

Shot Analysis of Electron Transport in NSTX

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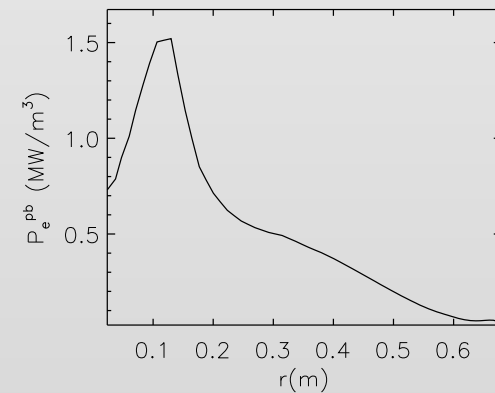
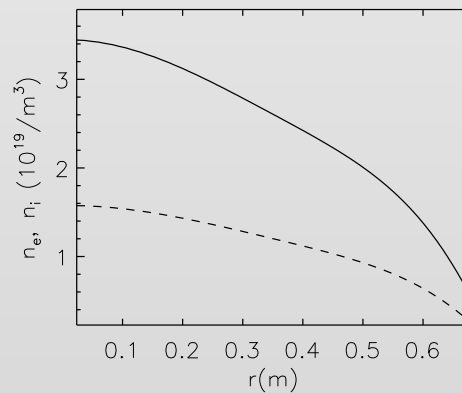
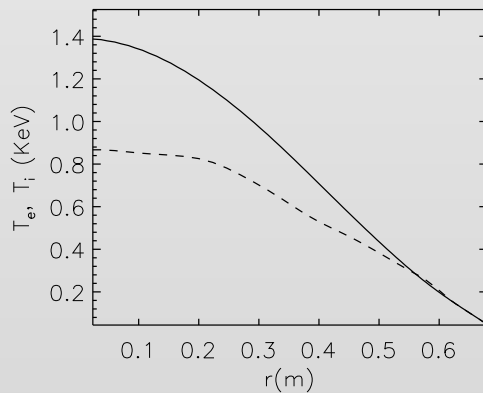
Overview

- NSTX 106194 Data Specification
- Power Balance Analysis
- Comparison of Power Balance with ETG and TEM
- ETG Model analysis and Nonlinear Simulation Result

Data Specification

NSTX 106194

- $R = 0.85$ m, $r = 0.68$ m and $B_0 \sim 0.45$ T, deuterium plasmas
- $\rho_e(0) = 0.2$ mm, $\rho_s(0) = 1.7$ cm and $d_e(0) = c/\omega_{pe} = 0.9$ mm at the core
- High Harmonic Fast Wave(HHFW) $P_e^{\text{total}} = 2.4$ MW
- $\epsilon_n = L_{ne}/R$ ranges from 0.2 ($r = 0.6$ m) to 2.1 ($r = 0.1$ m)
- $\eta_e = L_{ne}/L_{Te} \geq 1.5$ and reach the maximum $\eta_e = 2.5$ at $r = 0.43$ m.



Power Balance Analysis

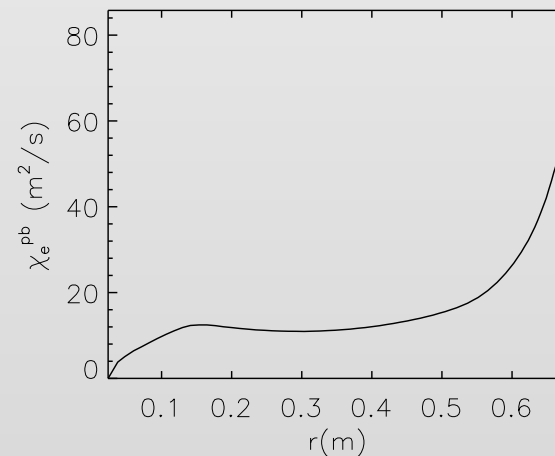
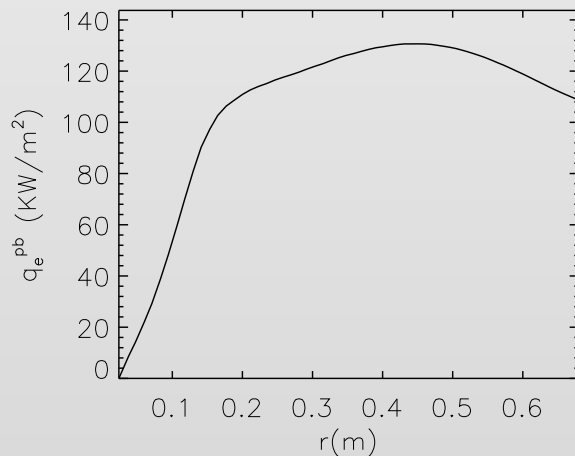
The heat flux, q_e , is from $\nabla q_e = P_e$

