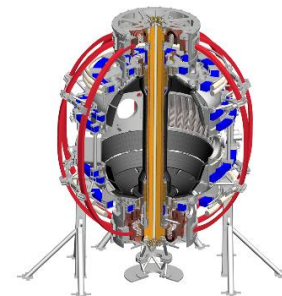


PFCR-WG Update

M.L. Reinke

*PFCR-WG Meeting
B-252
9/19/2018*



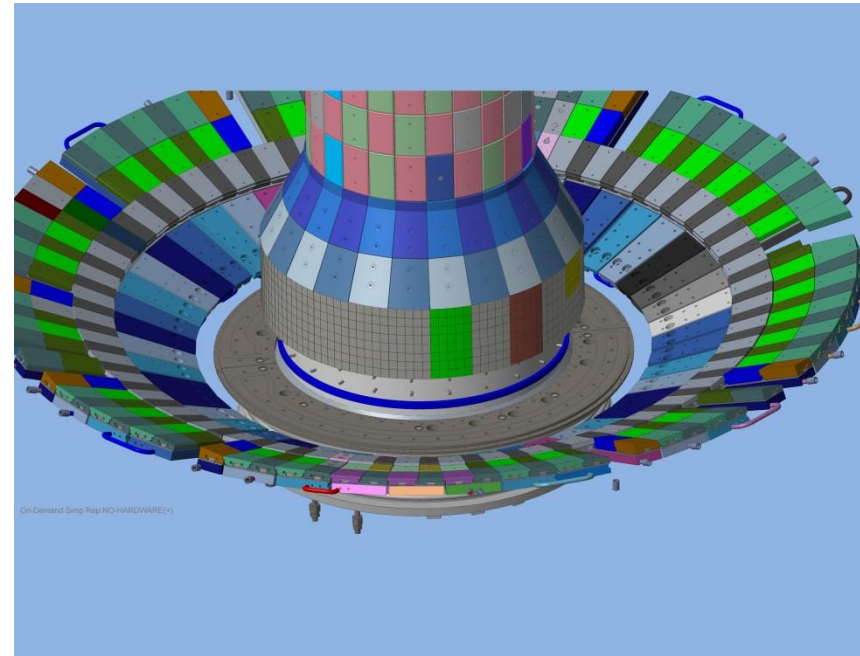
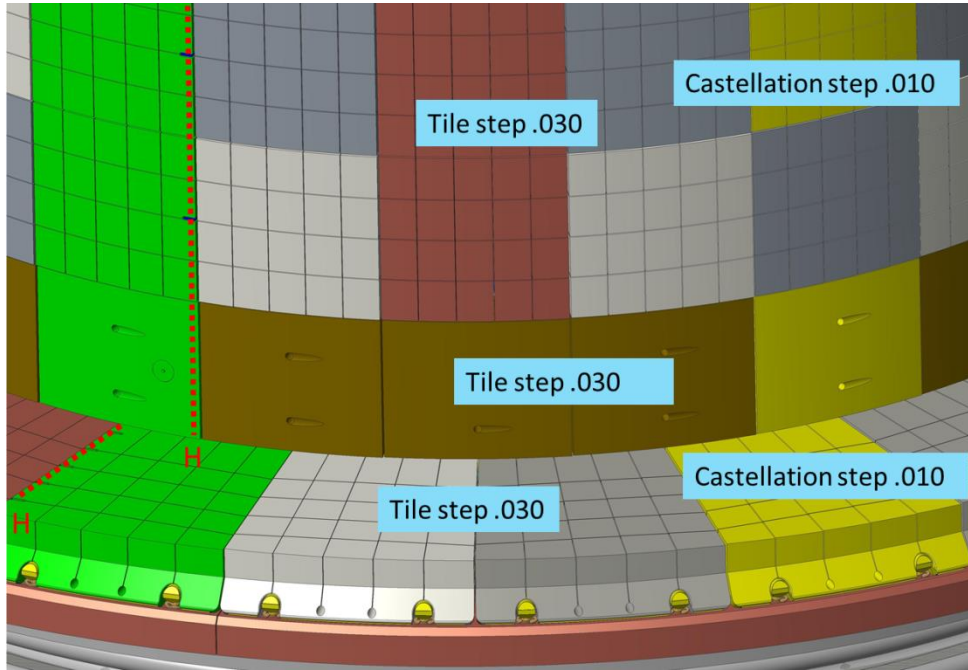
Goals of the Meeting

- update on the status of the PFC Engineering activities
- MEMO's remaining for FY18 (very early FY19)
- presentation on 3D Heat Flux from coil misalignments (S. Munaretto – GA)
- discuss status of R18-1 Milestone Work
 - T. Looby (UT-K): Heat Flux Model Validation Using Embedded Thermocouples
- discuss FY19 plans for Working Group

