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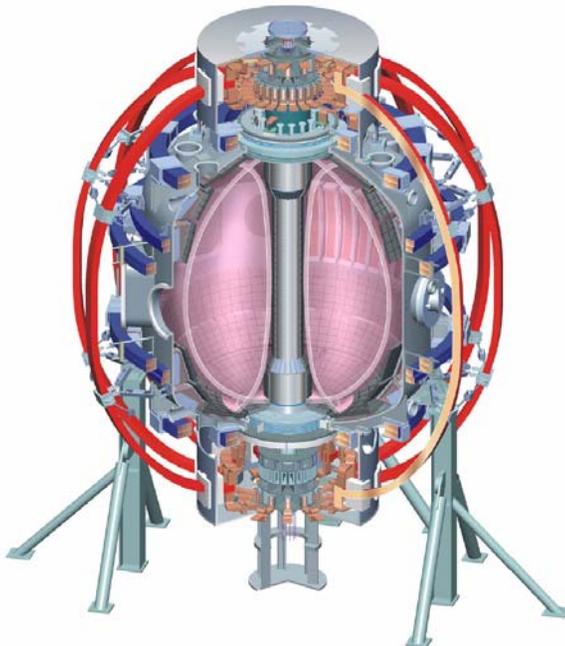
NSTX error field results (and needed modeling capabilities)

J. Menard

MHD SFG Meeting

April 19, 2006

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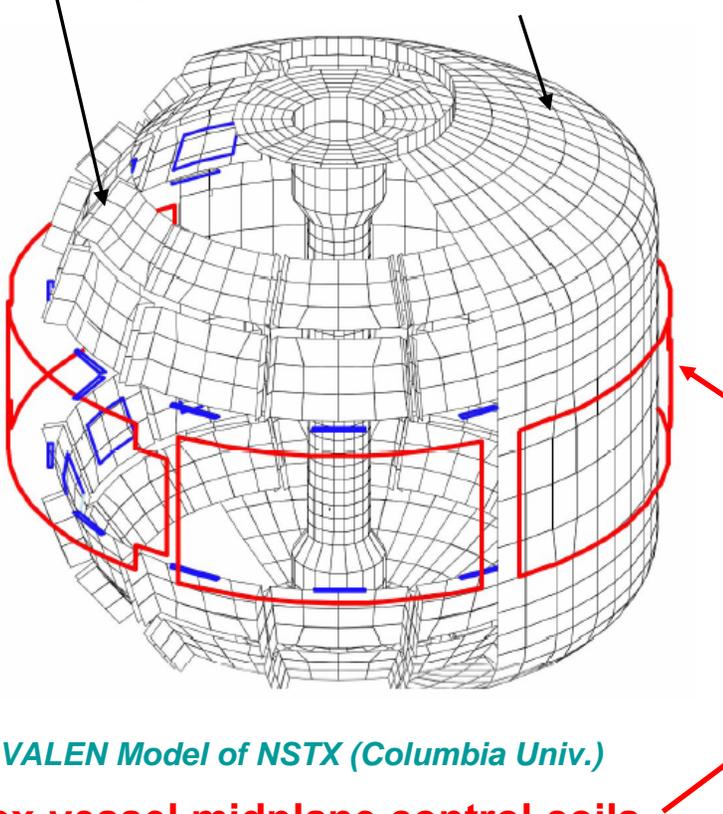
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6 non-axisymmetric RWM/EF coils and 3 switching power amplifiers (SPA) used in experiments



Copper passive conductor plates

SS Vacuum Vessel

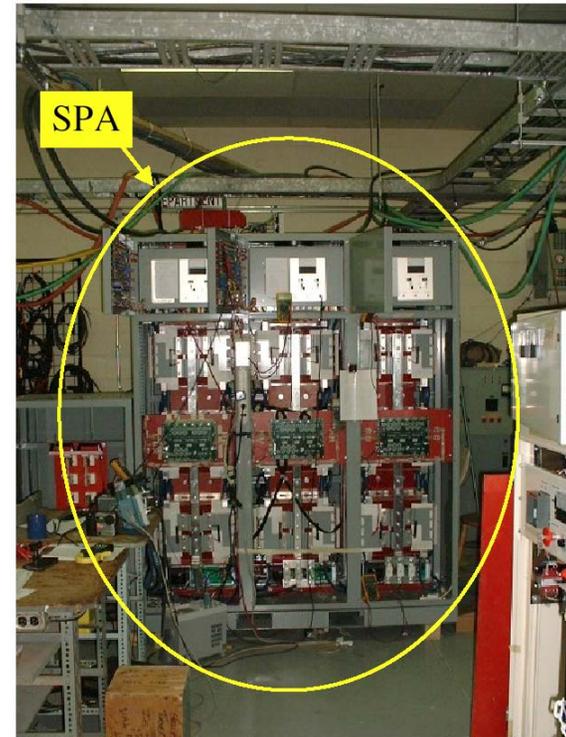


VALEN Model of NSTX (Columbia Univ.)

6 ex-vessel midplane control coils
+ 24 B_R and 24 B_P in-vessel sensors

NSTX RWM/EF coil and SPA capabilities:

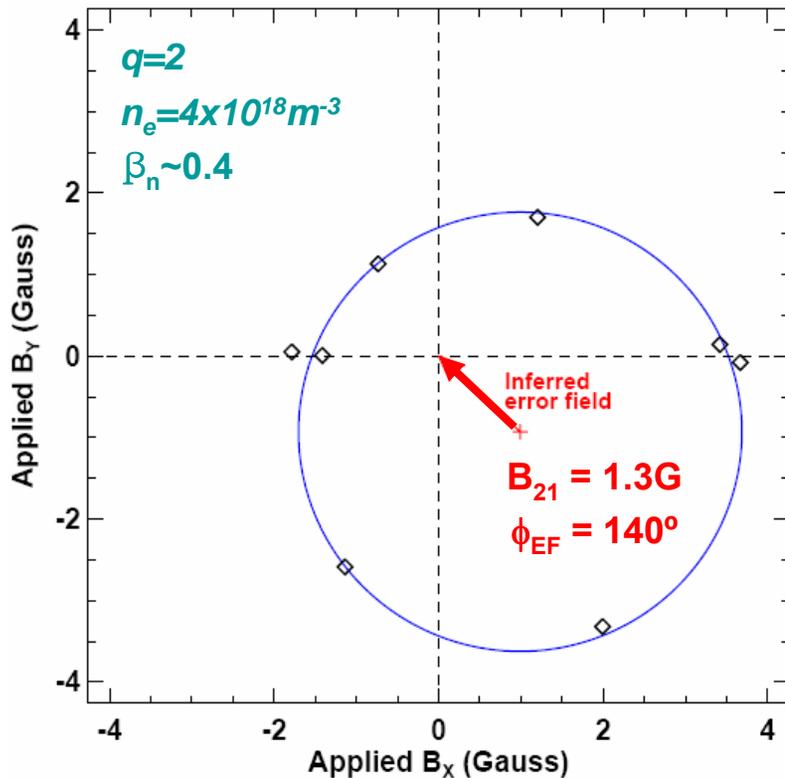
- 3 opposing coil pairs in anti-series (n=1, 3)
 - n=2 interconnection also possible
- 3 independent SPA circuits – 3.3kA, 7.5kHz
- Can produce 10-15G n=1 resonant B_{\perp} at q=2
- EF correction, magnetic braking, feedback



