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## TO: DISTRIBUTION

FROM: C NEUMEYER
SUBJECT: OUT OF PLANE LOADS ON TF FLAG

SOLFI was used to calculate the vertical field seen by the TF flags due to $\mathrm{OH}=24 \mathrm{kA}$, $\mathrm{PF} 1 \mathrm{~A}=15 \mathrm{kA}, \mathrm{PF} 1 \mathrm{~B}=20 \mathrm{kA}, \mathrm{PF} 2=20 \mathrm{kA}, \mathrm{PF} 3=20 \mathrm{kA}, \mathrm{PF} 5=20 \mathrm{kA}$, and the corresponding force with $\mathrm{ITF}=71.2 \mathrm{kA}$.

As a simplifying assumption, the field due to the PF coils in the opposite half plane was not included. Due to $1 / \mathrm{r}$ effects, this should be reasonable.

The fields and forces were calculated at four elevations, namely the inner edge of the inner tier flags, the outer edge of the inner tier flags, the inner edge of the outer tier flags, and the outer edge of the outer tier flags. These are referred to with suffixes 11, 12, 21, and 22 , respectively.

The following curve shows the field contribution of the various coils, and the total, at the inner edge of the inner tier flags (worst case).


The following curve shows the total vertical field at the four locations.


The following table gives the forces at $\mathrm{Bt}=6 \mathrm{kG}$.

| R | $\mathrm{R}^{\prime}$ | Component | F $\Phi 1$ | $\sum F \Phi 1$ | $\mathrm{~F} \Phi 2$ | $\sum \mathrm{~F} \Phi 2$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (inch) | (inch) |  | (lbf/in) | (lbf) | (lbf/in) | (lbf) |
| 3.8480 | 0.0000 | Flag | 334.5 | 0.0 | 192.3 | 0.0 |
| 4.8480 | 1.0000 | Flag | 327.5 | 331.0 | 190.8 | 191.6 |
| 5.8480 | 2.0000 | Flag | 319.6 | 654.6 | 189.0 | 381.5 |
| 6.8480 | 3.0000 | Flag | 311.0 | 969.9 | 187.0 | 569.5 |
| 7.8480 | 4.0000 | Flag | 302.1 | 1276.4 | 184.7 | 755.4 |
| 8.8480 | 5.0000 | Flag | 292.9 | 1573.9 | 182.2 | 938.8 |
| 9.8480 | 6.0000 | Flag | 283.8 | 1862.3 | 179.4 | 1119.6 |
| 10.8480 | 7.0000 | Flag | 274.9 | 2141.7 | 176.5 | 1297.6 |
| 11.8480 | 8.0000 | Flag | 266.3 | 2412.3 | 173.5 | 1472.6 |
| 12.8480 | 9.0000 | Flag | 257.9 | 2674.4 | 170.3 | 1644.6 |
| 13.8480 | 10.0000 | Flag | 249.9 | 2928.2 | 167.1 | 1813.3 |
| 14.8480 | 11.0000 | Flag | 242.1 | 3174.2 | 163.7 | 1978.6 |
| 15.8480 | 12.0000 | Link | 234.7 | 3412.7 | 160.3 | 2140.6 |
| 16.8480 | 13.0000 | Link | 227.6 | 3643.8 | 156.8 | 2299.2 |
| 17.8480 | 14.0000 | Link | 220.6 | 3867.9 | 153.2 | 2454.2 |
| 18.8480 | 15.0000 | Link | 213.9 | 4085.2 | 149.7 | 2605.6 |
| 19.8480 | 16.0000 | Link | 207.3 | 4295.8 | 146.0 | 2753.5 |
| 20.8480 | 17.0000 | Link | 200.8 | 4499.8 | 142.4 | 2897.7 |
| 21.8480 | 18.0000 | Link | 194.4 | 4697.5 | 138.7 | 3038.3 |
| 22.8480 | 19.0000 | Link | 188.0 | 4888.7 | 135.1 | 3175.2 |


| 23.8480 | 20.0000 | Link | 181.7 | 5073.5 | 131.4 | 3308.4 |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| 24.8480 | 21.0000 | Link | 175.3 | 5252.0 | 127.7 | 3438.0 |
| 25.8480 | 22.0000 | Link | 168.9 | 5424.1 | 124.1 | 3563.9 |
| 26.8480 | 23.0000 | Link | 162.5 | 5589.8 | 120.4 | 3686.2 |
| 27.8480 | 24.0000 | Link | 156.1 | 5749.1 | 116.8 | 3804.8 |
| 28.8480 | 25.0000 | Outer Leg | 149.6 | 5901.9 | 113.2 | 3919.8 |
| 29.8480 | 26.0000 | Outer Leg | 143.3 | 6048.4 | 109.6 | 4031.2 |
| 30.8480 | 27.0000 | Outer Leg | 137.0 | 6188.5 | 106.1 | 4139.1 |
| 31.8480 | 28.0000 | Outer Leg | 130.8 | 6322.4 | 102.6 | 4243.5 |

The calculated fields are in general agreement with the results from HM Fan's original ANSYS model, but it is difficult to check because only the color plots are available from the ANSYS runs. HM is not able to re-run his code from the earlier ANSYS version. It is noted that HM only included the effects from OH and PF1A; the outer PF's were omitted.

A cross check was performed using another field solver for one of the field calculations (PF2) and good agreement was found.

Connection scheme from end of flag to outer leg is complex. There is one style of connector associated with the inner layer and two styles associated with the outer layer. Bottom and top of machine are identical. The following figures depict typical connection paths.



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