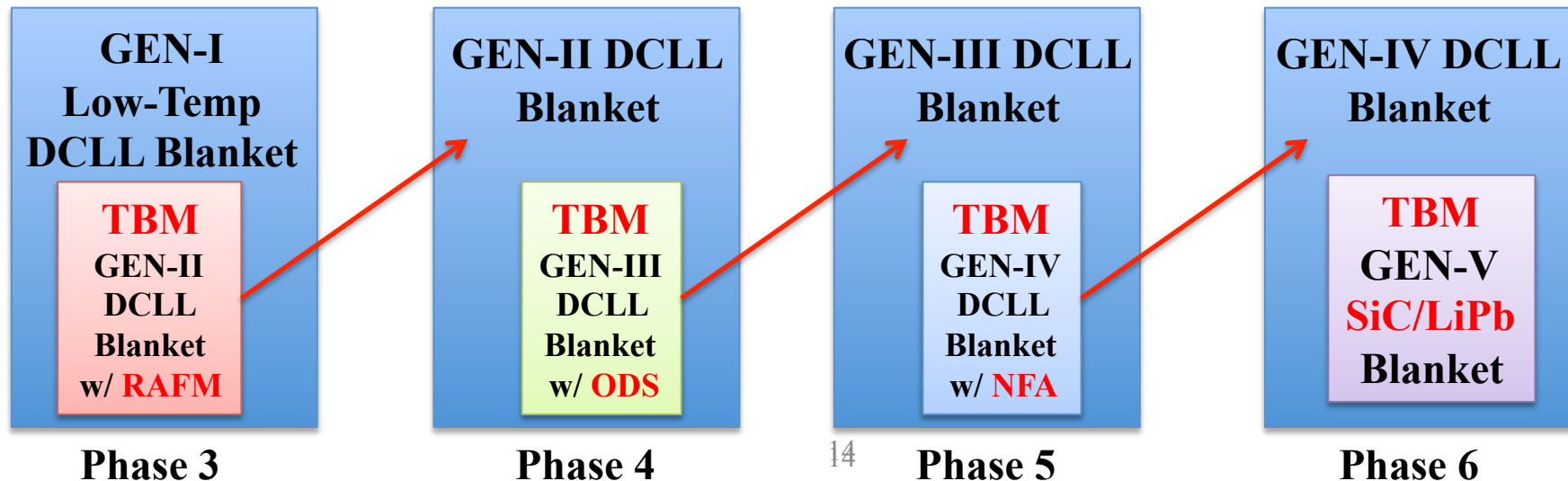
### FS/Al<sub>2</sub>O<sub>3</sub>/FS FCI



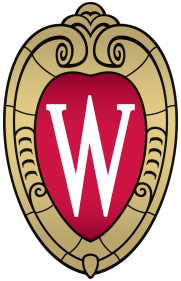


# DCLL Blanket Development, Testing, and Qualification

- **Five generations of blankets will be developed for FNSF:**
  - **GEN-I** low-temperature DCLL blanket: with FS/Alumina/FS FCI, RAFM structure (F82H of EUROFER) operating at 350-550°C, maximum LiPb and He exit temperature of 450°C, and maximum interface steel/LiPb temperature of 450°C.
  - **GEN-II** DCLL blanket first tested successfully in TBM and later installed in all sectors to qualify it if necessary for DEMO and/or power plants: DCLL blanket with SiC FCI, RAFM structure operating at 350-550°C, LiPb exit temperature of 700°C, He exit temperature of 500°C, and maximum interface steel/LiPb temperature of 500°C (for corrosion considerations).
  - **GEN-III** DCLL blanket first tested successfully in TBM and later installed in all sectors to qualify it if necessary for DEMO and/or power plants: DCLL blanket with SiC FCI, ODS-FS structure operating at 600°C, LiPb exit temperature of 750°C, He exit temperature of 500°C, and maximum interface steel/LiPb temperature > 500°C.
  - **GEN-IV** DCLL blanket first tested successfully in TBM and later installed in all sectors to qualify it if necessary for DEMO and/or power plants: DCLL blanket with SiC FCI, NFA structure operating at 700°C, LiPb exit temperature of 800°C, He exit temperature of 500°C, and maximum interface steel/LiPb temperature > 500°C.
  - **GEN-V** SiC/LiPb blanket tested in TBM for more advanced DEMO or power plants: advanced SiC/LiPb blanket with SiC/SiC composites operating at 1000°C and LiPb exit temperature of 1100°C.
- For GEN III and IV blankets, it is assumed that ODS-FS and NFA (that operate at higher temperatures than 550°C) are employed everywhere in FW and blanket to enhance radiation lifetime and thermal conversion efficiency. LiPb/FS corrosion solutions should be found by 2030.