<http://nstx-u.pppl.gov/program/working-groups/pfc-requirements-working-group>

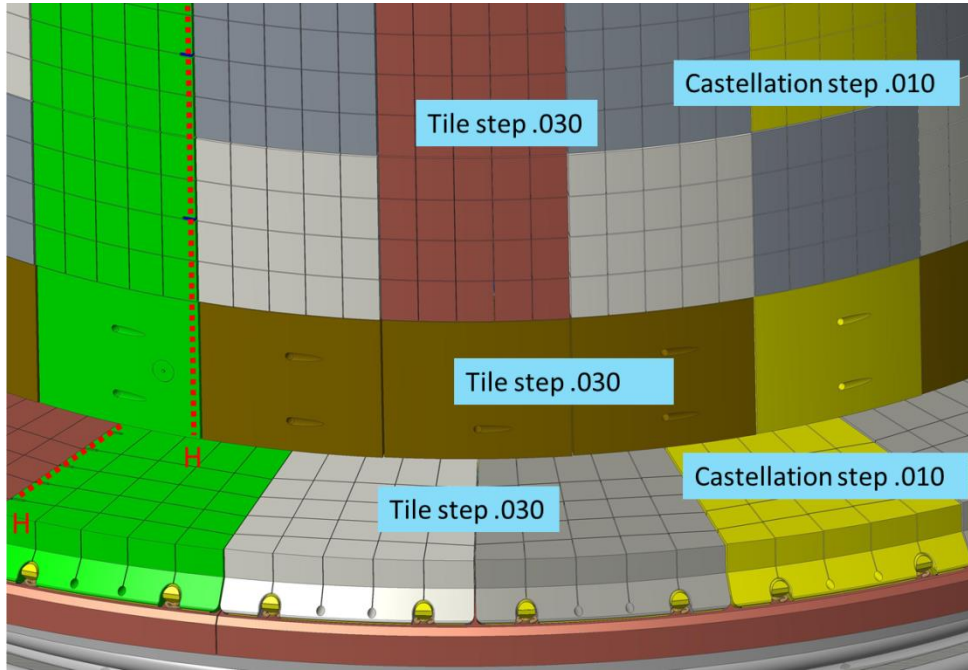
PFCs Moving to Final Design Review - 9/28

<https://sites.google.com/pppl.gov/20180926pfcs-pempfdr/home>



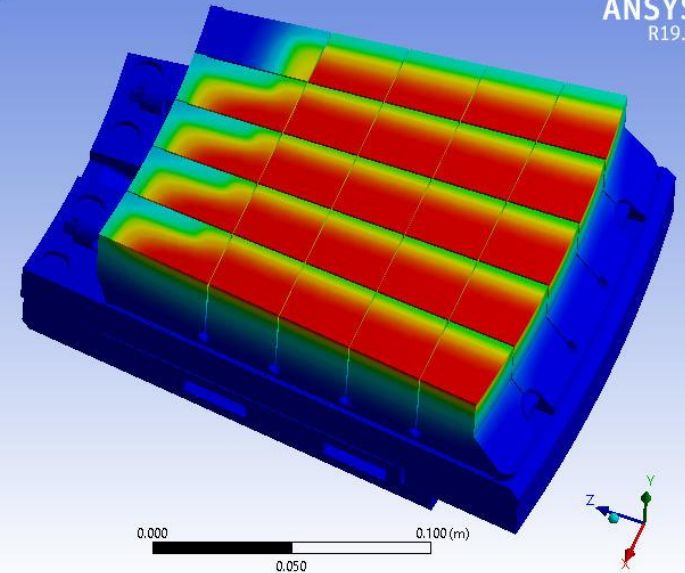
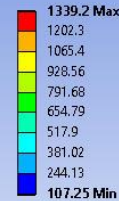
PFCs Moving to Final Design Review - 9/28

<https://sites.google.com/pppl.gov/20180926pfc-pempfd/home>



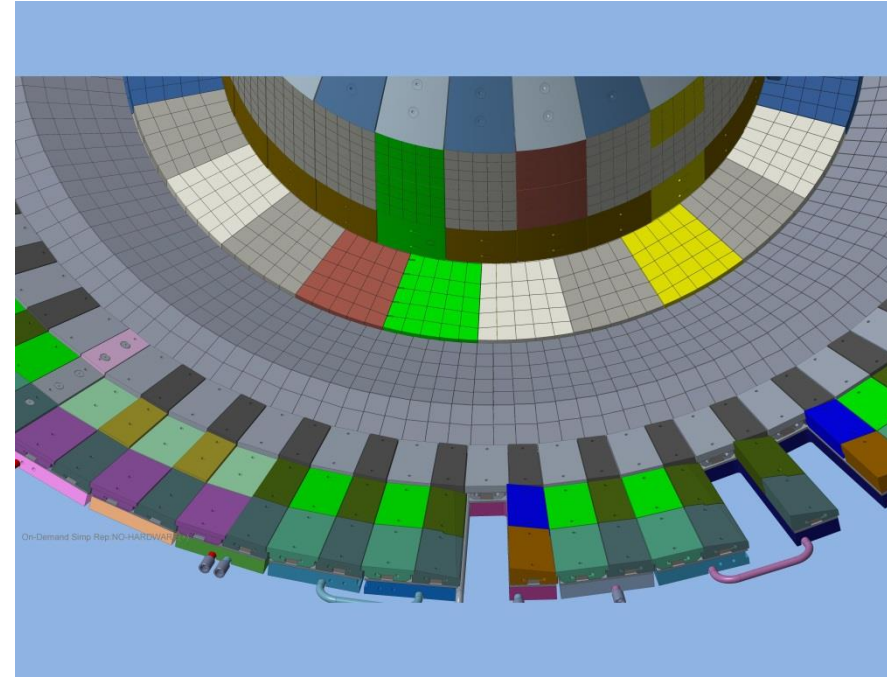
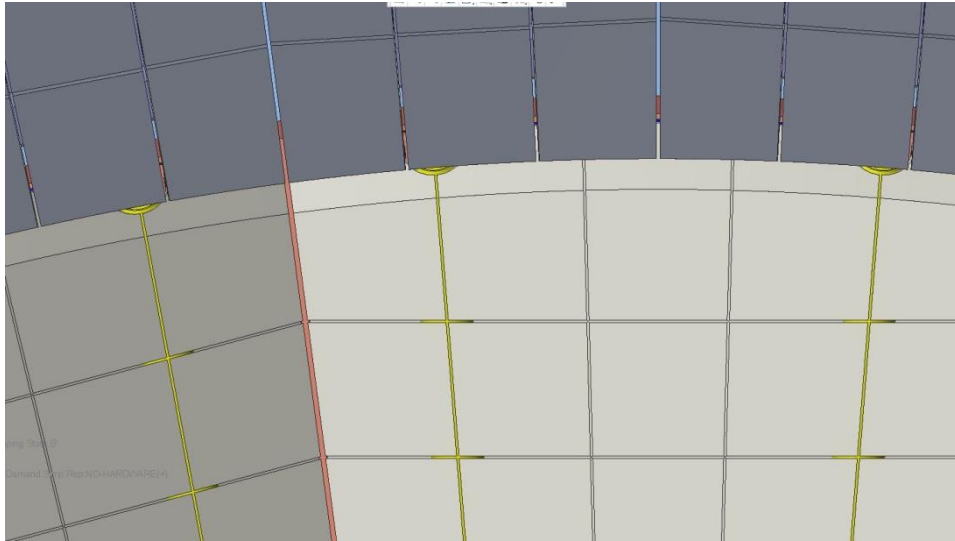
B: Transient Thermal