$$q_e(r) = \frac{1}{r} \int_0^r r' P_e(r') dr' \quad (1)$$

and the heat diffusivity is

$$\chi_e^{pb} = \frac{-q_e}{n_e \nabla T_e} \quad (2)$$

Energy confinement time $\tau_E = a^2 / \chi_e^{pb} = 40$ ms,



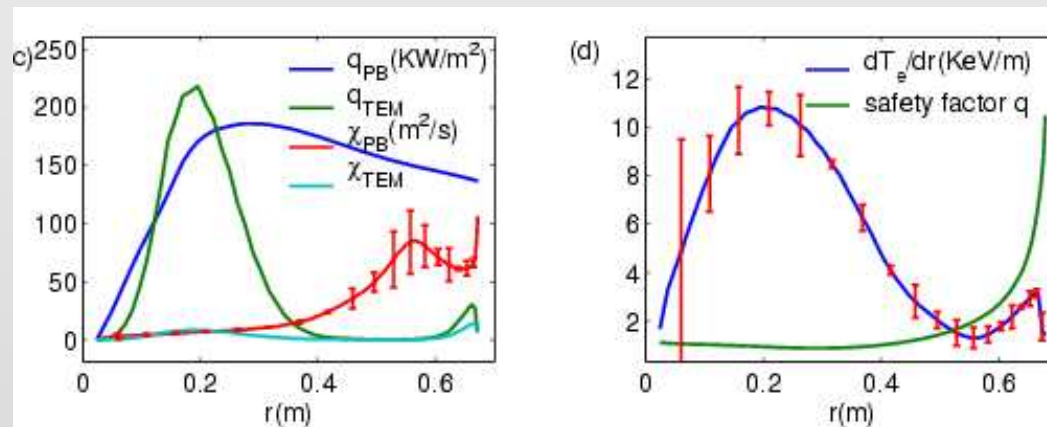
Trapped Electron Mode(TEM)

In the low-aspect ratio R/a like NSTX, there are the large pitch angle electrons with density fraction $\delta n_t = n_0 \delta$, where $\delta = (B_{\max}/B_{\min})^{1/2} - 1 \approx (2r/R)^{1/2}$ near the axis.

The particle and heat diffusivities are given by Kadomtsev and Pogutse(1970)

$$D_t = c_{TEM} D_{gB} \left(\frac{c_s R}{\nu_e L_n^2} \right) \quad (3)$$

$$\chi_e^{TEM} = \frac{3}{2} D_t \left(\frac{R}{L_{Te}} \right). \quad (4)$$



From Horton et. al. Nuclear Fusion 2005

Electron Temperature Gradient(ETG)