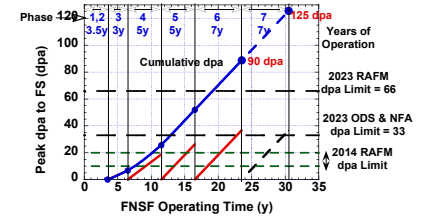


# **Materials Testing Strategy**



# MTM Will Develop More Advanced Materials for Fusion

- **Goal:** Develop comprehensive multi-materials database for **up to 90 dpa** with possibility of **extending tests to 125 dpa in Phase #7**.
- Whole **list of new materials** could be tested in MTM:
  - New GEN of FS (as first generation of ferritic steels (F82H and EUROFER) are **not** performing well at high and low temperatures):
    - Extend max operating temp into 550-1000°C regime (for FW, blanket, SR, and divertor)
    - Develop FS variant less susceptible to DBTT in low-temp regime (for VV and LT shield)
    - Develop reusable NFA if temp exceeds 1000°C during severe accidents.
  - SiC/SiC composites for FW/blanket
  - W alloys (W-TiC, WL10, W-K, W/W composites, VMW, etc.) for divertors
  - LTS and HTS magnet materials: superconductors, jackets, insulators, etc..
- Pre-FNSF characterization and **theoretical predictive modeling** using advanced computing methods will **define MTM testing environment**.







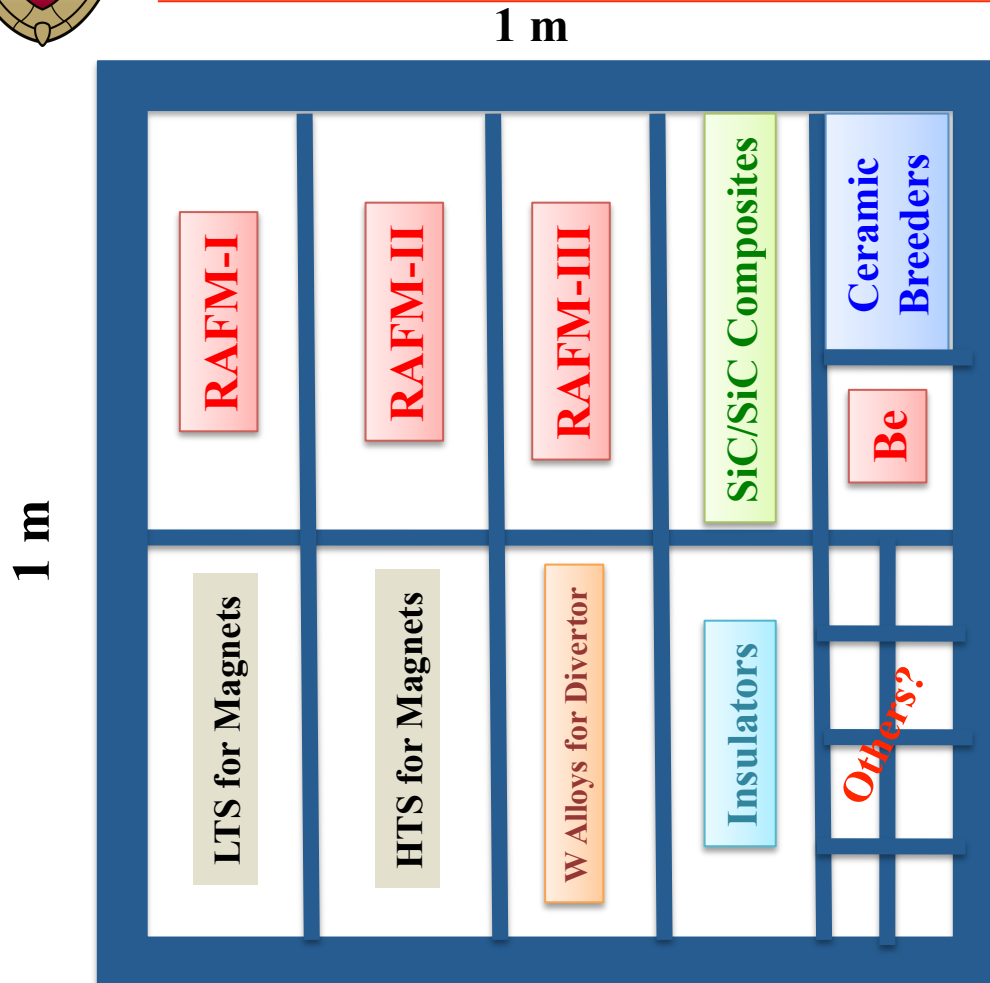
## MTM Provides Critically Important Resource for Evaluation and Validation of Materials Performance in 14 MeV Neutron Environment