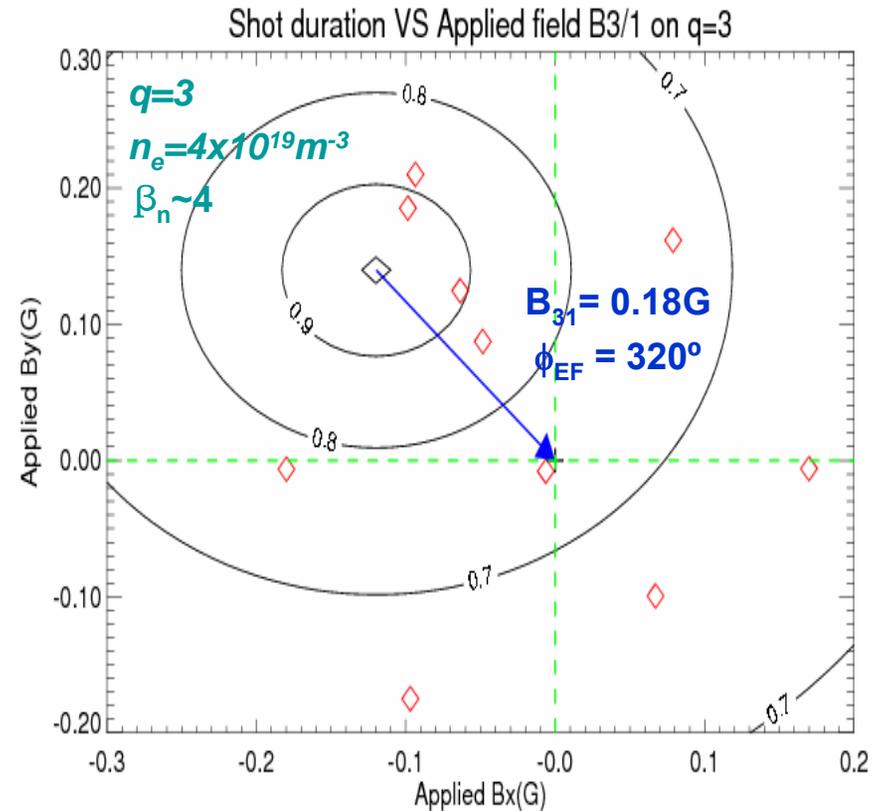
Error-field inferred from high- β experiments has direction **opposite** to that obtained at low n_e & β



Inferred 2/1 EF at Low- β

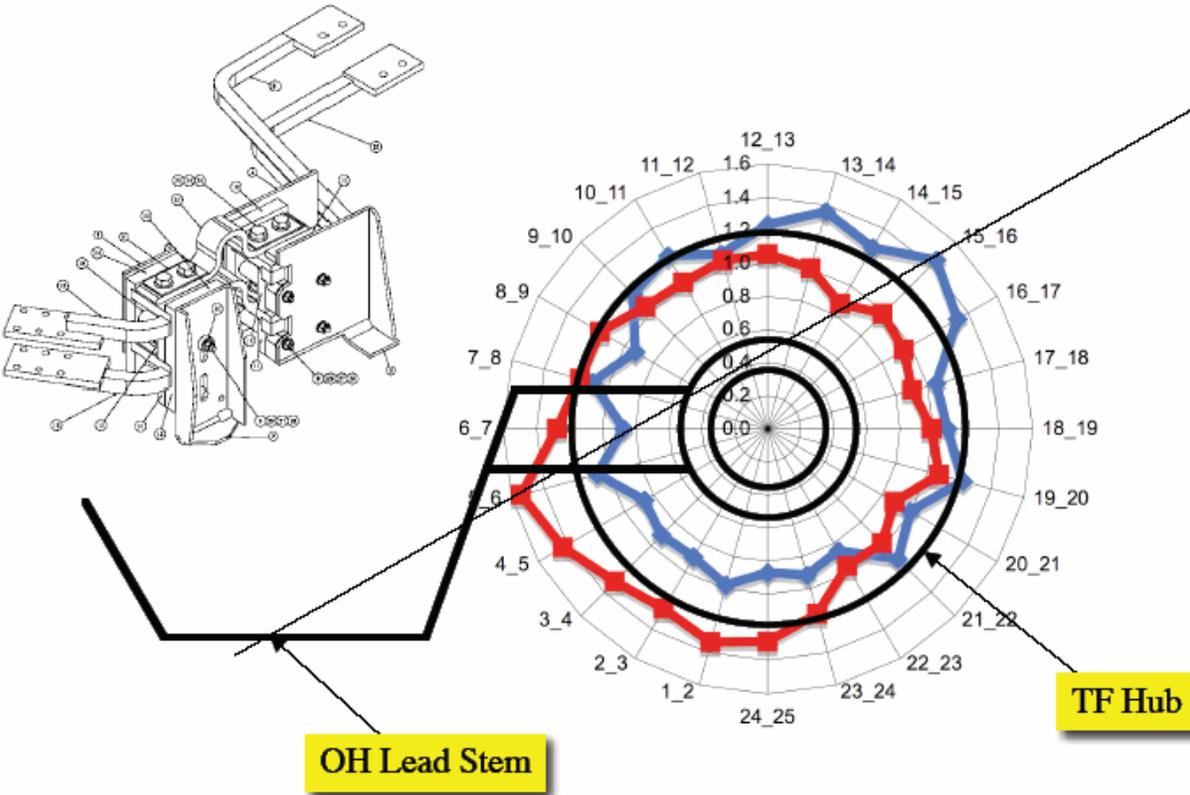


Inferred 3/1 EF at High- β

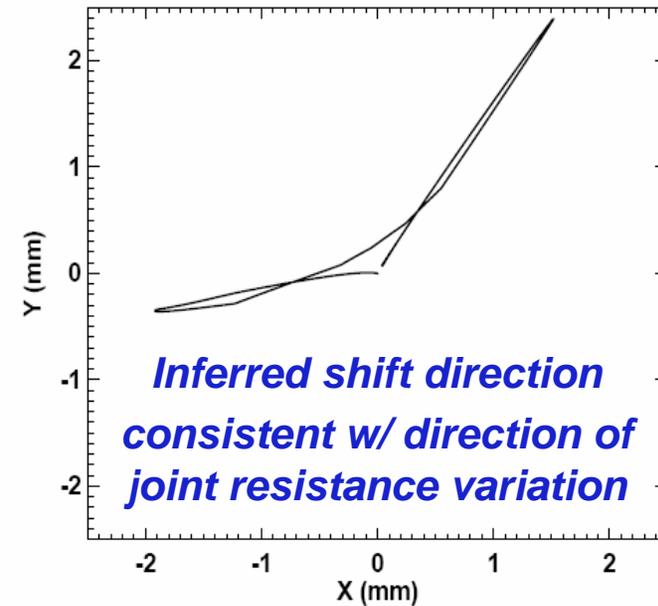


\Rightarrow additional EF source is present, or EF is not static

TF flag-joint resistance measurements imply interaction between OH transformer and TF coil \Rightarrow TF motion