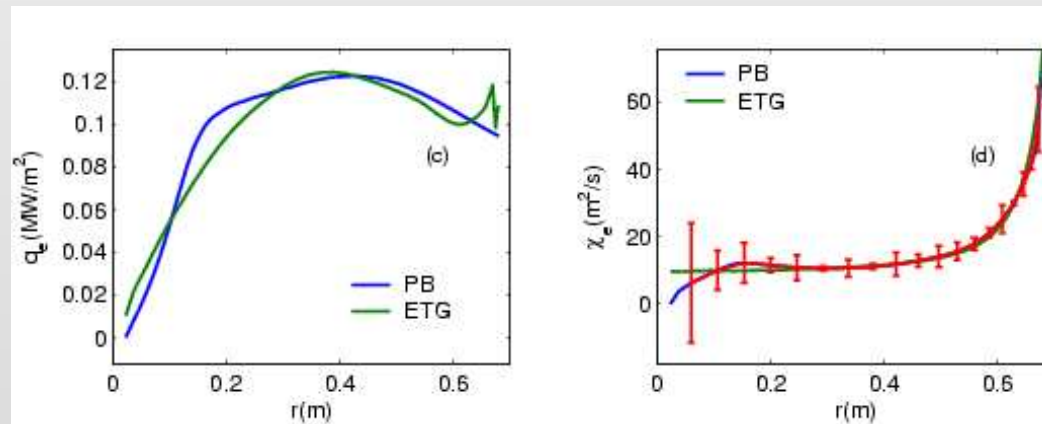
For ETG mode,

$$q_e = C_e^{em} n_e T_e q \frac{c^2}{\omega_{pe}^2} \frac{v_e}{R} \left(\frac{R}{L_{Te}} - \frac{R}{L_c} \right) \quad \beta_e > \beta_{e,cr} \quad (5)$$

$$q_e = C_e^{es} n_e T_e q^2 \left(\frac{\rho_e^2 v_e}{L_{Te}^2} \right) \left(\frac{R}{L_{Te}} - \frac{R}{L_c} \right) \quad \beta_e < \beta_{e,cr} \quad (6)$$

where $\beta_{e,cr} = (L_{Te}/qR)^2$ ETG mode is electromagnetic,

$\beta_e > \beta_{e,cr}$ where $r > 0.32$ m



From Horton et. al. Nuclear Fusion 2005

Critical Temperature Gradient

Generally, the heat flux is defined by

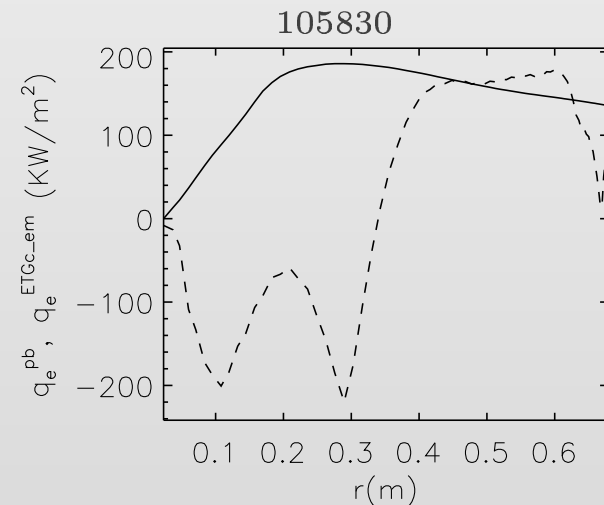
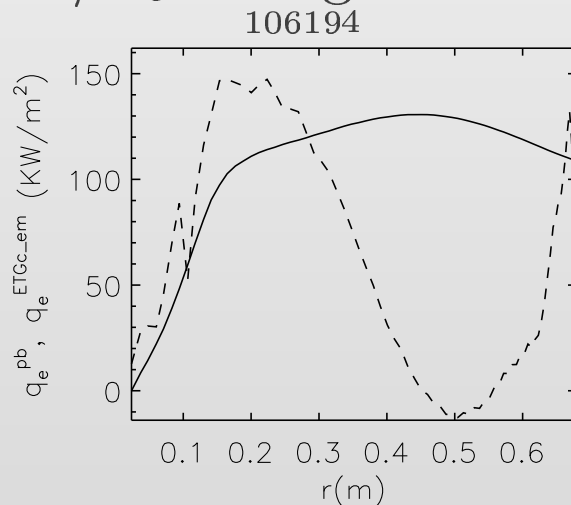
$$q_e = -n_e \chi_e [(\nabla T_e) - (\nabla T_e)_c] \quad (7)$$

where (from Horton et. al. NF 2005)

$$R/L_c = 5(\pm 1) + 10(\pm 2)|s|/q \quad (\text{TH})$$

$$R/L_c = 1.9(|s|/q)(1 + Z_{\text{eff}} T_e/T_i) \quad (\text{EX} - \text{ToreSupra})$$