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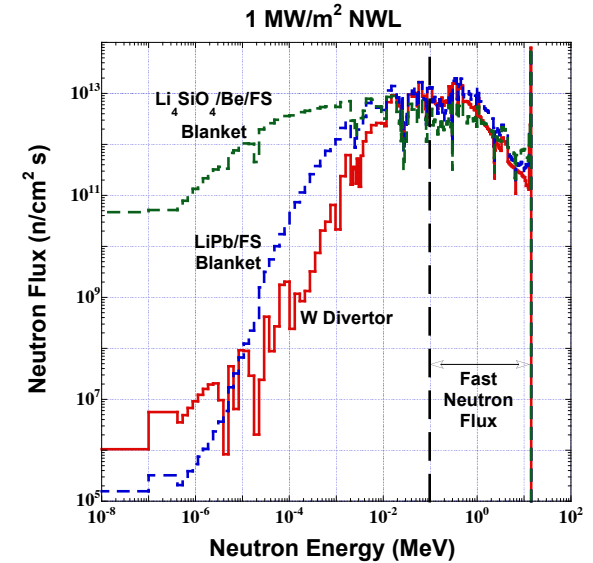
- Other data developed with continuous radiation sources (SNS, IFMIF or early Neutron Source):
  - Is essential for **developing science-based understanding of 14 MeV neutron radiation damage phenomena** that underpins development of damage-resistant materials.
  - Forms basis for **developing engineering database** for designing and licensing FNSF.
- MTM is **complementary resource** with advantages of:
  1. Carrying higher **multiplicity of larger specimens** compared to 10-500 ml range available in the SNS/IFMIF
  2. Providing radiation effects data in **pulsed neutron environment**
  3. Providing **surveillance program** to track performance of several materials irradiated in same 14 MeV neutron environment using **range of specimen geometries**
  4. Provide a means of irradiation **testing of new materials variants** arising from:
    - Continuing development of improved compositions/microstructures
    - Application of advances in fabrication technologies (additive manufacturing, precision casting, joining technologies, etc).



# MTM Offers Testing in Real Fusion Environment (unavailable in IFMIF, HFIR and SNS)



## Fusion Spectra



Replaceable FS structural frame upon reaching dpa limit while tested materials could be re-installed after each change out.

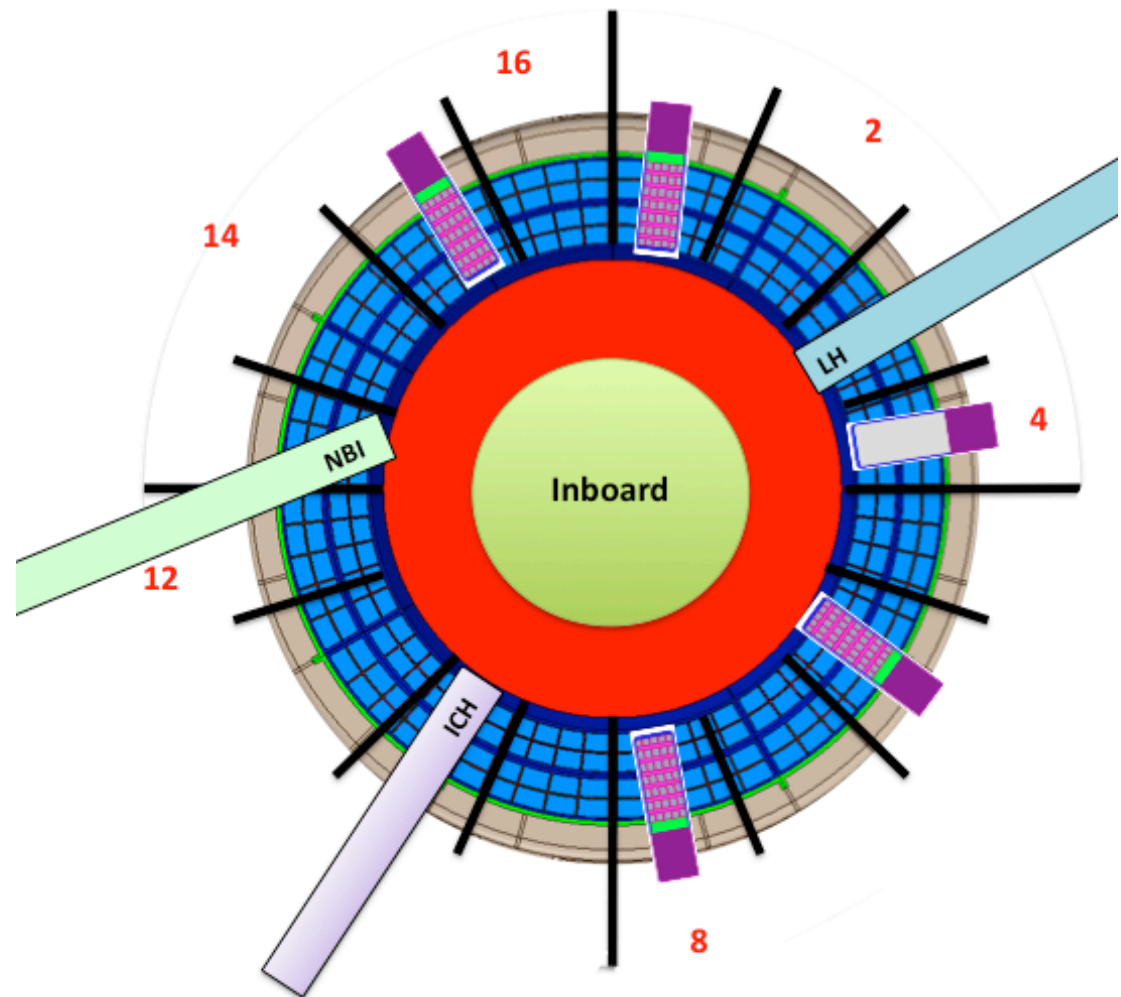
**Layout of material samples within MTM  
(with varying shapes, sizes, thicknesses, etc.)**