Temperature
Type: Temperature
Unit: °C
Time: 5
Custom Obsolete
9/9/2018 8:56 PM



PFCs Moving to Final Design Review - 9/28

<https://sites.google.com/pppl.gov/20180926pfc-pempfdr/home>



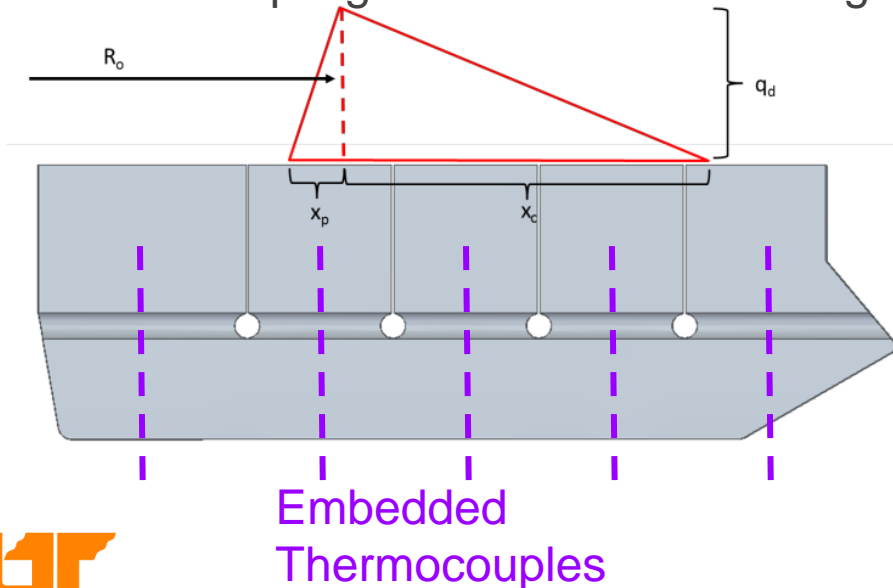
MEMO's to be Completed

- MEMO-007 (Reinke) on the W_PFC heat flux code
- MEMO-022 (Reinke) on the erosion/ablation calculations which fed requirements for shaping, summarized in R18-1 report
- MEMO-023 (Erickson) summary of image based heat flux control
- MEMO-024 (Reinke) final milestone summary, expanding on what was in the R18-1 report, matching to MEMO-014 on goals
- MEMO-025 (Looby) summary of NN work, basically his Master's thesis which is due in early FY19
- Others?

Sub-Surface Temperature Sensing

- UT-K (T. Looby) masters thesis project

Demonstrate how unknown heat flux model parameters can be derived with various sampling mechanisms within a given parameter space.



Simplified Eich Model:

$$x_p = S f_x$$

$$x_c = \lambda_q f_x$$

$$P_{heat} = \int_{R_o - x_p}^{R_o + x_c} q(R) 2\pi R dR$$

$$\frac{S}{\lambda_q} = C_1$$

$$\lambda_q [mm] = C_2 P_{heat}^{C_3} B_p^{C_4}$$

$$0.1 < C_1 < 0.3$$

$$1.0 < C_2 < 2.5$$

$$-0.1 < C_3 < 0.25$$

$$-1.2 < C_4 < -0.5$$

$$0.2 < B_p [T] < 0.6$$

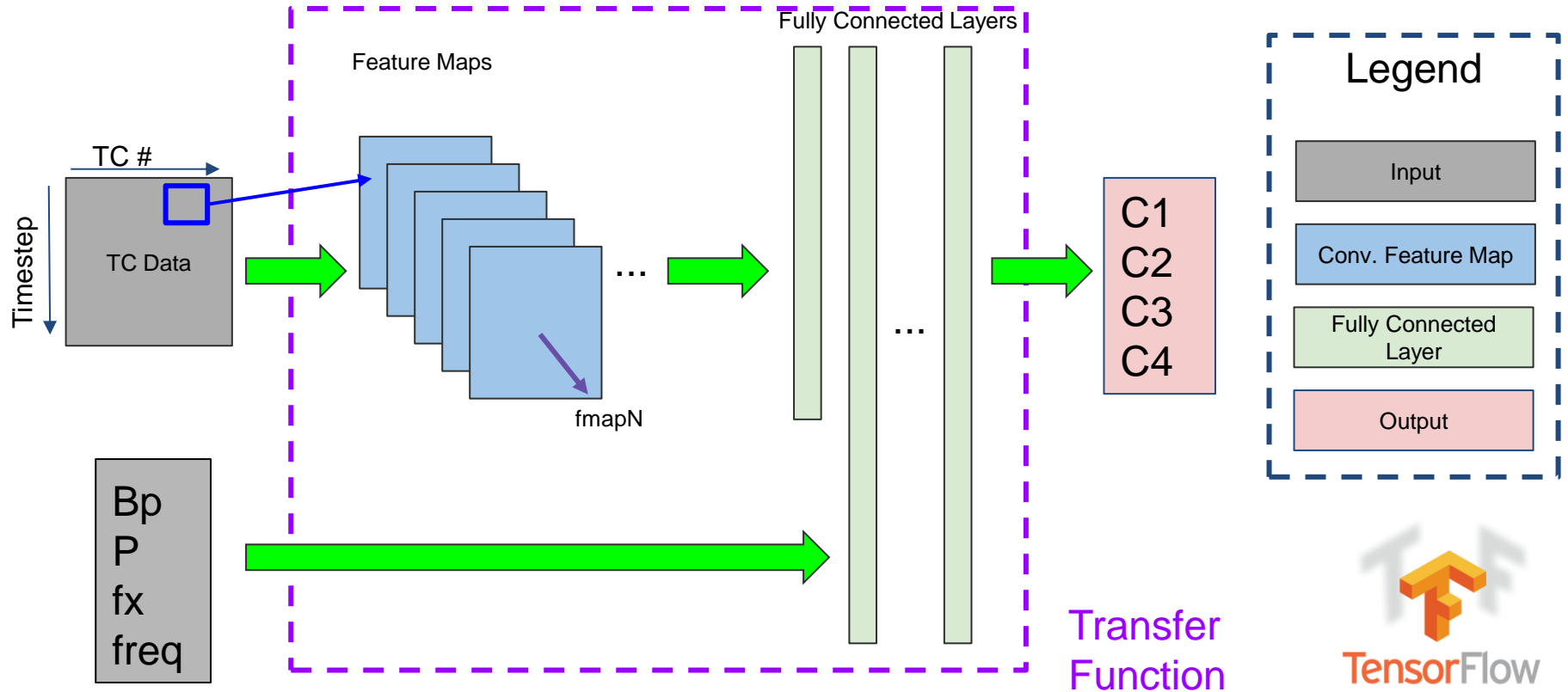
$$0.5 < P_{heat} [MW] < 4.9$$

$$4 < f_x < 30$$

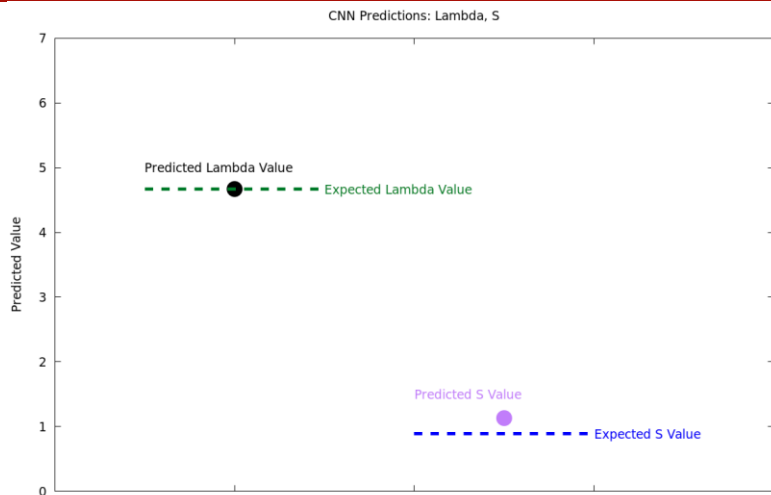
$$46.0 < R_o [cm] < 57.5$$

$$1 < \Delta t [sec] < 5$$

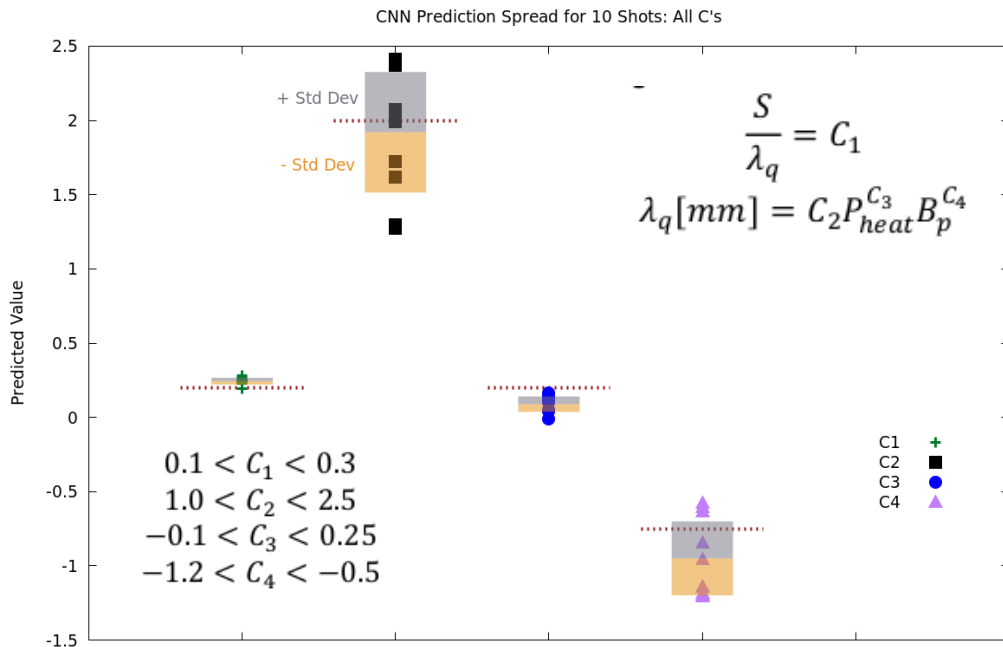
First Neural Network Attempts



'1-Shot' Analysis gives S , λ_q , Degeneracy for C_1 - C_4



- Possible λ Domain [mm]:
(1.0836, 25.493)
- Possible S Domain [mm]:
(0.10836, 7.6479)