Magnetics measure $n=1$ radial field $\propto I_{OH} \times I_{TF} \Rightarrow$ Can infer TF shift direction:



Inferred shift direction consistent w/ direction of joint resistance variation

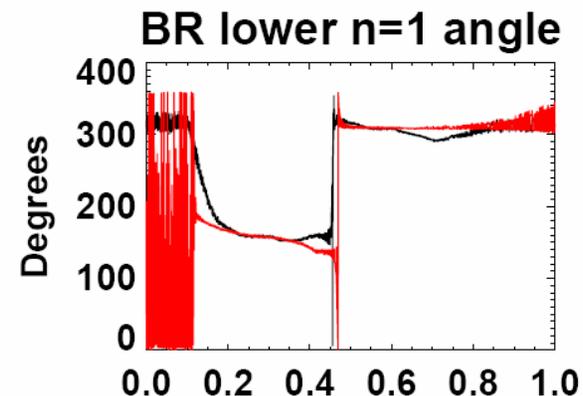
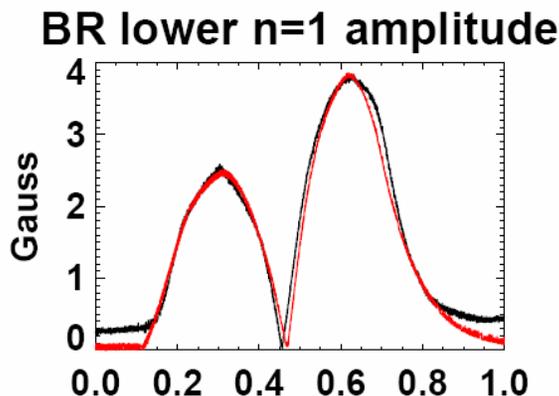
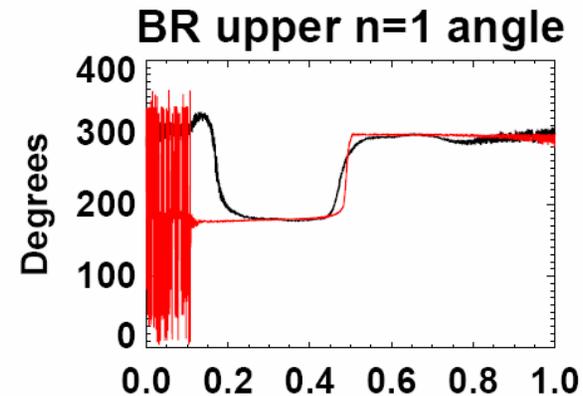
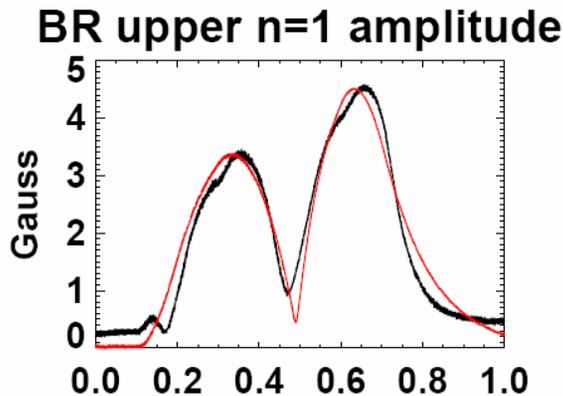
Accumulated data strongly suggests OH/TF interaction causes TF motion which creates a time-dependent error field that varies throughout shot even when all other plasma parameters and coil currents are fixed

Accurate modeling of $n=1$ B_R error field from $\text{OH} \times \text{TF}$ requires inclusion of time lag and polarity dependence



- Have developed TF model allowing **both shift and tilt** – 4 degrees of freedom
- Filter time-constant of approx. 100ms needed to capture time lags (inertia?)
- Prediction of EF at sensor \rightarrow prediction of EF in plasma

*Measured
& Simulated
error field
at sensors*

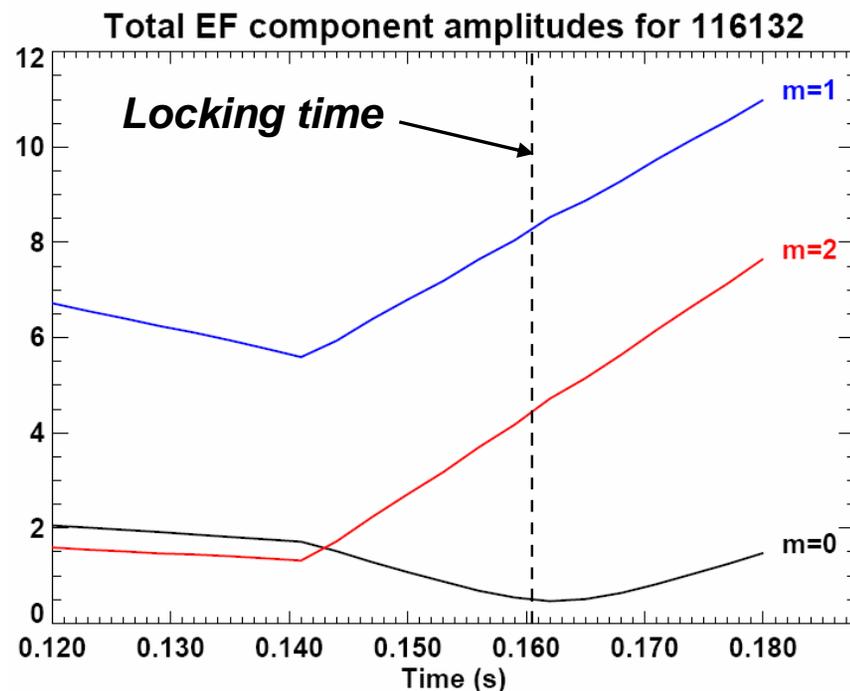
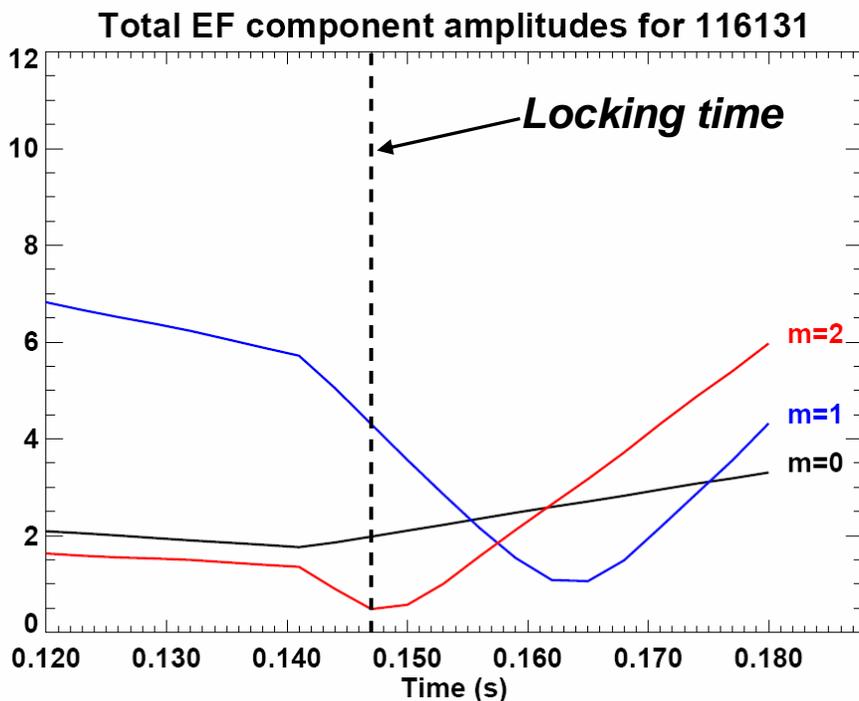


Locked-mode experiments indicate $m=0$ EF component may dominate rotation damping & locking



Assuming I have all the signs correct...