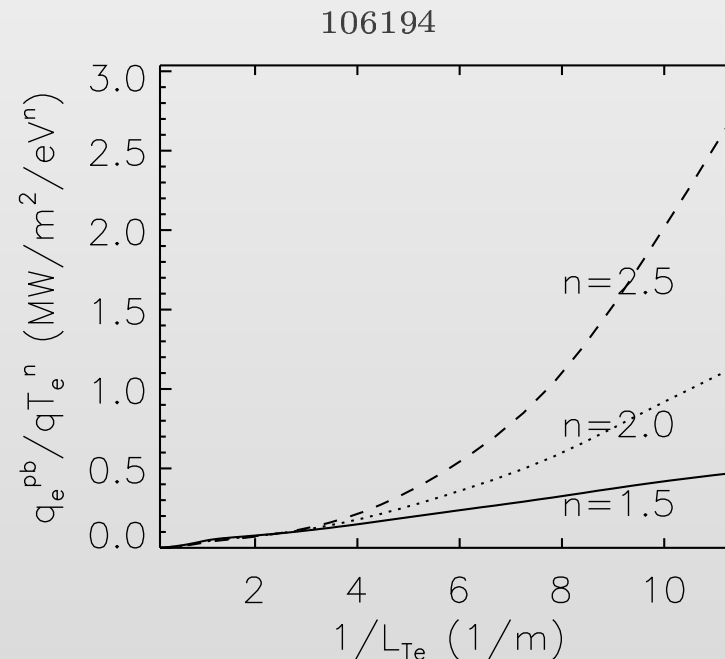
Both R/L_c s disagree with power balance heat flux.



Temperature Dependence

The scaling law shows that heat flux is proportional to

- ETG EM $\sim T_e^{3/2}$
- Bohm $\sim T_e^2$
- gyro-Bohm $\sim T_e^{5/2}$
- ETG ES $\sim T_e^{5/2}$



ETG Model

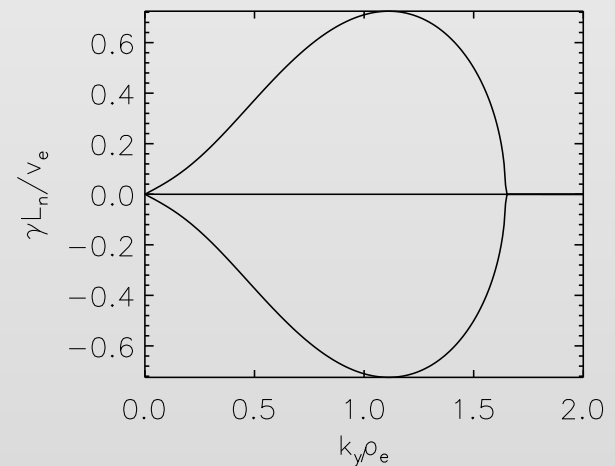
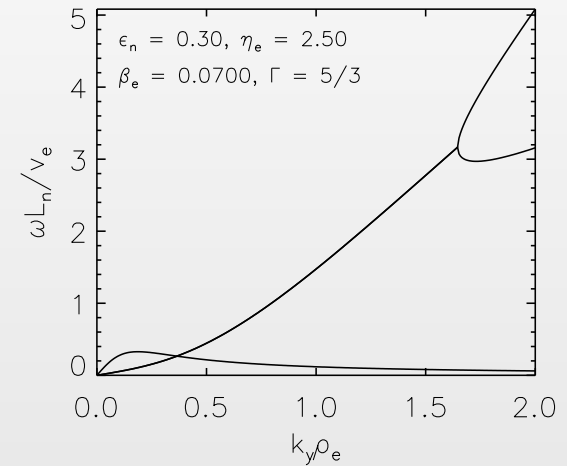
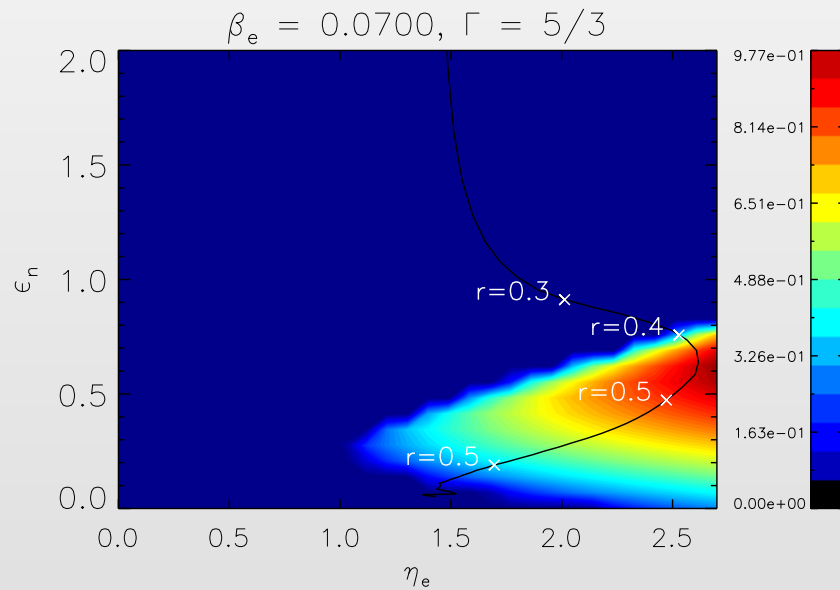
The non-dimensional ETG three-field model is derived by Horton (NF, 2005) in the locally toroidal geometry,