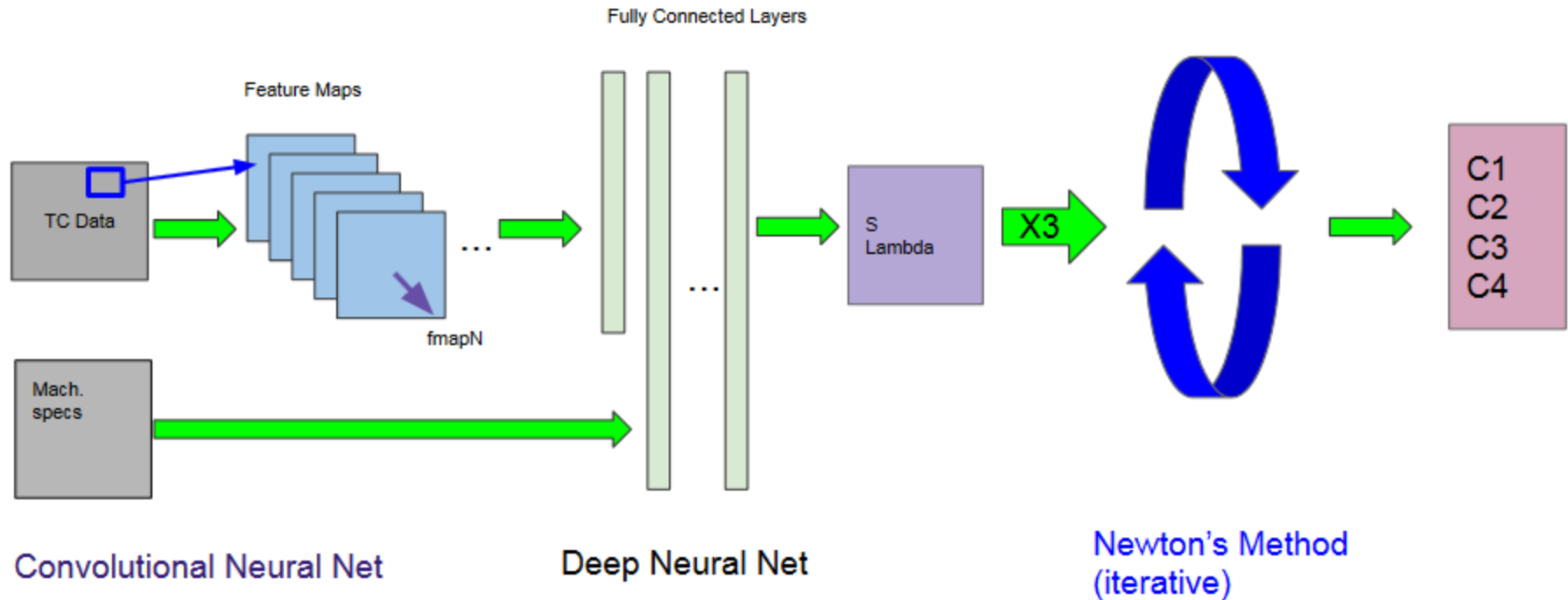


Result led us to explore using 'triplets' to break degeneracy

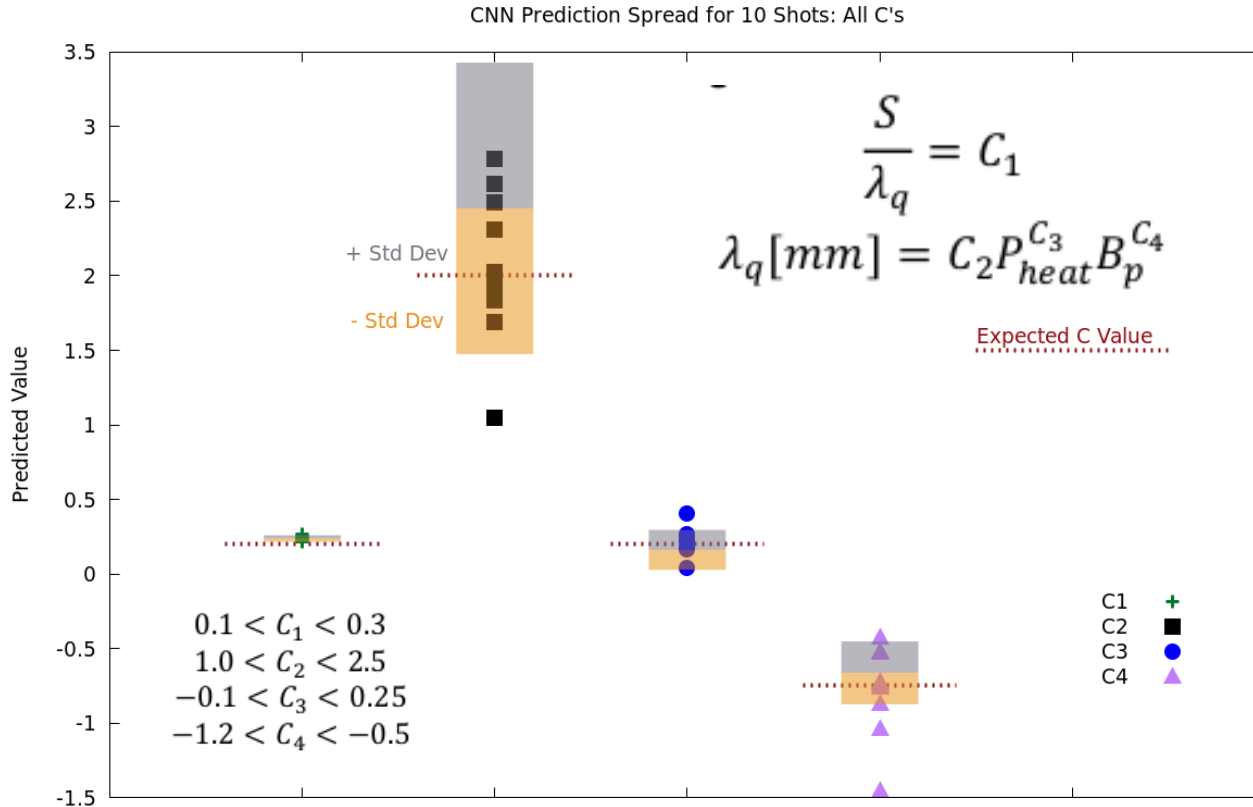
Problems with Triplet Method, Limits of Use for CNN