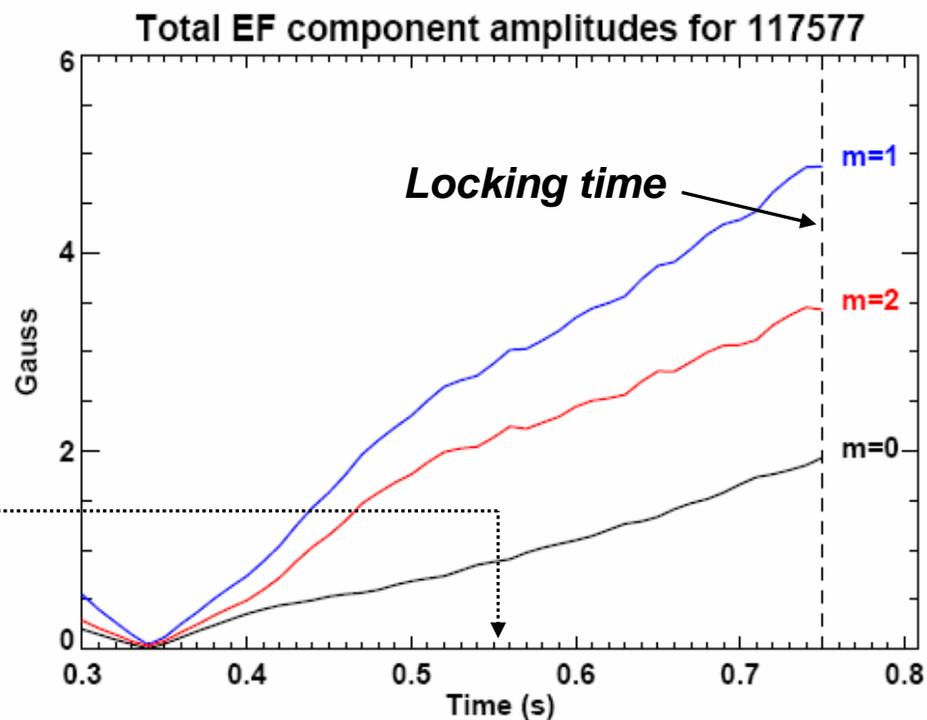
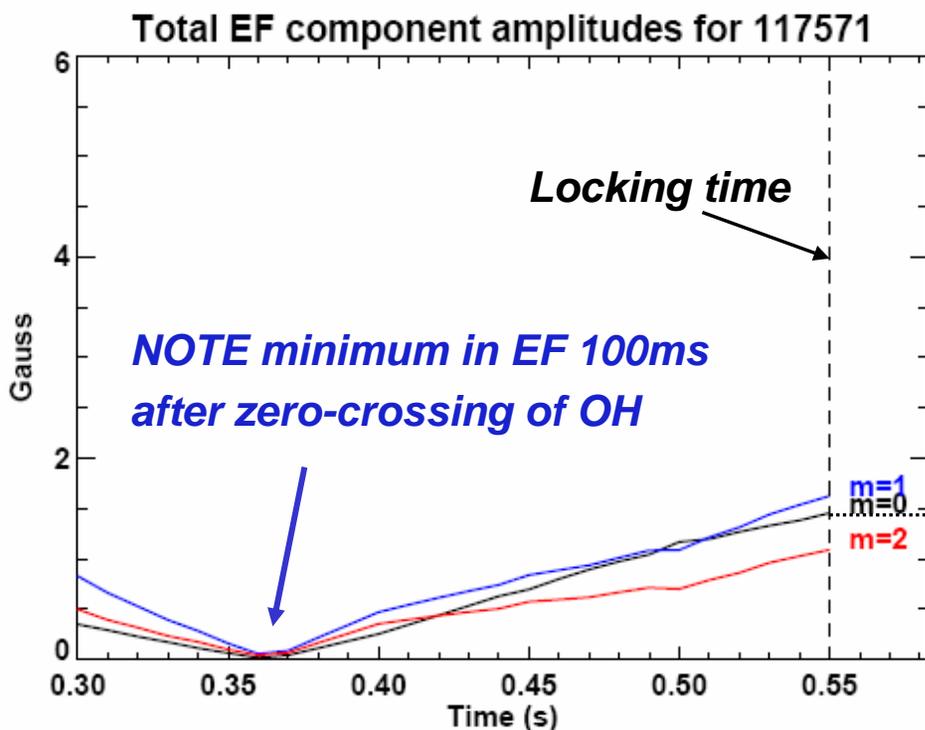
- $m=1, 2$ components ***larger*** in shot with later locking
- But, $m=0$ is reduced in shot with later locking
- NOTE: external EF is ramped linearly beginning at 140ms



High-beta experiments also indicate $m=0$ EF component may dominate rotation damping & locking



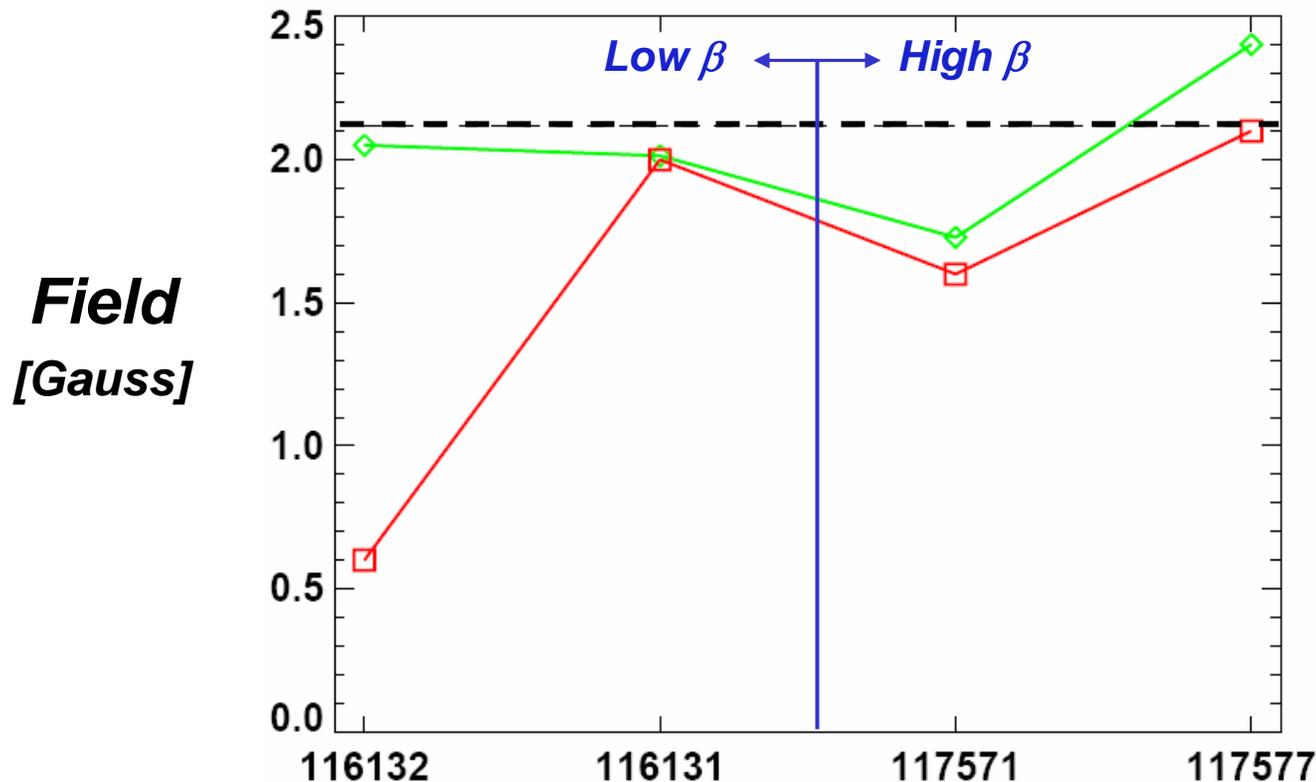
- NOTE: external EF reaches flat-top at 500ms
- $m=1, 2$ components are again **larger** in shot with later locking
- $m=0$ is again reduced in shot with later locking