# **Preliminary Layout of FNSF with 8 Ports**



# Layout Guidelines

- **16 sectors:**
  - 8 sectors containing 8 ports
  - 8 sectors w/o ports.
- High degree of neutron flux symmetry at TBM surface is desirable in order to compare blanket concept performance under same operating conditions
- TBM ports at OB midplane should be arranged to exchange TBMs and MTM rapidly. All coolant pipes should be accessible from outside VV.



# **FNSF Breeding Potential**



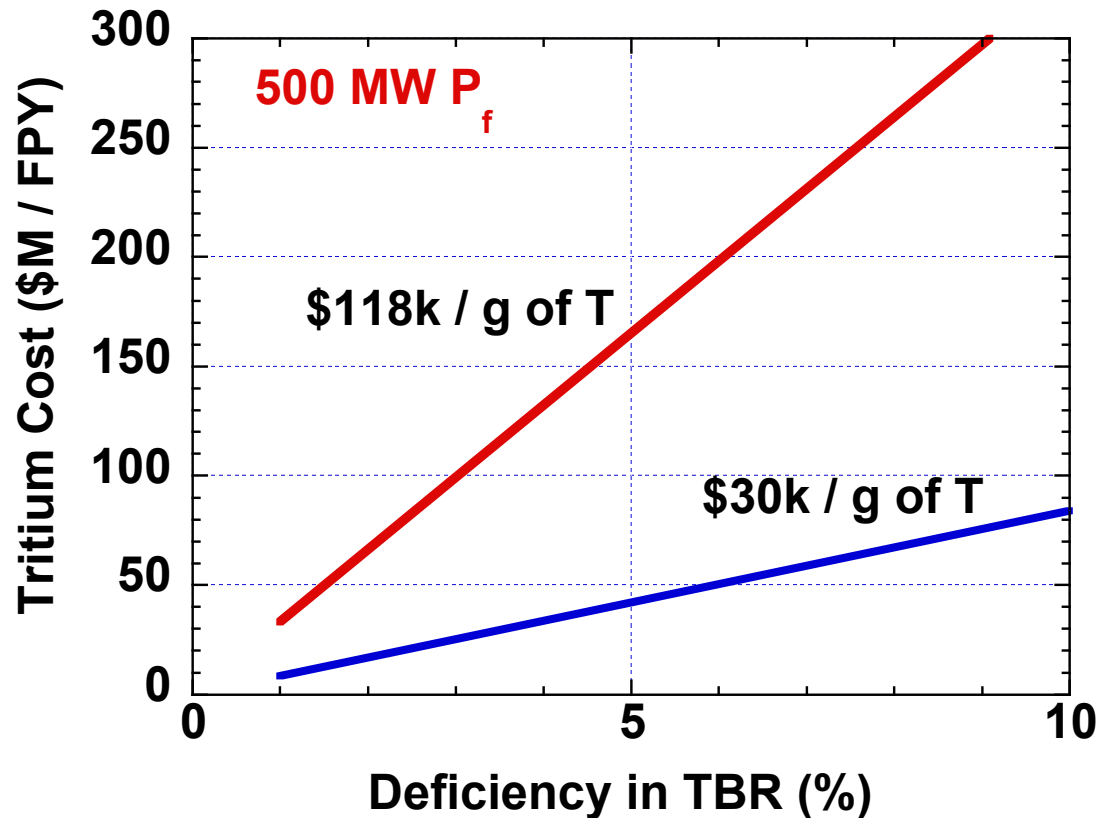
# Tritium Breeding Ratio (TBR)

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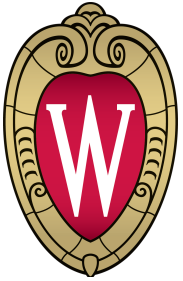
- TBR is a metric for T self-sufficiency  $\Rightarrow$  **Calculated TBR > 1.**
- FNSF **must breed their own T** needed for plasma operation as external sources of T are insufficient, impractical, and/or inaccessible. (Available T resources from CANDU reactors will all be used by ITER).
- Annual T consumption for **500 MW** fusion power is high (**28 kg per full power year (FPY)**).
- T is extremely expensive (**\$30-118k per gram**).