- method of training on ‘triplets’ of data to break degeneracy only using NN were problematic
 - Requires large dataset generation, long (few days) training
 - NN was trying to assign meaning to the ordering of triplet
- CNNs’ strength is in pattern recognition, object detection, and computer vision.
 - TC data is an excellent application for CNN pattern recognition.
- NNs are not the best for solving small (non)linear systems
 - e.g. solving system of equations for relating S, λ_q to eng. param.

New Hybrid Model for Solving for C_1 - C_4

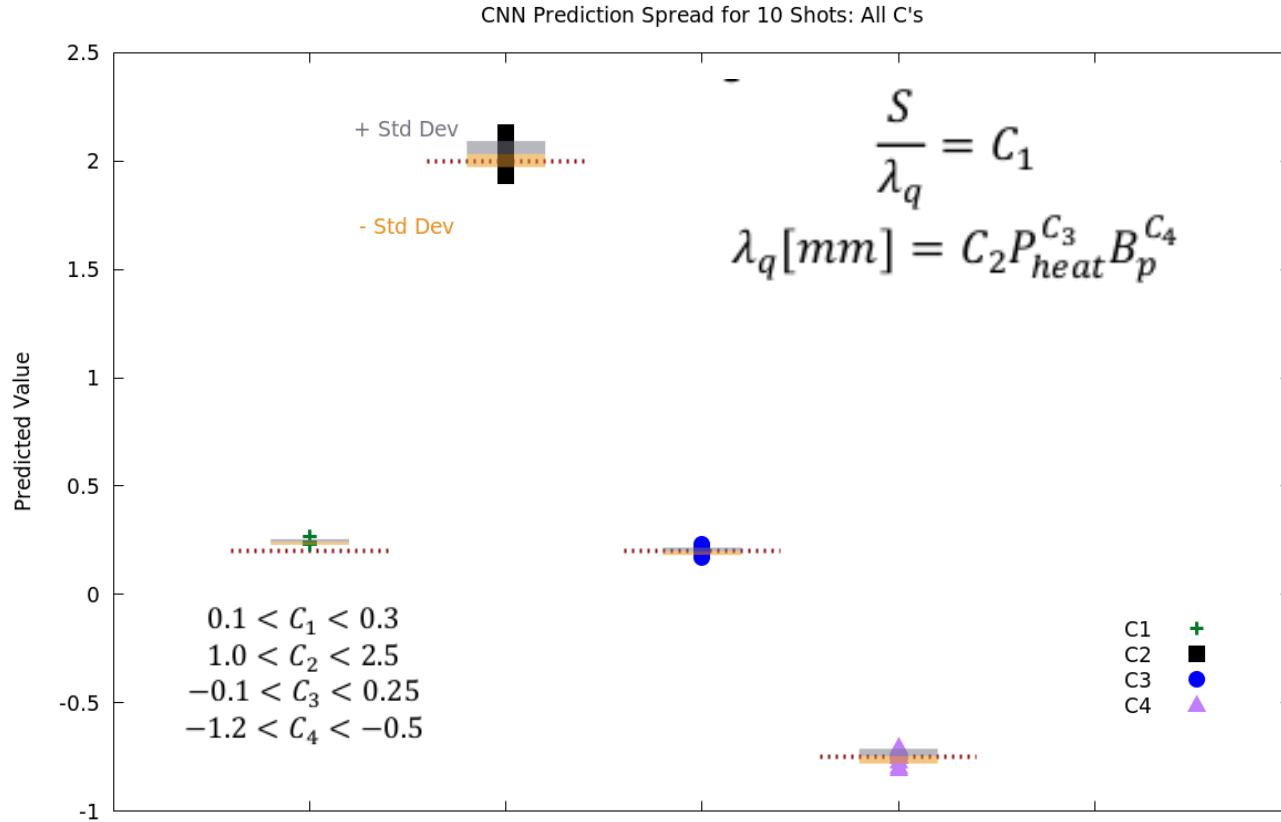


Method Works, But Requires Accurate Training



CNN training
99% accuracy for
 S, λ_q within 3%
(e.g. 99% of the
cases predict $S,$
 λ_q within 3%)