Low and high-beta data can be used to compute empirical scaling for locking disruption threshold



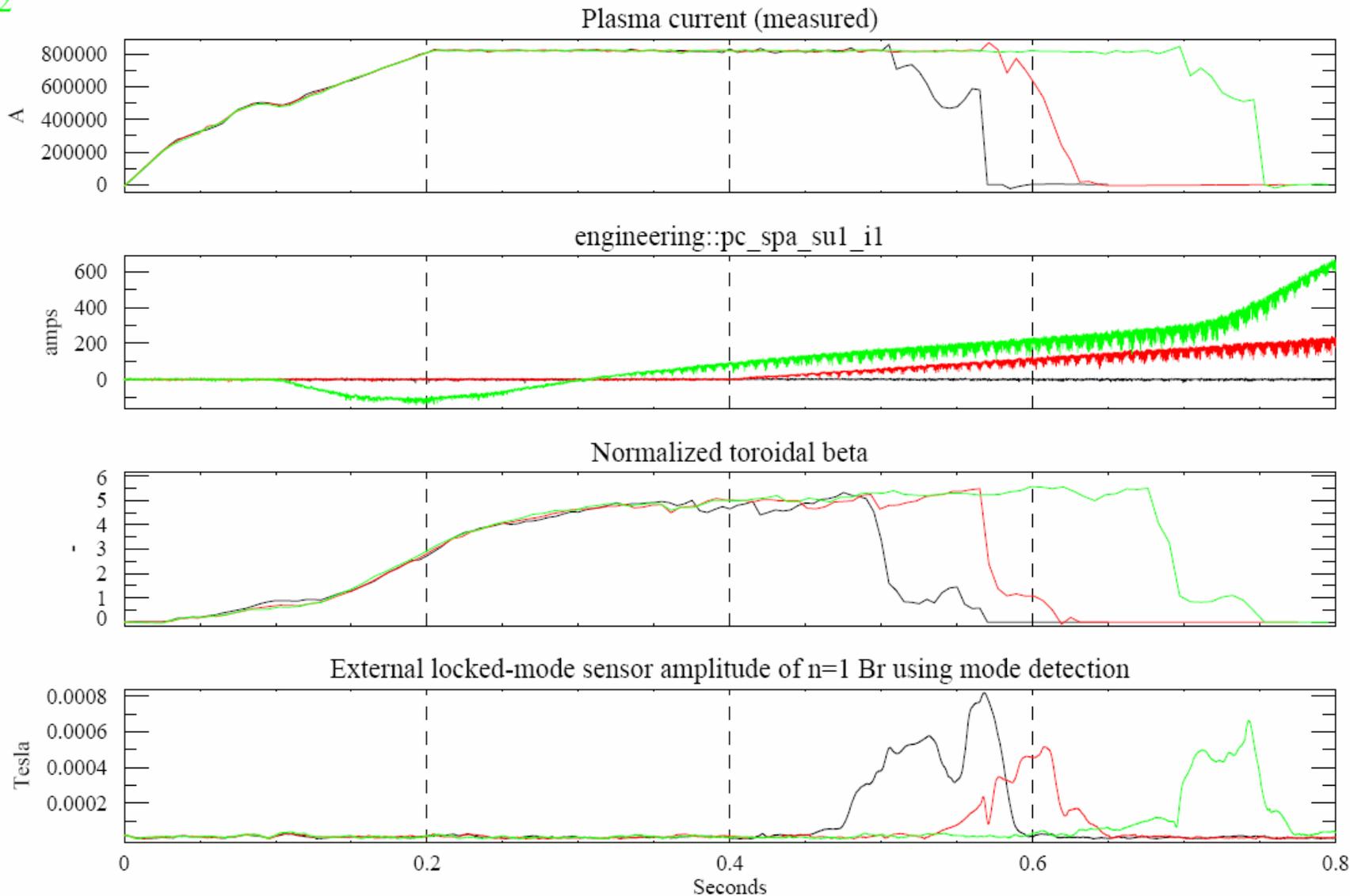
- Empirical threshold: $\sqrt{B_{m=0}^2 + 0.22 \times B_{m=2}^2} < 2.1$ Gauss
 - Addition of m=1 component changes m=0+2 fit very little
- Good fit with only m=0 and m=2 components: $\pm 12\%$ variation
- Poor fit if only m=0 component is included: $\pm 38\%$ variation