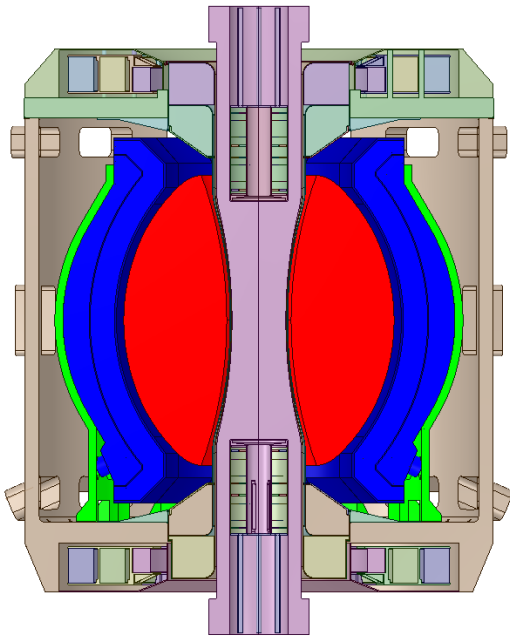
## Small Deficiency in TBR Represents Significant Contribution to FNSF Operational Cost



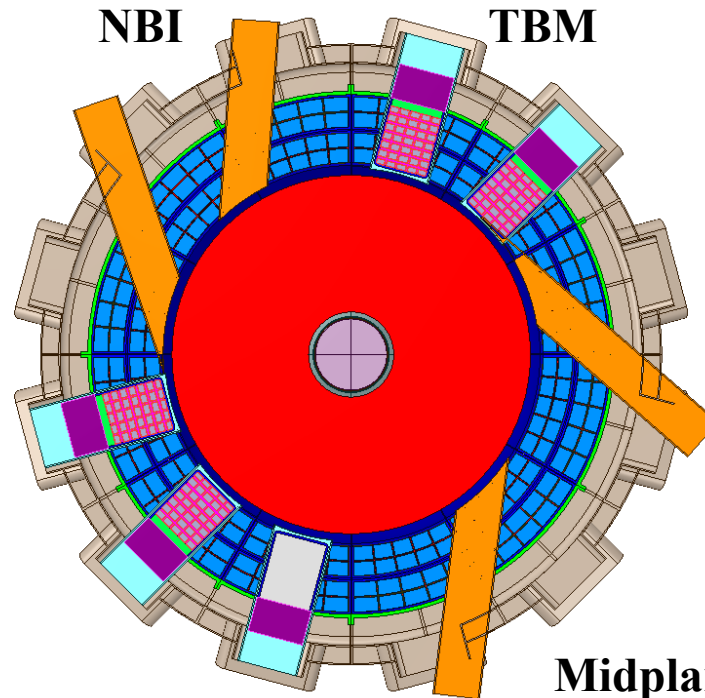
- **1% less TBR in FNSF** means T shortage of ~300 g/FPY, costing **\$8-33M** to purchase annually from *unknown* external sources.
- TBR must meet breeding requirement and should be calculated with high accuracy.



# Example: TBR of ST-FNSF (1.7 m Device)



**3-D Neutronics Model  
(R= 1.7 m)**



**MTM**

**Midplane Cross Section with  
4 TBMs, 1 MTM, and 4 NBIs**

**TBR ~ 0.97**

## **Design measures to enhance TBR:**

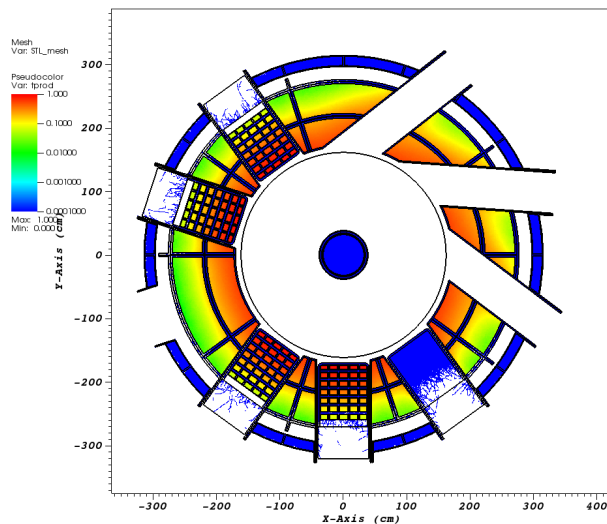
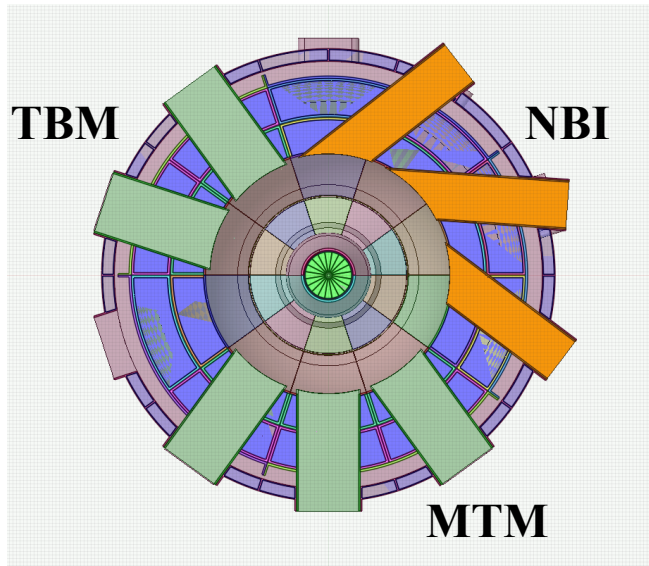
- Less cooling channels within blanket
- Replace PF coil shield by blanket (~3%)
- Smaller opening to divertor to reduce neutron leakage
- Thicker IB VV with internal breeding.