Method Works, But Requires Accurate Training

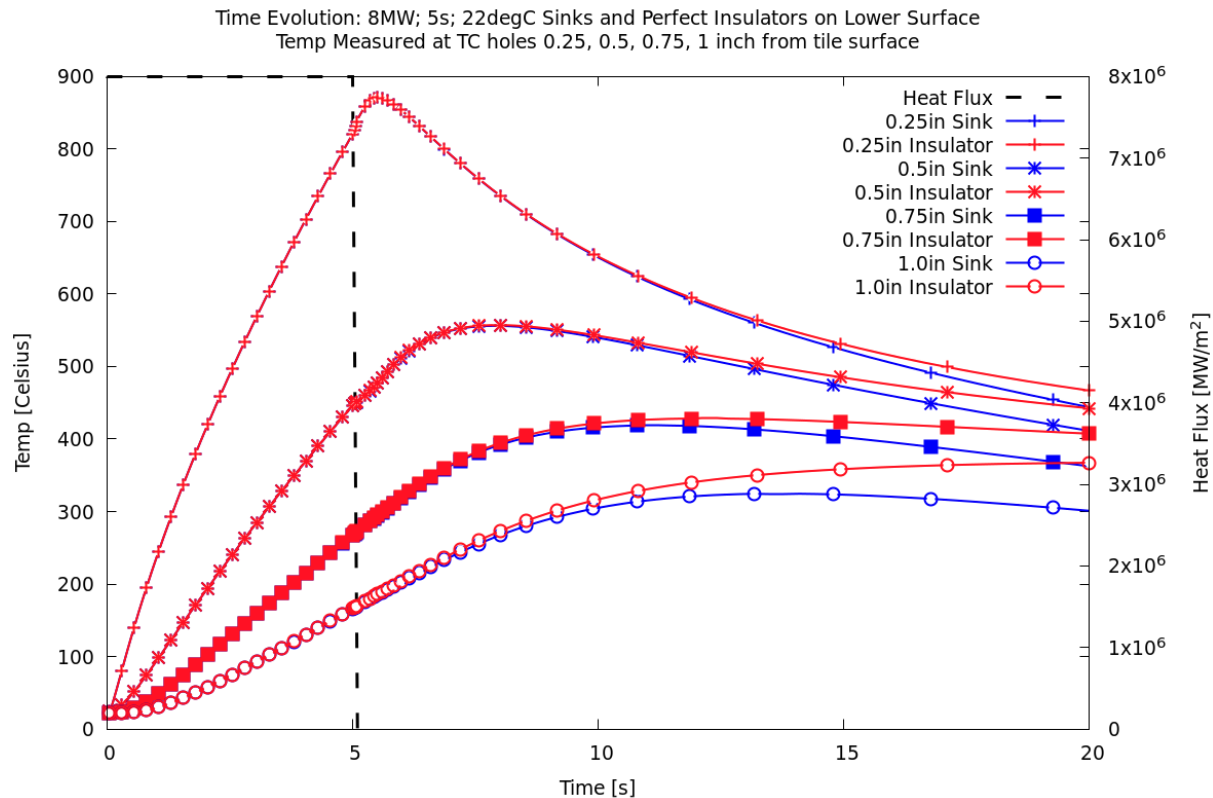


CNN training
93% accuracy for
 S , λ_q within 0.5%

***What happens to
this method when
systematic errors
are including?***

Exploring Possible Systematic Errors

- impact of offsets/problems with TCs?
- impact of model and it's back-end structure depends on desgin