$$\begin{aligned}
 (1 - \nabla_{\perp}^2) \frac{\partial \hat{\phi}}{\partial t} &= [1 - 2\epsilon_n + (1 + \eta_e)\nabla_{\perp}^2] \frac{\partial \hat{\phi}}{\partial y} + 2\epsilon_n \frac{\partial \delta \hat{T}_e}{\partial y} \\
 &\quad + [\hat{\phi}, \nabla^2 \hat{\phi}] + \partial_{\parallel}^{nl} \nabla_{\perp}^2 \hat{A} - \mu \nabla^4 \hat{\phi} \\
 \left(\nabla^2 - \frac{\beta}{2} \right) \frac{\partial \hat{A}}{\partial t} &= \frac{\beta}{2} (1 + \eta_e) \frac{\partial \hat{A}}{\partial y} + 2\partial_{\parallel}^{nl} \hat{\phi} - \partial_{\parallel}^{nl} \delta \hat{T}_e - [\hat{\phi}, \nabla^2 \hat{A}] - \frac{\eta}{\mu_0} \nabla^2 \hat{A} \\
 \frac{\partial \delta \hat{T}_e}{\partial t} &= S_{\text{rf}}(r) - s_{\text{edge}}(r) - [\eta_e - 4\epsilon_n(\Gamma - 1)] \frac{\partial \hat{\phi}}{\partial y} - 2\epsilon_n(2\Gamma - 1) \frac{\partial \delta \hat{T}_e}{\partial y} \\
 &\quad - (\Gamma - 1) \partial_{\parallel}^{nl} \nabla^2 \hat{A} - [\hat{\phi}, \delta \hat{T}_e] + \chi_{\perp} \nabla_{\perp}^2 \delta \hat{T}_e + \chi_{\parallel} \left(\partial_{\parallel}^{nl} \right)^2 \delta \hat{T}_e
 \end{aligned}$$

where $T_e/T_i = 1.0$ is assumed and $(x, y)/\rho_e \rightarrow (x, y)$,
 $tv_e/L_n \rightarrow t$.