1.7 m device has potential to achieve TBR > 1  
– major advantage over smaller devices



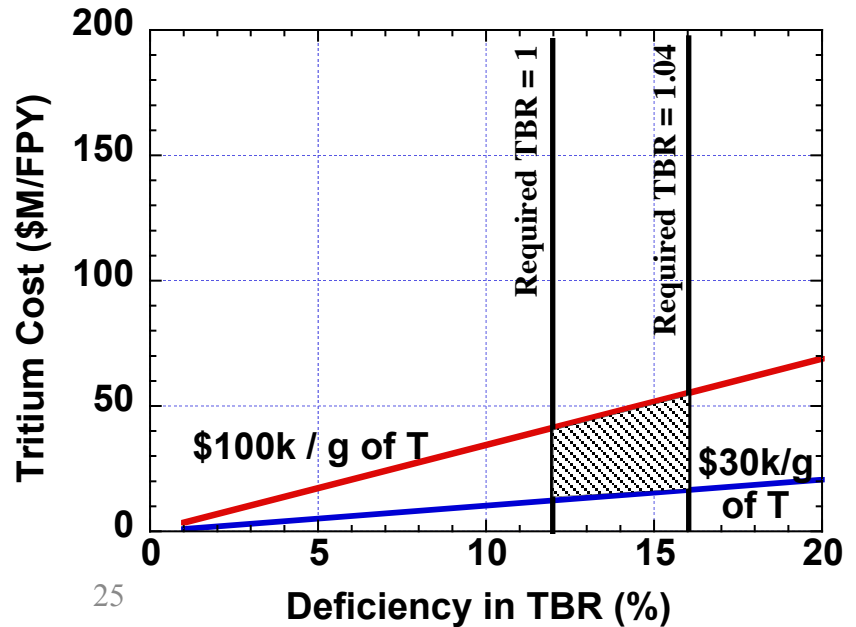


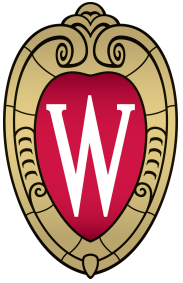
# Example: TBR of ST-FNSF (1.0 m Device)



**TBR ~ 0.88**

- 1 m device cannot achieve  $TBR > 1$  even with design changes
- **Solution:** purchase ~3kg of T/FPY from outside sources at \$30-100k/g of T, costing \$12-55M/FPY.