XP614: Comparison of EFC techniques at high β_N – Menard

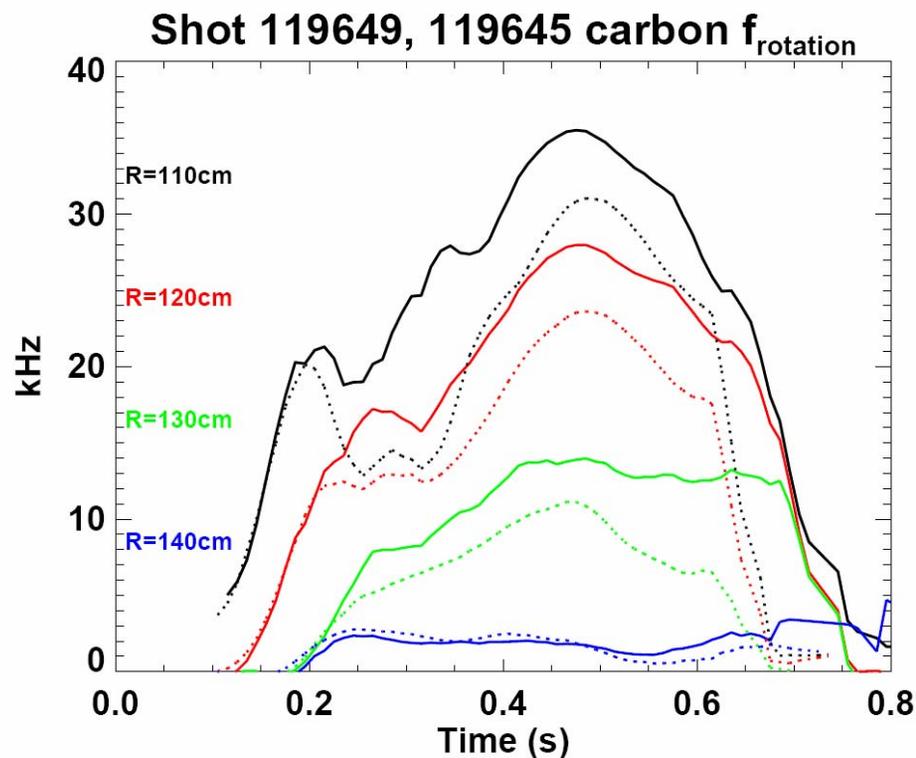
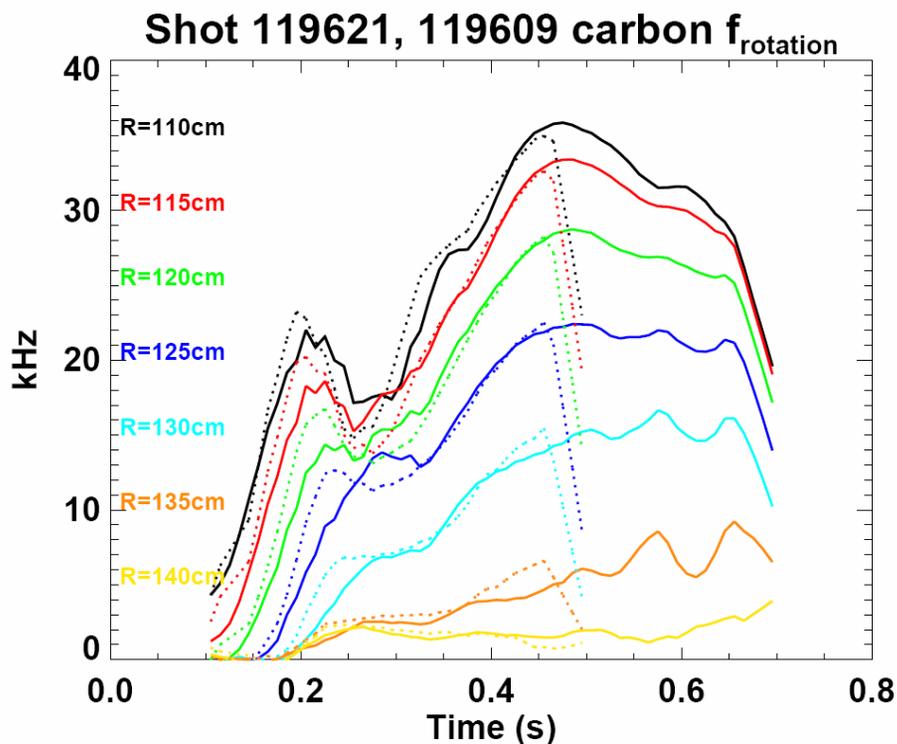
119609
119615
119622

- Longest duration, highest β_N achieved with OHxTF predictive EFC (119622)
- Pre-programmed ramp (119615) guesses at OH evolution \Rightarrow not as good



Applying EFC sustains plasma rotation and can increase β
(119609 no EFC - dashed, 119621 w/ EFC - solid)

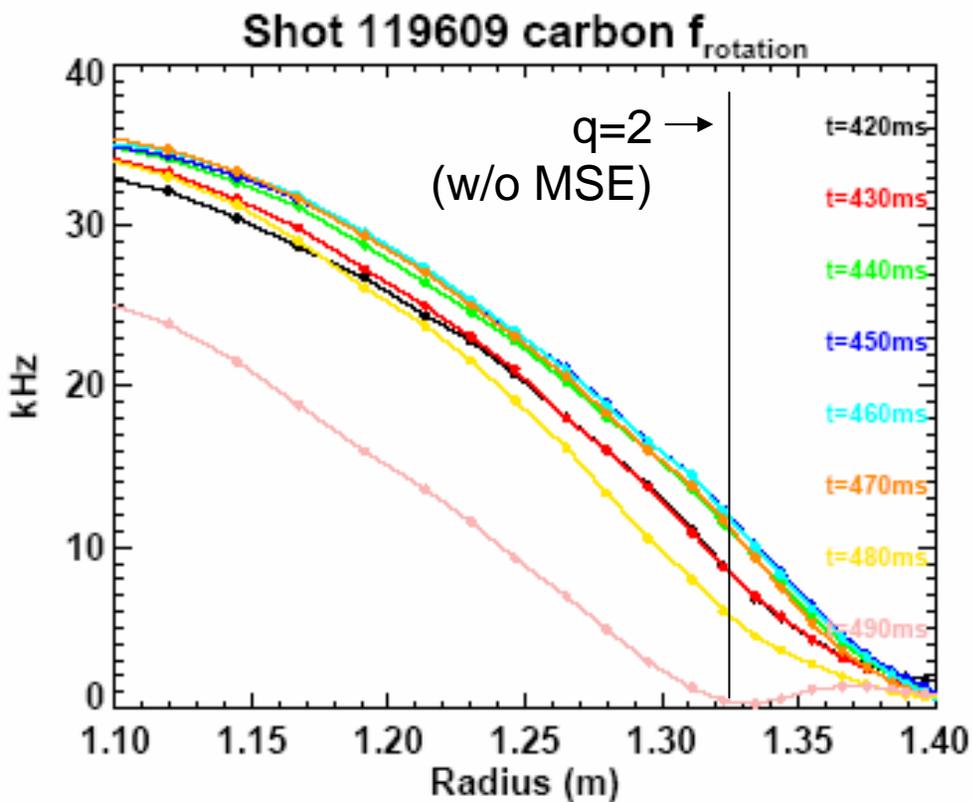
- Scan of EFC amplitude finds that optimal proportionality value (119649) results in higher rotation and beta than shot with non-optimal value (119645 - dashed)