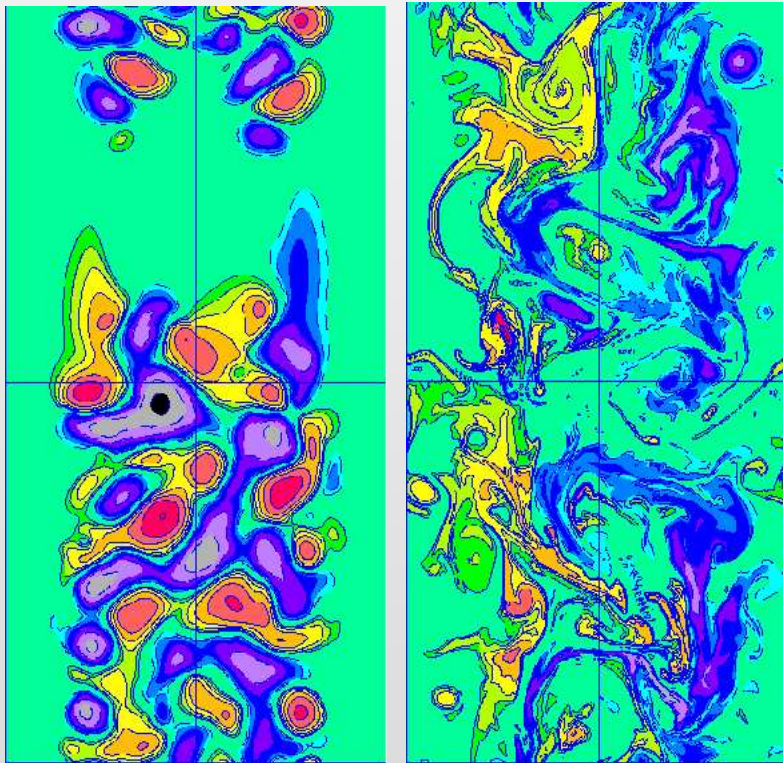
Linear Analysis

$k_y \rho_e \sim 1$ mode has the maximum growth rate even at $\beta_e > \beta_{e,cr}$.
Mainly the electrostatic modes are destabilized.



Nonlinear Simulation

Using the pseudospectral method, the set of the electrostatic equations are solved with the source and sink at $x = \pm L_x/4$ for $\epsilon_n = 0.2$ and $\eta_e = 2.0$. The box size is $[120\rho_e, 240\rho_e]$.



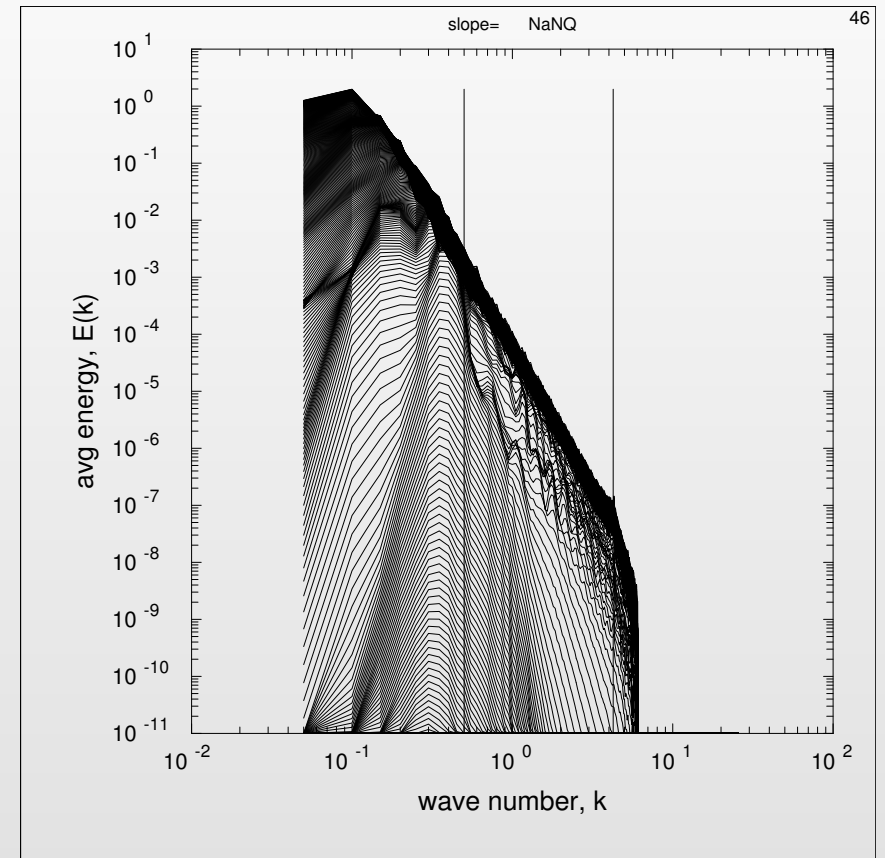
Inverse Cascade

- The most energies are pumped into $k_y \rho_e \sim 0.7$.
- During the turbulence, the energies are transferred to the lower $k_y \rho_e \sim 0.1$.
- The correlation length