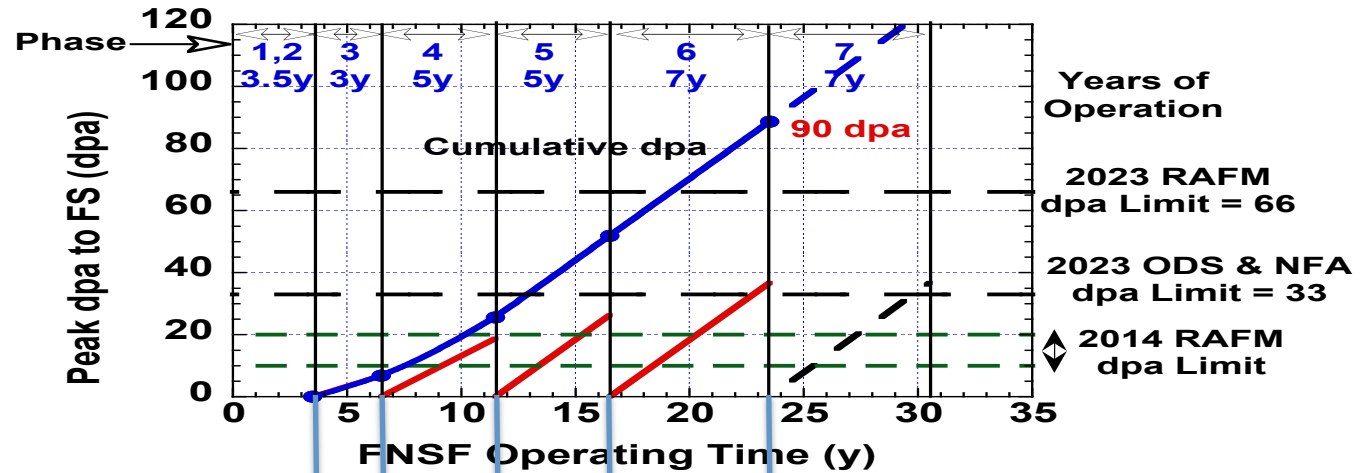
# Final Remarks

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- T self-sufficiency and materials testing should be essential part of FNSF mission.
- **TBMs and MTM** serve as preliminary breadboard prototypes to test future generations of blankets and materials in real fusion environment ( $\text{He}/\text{dpa} = 10$ ).
- **Initial blanket surrounding TBMs and MTM** must be robust and highly reliable, provide adequate tritium breeding, have adequate design margin and lifetime, and able to withstand high heat flux and disruptions during off-normal events.
- **More advanced generations of incrementally improved blanket concepts** can first be tested in TBMs, and then converted into full sectors to validate/qualify blanket for DEMO and power plants.
- **Strong pre-FNSF R&D program** combined with state-of-the-art predictive capability (extensive modeling and computer simulation) assure success of TBM testing and FNSF operation.
- **Do not limit scope of testing.** Develop flexible TBM and MTM capable of testing and validating more attractive blankets/materials than presently known.



# Single Phase Testing in FNSF



## TBM:

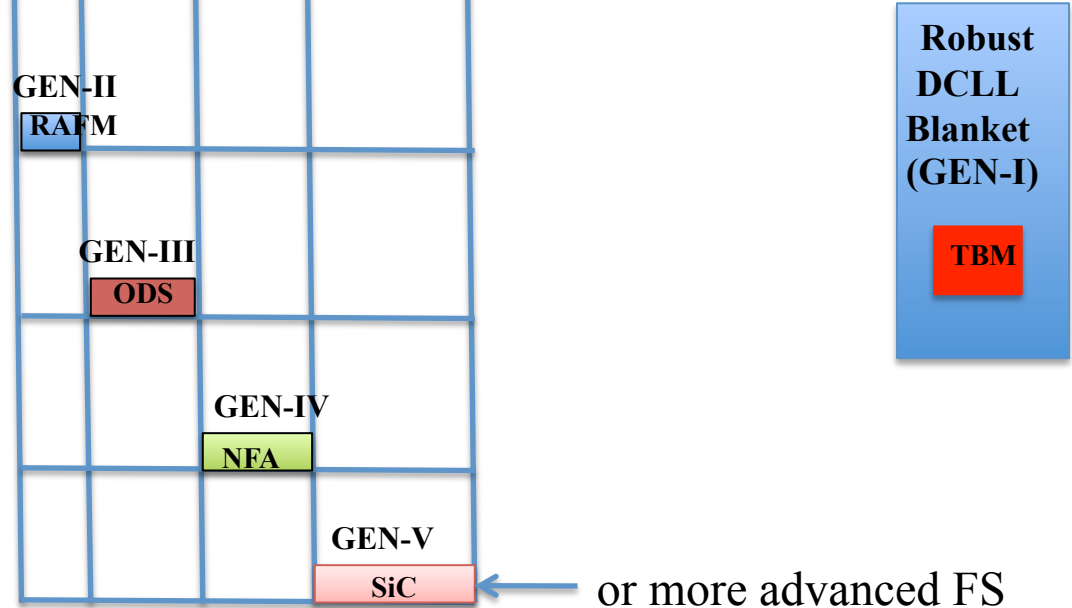
**dpa MWy/m<sup>2</sup>**

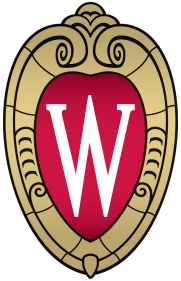
**Phase 3:** 3 y (0.45 FPY); 7 dpa; 0.7 MWy/m<sup>2</sup>

**Phase 4:** 5 y (1.25 FPY); 20 dpa; 2 MWy/m<sup>2</sup>

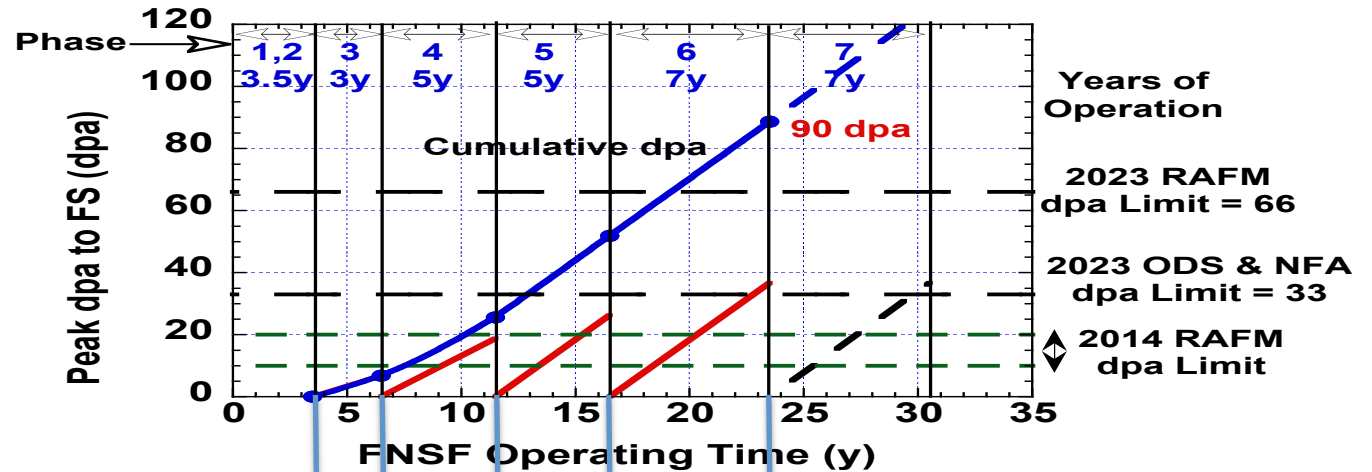
**Phase 5:** 5 y (1.75 FPY); 26 dpa; 2.6 MWy/m<sup>2</sup>