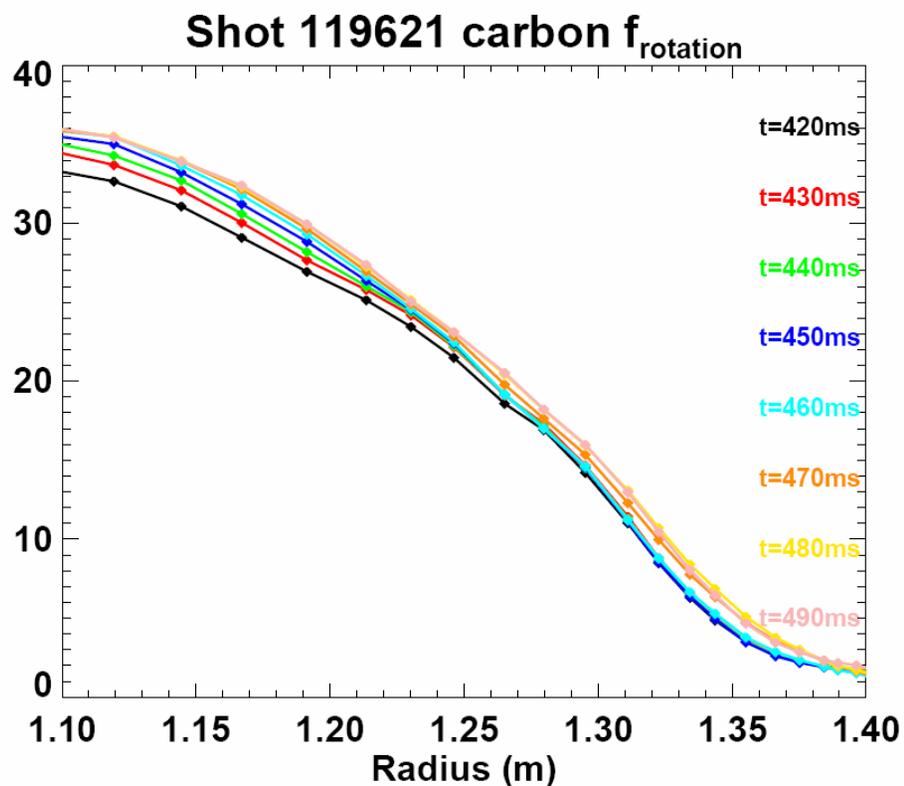
Rotation responds strongly to only
20% variation in EFC amplitude

Applying EFC keeps rotation high at location of $q=2,3$ surfaces

No EFC

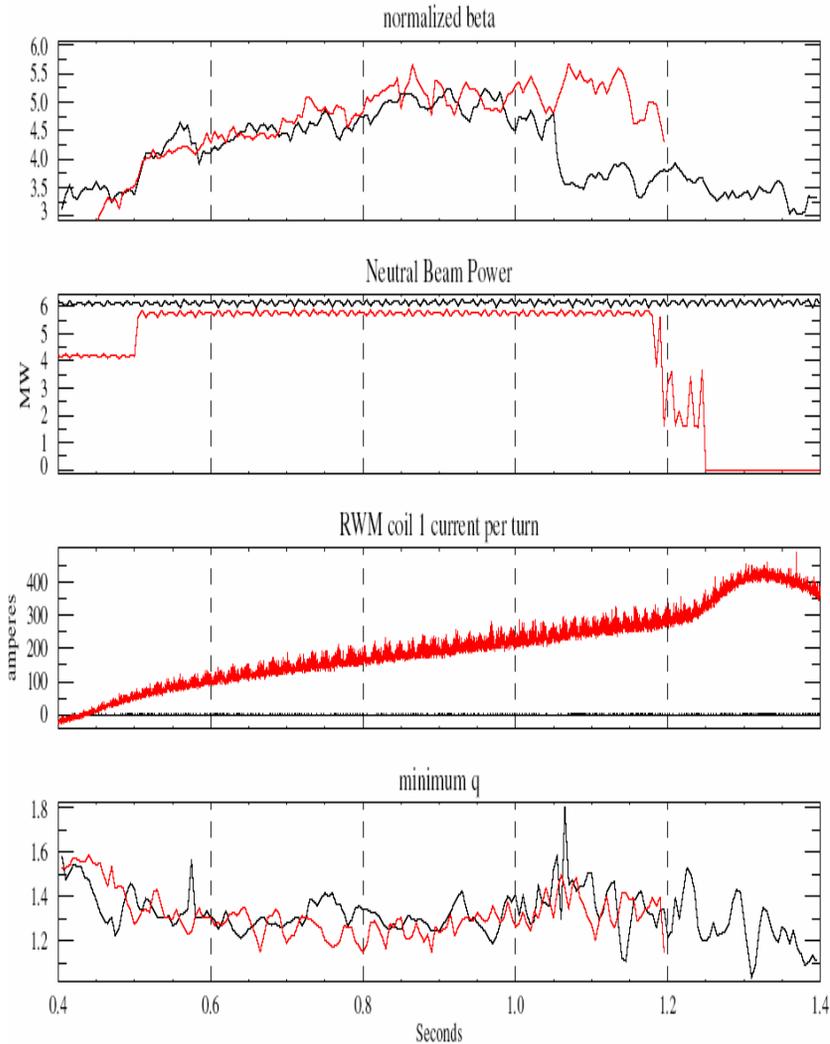


With EFC

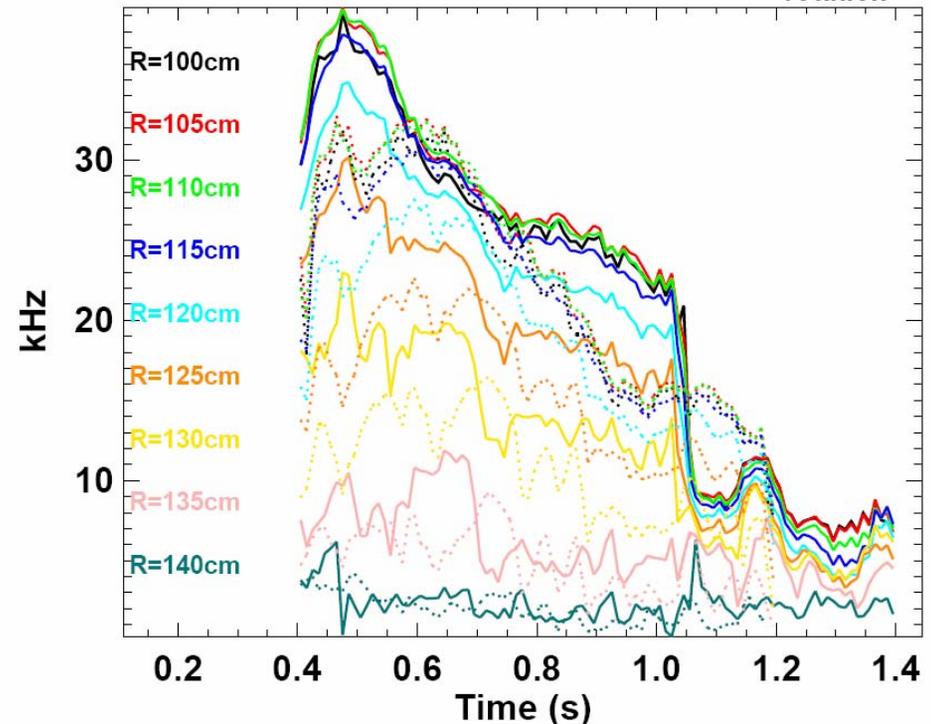


High β_N phase is longer in recent 750kA long-pulse shots using EFC, **but rotation is lower late in shot...**

- After 800ms, rotation decreases with n=1 EFC current present
- **Suspect EFC amplitude/phase is not optimal late in shot (higher I_{OH})**
 - Similar trend seen in 1MA shots