$$l_c \sim 10.0 \rho_e$$

agrees with

$$d_e = \sqrt{\beta_e \rho_e} \sim 5 \rho_e .$$

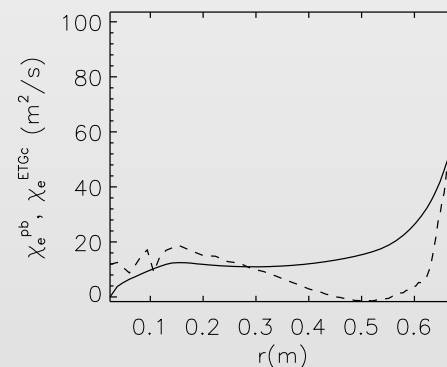
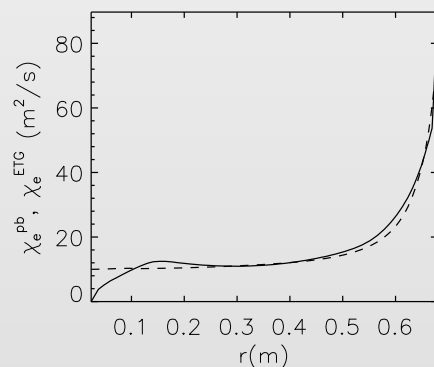
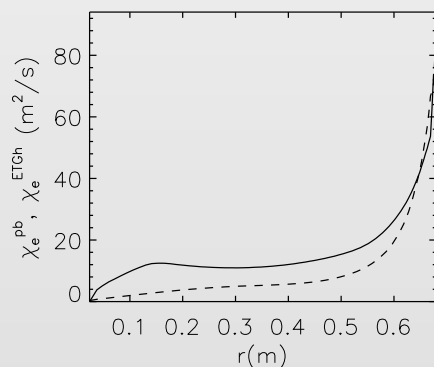
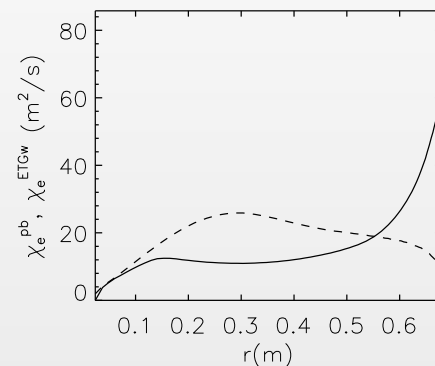
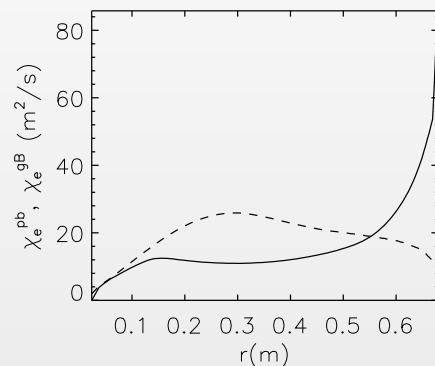
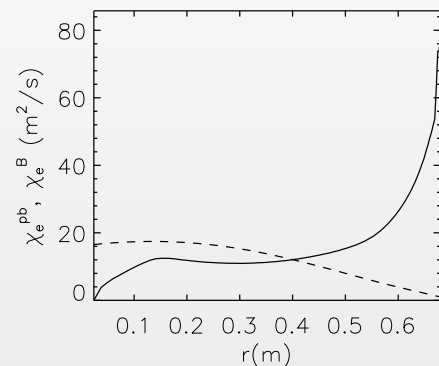


Conclusion

- The electron heat transport in NSTX shot 106194 can be explained by the electromagnetic electron temperature gradient(ETG) mode.
- We couldn't find the evidence of critical temperature gradient.
- The linear analysis indicates that the electromagnetic ETG mode are unstable outside $r = 0.4$ m and the modes with the strongest growth rate are electrostatic.
- The inverse cascade leads the ETG turbulence to the electromagnetic perturbation.
- Now we include microtearing mode with current gradients.

NSTX 106194

Using Least-Square Method, the coefficients are obtained.



NSTX 105830

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