Generic Solution for Power Law Scalings

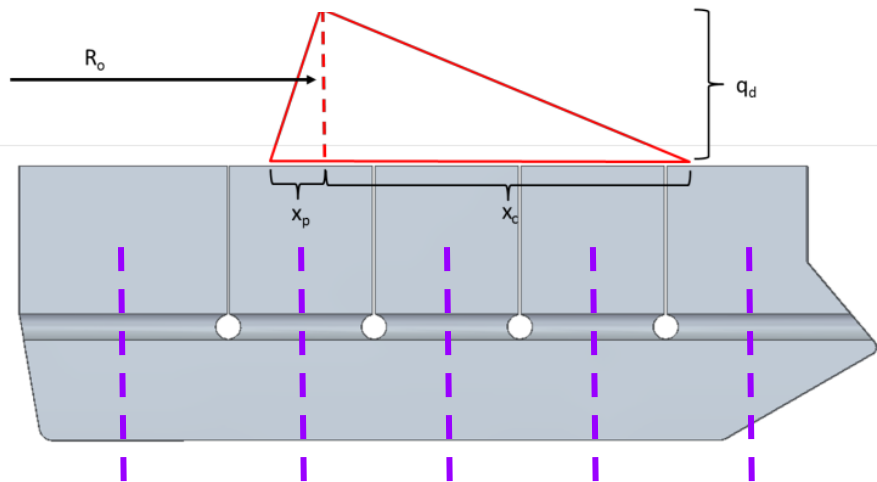
$$x_p = S f_x$$

$$x_c = \lambda_q f_x$$

$$P_{heat} = \int_{R_o - x_p}^{R_o + x_c} q(R) 2\pi R dR$$

$$\frac{S}{\lambda_q} = C_1$$

$$\lambda_q [mm] = C_2 P_{heat}^{C_3} B_p^{C_4}$$



Embedded
Thermocouples

$$x_p = C_1 C_2 P_h^{C_3} B_p^{C_4} f_x$$

$$x_c = C_2 P_h^{C_3} B_p^{C_4} f_x$$

Take 3 shots, A, B, C

$$C_1 = (x_p/x_c)_i$$

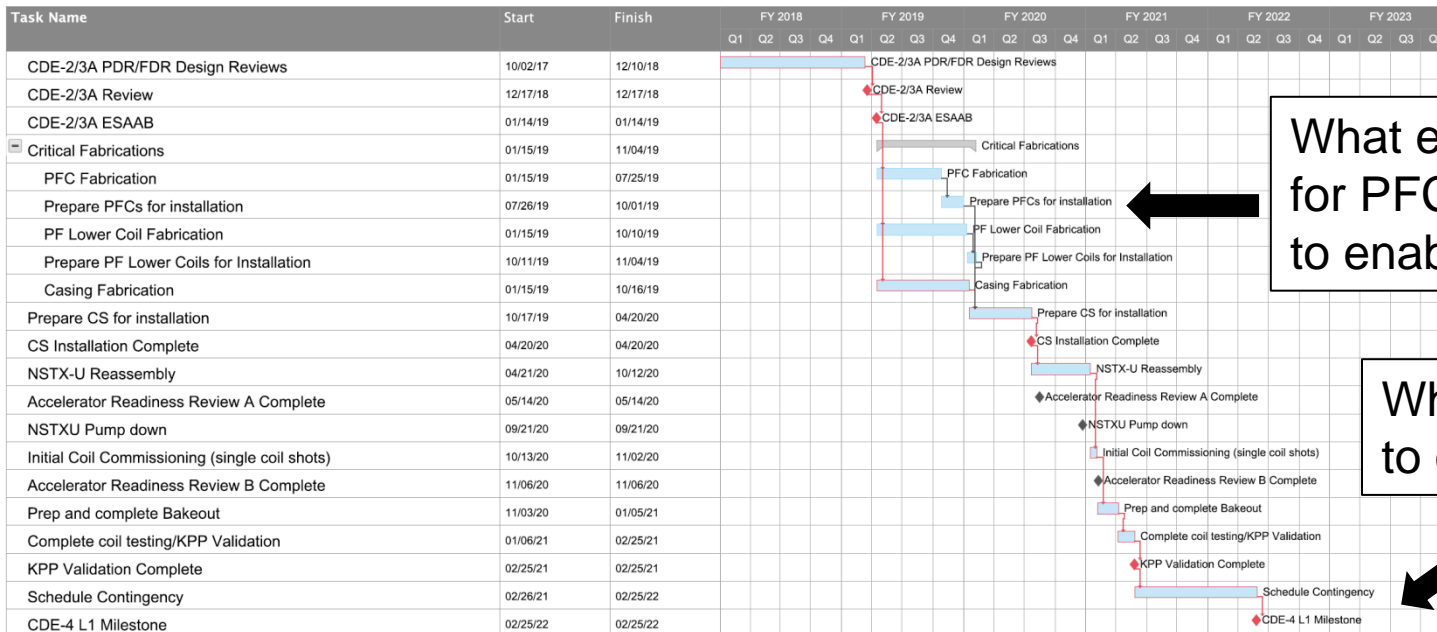
$$\ln(x_c/f_x) = \ln C_2 + C_3 \ln P_h + C_4 \ln B_p$$

$$\begin{bmatrix} \ln(x_c/f_x)_A \\ \ln(x_c/f_x)_B \\ \ln(x_c/f_x)_C \end{bmatrix} = \begin{bmatrix} 1 & \ln P_{h,A} & \ln B_{p,A} \\ 1 & \ln P_{h,B} & \ln B_{p,B} \\ 1 & \ln P_{h,C} & \ln B_{p,C} \end{bmatrix} \cdot \begin{bmatrix} \ln C_2 \\ C_3 \\ C_4 \end{bmatrix}$$

can extend to arbitrary number of engineering parameters, find LS soln.

Discussion: Focus New FY19 Work?

- post-FDR, is there a purpose to the WG prior to a ramp up to operations (some carryover of R18-1 work into FY19)



What else is needed to for PFCs prior installation to enable monitoring?

What is needed prior to operations?

Plans for FY19

- WG will be put on 'hiatus' barring any PPPL lead to continue working on scope
 - no new deputy assigned, unless there are 'takers'
 - Reinke remains as contact point in case Recovery needs input and needs to ramp back up a specific mission
- post PFC FDR, post CDE2/3a timeline and scope for PFCs and any monitoring will be clarified
 - will revisit WG as a vehicle to deliver the operations-related scope in the original charge in mid-FY19

R18-1 Executed Within the PFCR-WG

R(18-1): Develop and Benchmark Operations-Focused Reduced Heat Flux and Thermo-Mechanical Models for use in PFC Monitoring

The NSTX-U Recovery Project will deploy new plasma facing components (PFCs) to meet updated heat exhaust requirements driven by narrower scrape-off-layer widths, increased heating power, and longer pulse durations relative to NSTX. Inter-shot monitoring or intra-shot control of heat flux to PFCs is anticipated for a range NSTX-U operating space, necessitating reduced models that can be run between shots or even in real-time. Monitoring requires a reliable instrumentation suite which can support or contradict model predictions and confirm PFC integrity. The goals of this milestone are three-fold: (1) **Develop tools for pre-shot planning and confirmation of post-shot PFC thermal observations** which use reduced models to predict time-evolving heat fluxes to shaped PFCs and estimate distances from engineering limits. Assess additional effort needed for implementation of reduced models in PCS. (2) **Where feasible, benchmark reduced models against boundary physics** (e.g. SOLPS, UEDGE) and finite element analysis (e.g. ANSYS) tools, and validate using experimental data from relevant tokamaks and results from Facility Milestone F(18-1). (3) **Evaluate examples of discrete monitoring systems that are sufficient to capture the evolution of the PFCs relative to engineering limits. Compare the ability for different techniques** (e.g. thermocouples vs. imaging) and technologies (e.g. near vs. long-wave infrared cameras) to achieve NSTX-U PFC monitoring objectives.

- ~~1. define which (additional) parameters need to be specified in an updated requirements document for the NSTX-U PFCs~~
2. facilitate generation of updated requirements utilizing:
 - a) available reduced models, empirical scalings, boundary simulations
 - b) ultimately, a validated model for specifying heat loads to all plasma facing components for arbitrary NSTX-U scenarios
3. in preparation for operations, develop:
 - a) instrumentation plan for intra and inter-shot PFC monitoring
 - b) a reduced model for heat loading for pre-shot planning
 - c) guidance on how to best integrate monitoring with operations
 - d) control, diagnostic requirements for real-time heat-flux control
4. work closely with engineers and analysts to develop and implement requirements