**Phase 6:** 7 y (2.45 FPY); 37 dpa; 3.7 MWy/m<sup>2</sup>



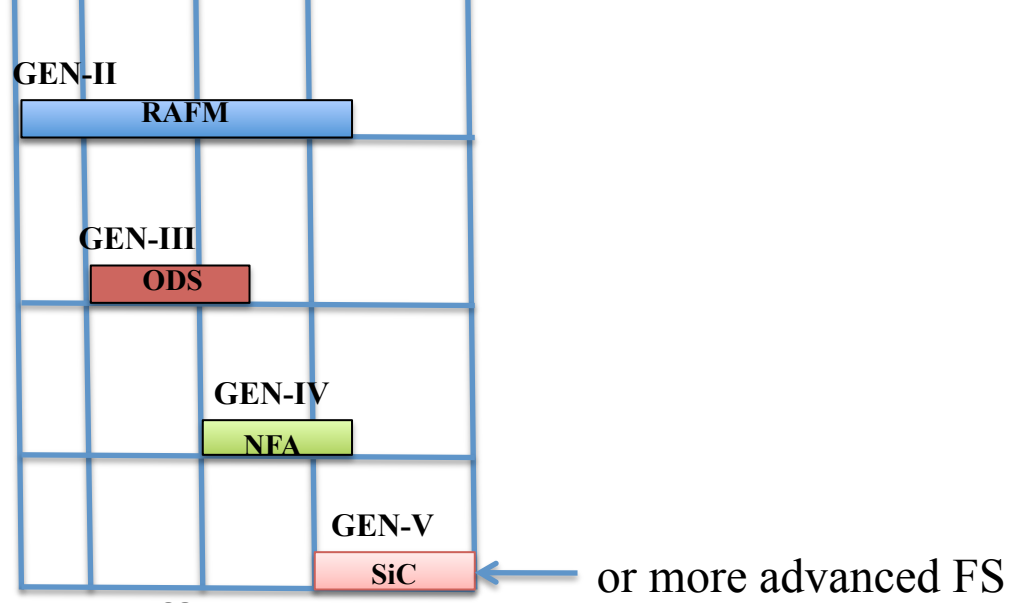


# Extending TBM Testing to Maximize Fluence



## Multiple phase testing:

	Max dpa	Max Fluence
15.5 y (4.4 FPY);	66 dpa;	6.5 MWy/m <sup>2</sup>
7.5 y (2.2 FPY);	33 dpa;	3 MWy/m <sup>2</sup>
6 y (2.1 FPY);	33 dpa;	3 MWy/m <sup>2</sup>
7 y (2.45 FPY);	?? dpa;	3.7 MWy/m <sup>2</sup>





# R&D Needs

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- Well planned R&D program for non-nuclear blanket testing\* before FNSF operation.
- State-of-the-art predictive capability to avoid failure and assure success of testing in FNSF.
- **Limited nuclear testing** (small mock-ups of blanket could be tested with 14 MeV neutrons in IFMIF, GDT, etc.).
- Specific **tests may continue** during FNSF operation.

\* S. Smolentsev et al., R&D Needs and Progress Measurement for Liquid Metal Blankets and Systems on the Pathway from Present Experimental Facilities to FNSF, presented at 21<sup>st</sup> TOFE-2014.



# MTM Attributes

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- Most important attribute would be the **much larger specimen volumes compared to 10-500 ml range** available in the SNS/IFMIF series of neutron sources.
- Provide a means of **testing larger size mechanical property specimens**:
  - Pressurized creep tubes and fracture toughness specimens with range of section thicknesses and crack geometries
  - Validation of data derived from highly miniaturized specimens irradiated in SNS/IFMIF.
- Provide a means of conducting critically important **surveillance program** using **range of specimen geometries** to track radiation-induced changes in mechanical properties and dimensional stability of FW/blanket materials, divertor materials, structural materials, etc.
- Provide a means of irradiation **testing of new materials variants** arising from:
  - Continuing development of improved compositions/microstructures
  - Application of advances in fabrication technologies (additive manufacturing, precision casting, joining technologies, etc).