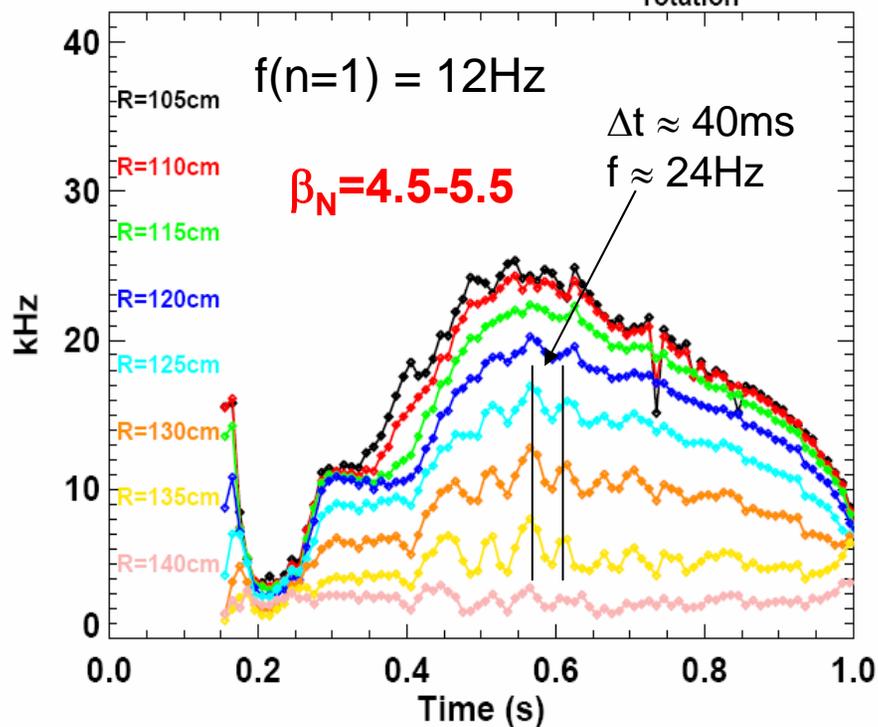
Shot 116313, 119922 carbon f_{rotation}



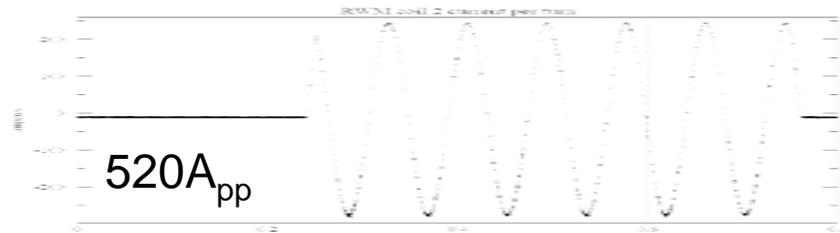
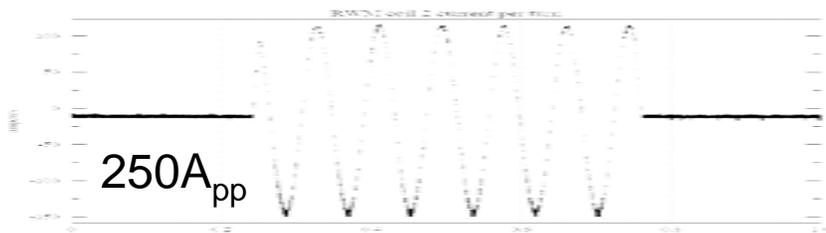
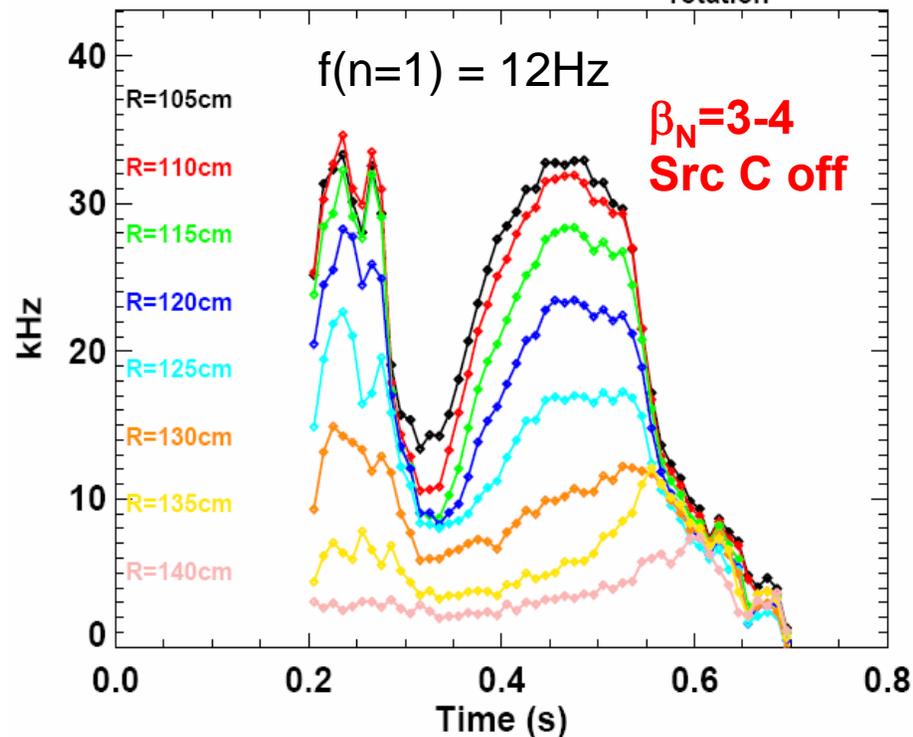
XP618: Optimize error field correction vs. rotation – LaHaye, Strait

- Observe rotation modulation at 2nd harmonic of applied field
- Little to no rotation modulation observed below no-wall limit

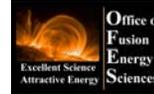
Shot 119629 carbon f_{rotation}



Shot 119631 carbon f_{rotation}



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Flow control and RWM physics in NSTX

Presented by J. Menard for:

S.A. Sabbagh¹, A.C. Sontag¹, W. Zhu¹, M.G. Bell², R. E. Bell², J. Bialek¹, D.A. Gates², A. H. Glasser³, B.P. LeBlanc², F. Levinton⁴, J.E. Menard², H. Yu⁴, D. Battaglia⁵, and the NSTX Research Team

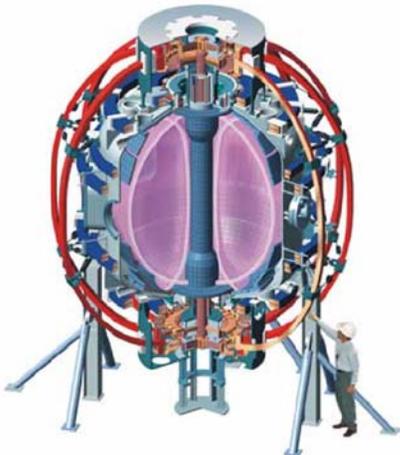
¹*Department of Applied Physics, Columbia University, New York, NY*

²*Plasma Physics Laboratory, Princeton University, Princeton, NJ*

³*Los Alamos National Laboratory, Los Alamos, NM*

⁴*Nova Photonics, Inc., Princeton, NJ*

⁵*University of Wisconsin, Madison, WI*



US/Japan Workshop on MHD

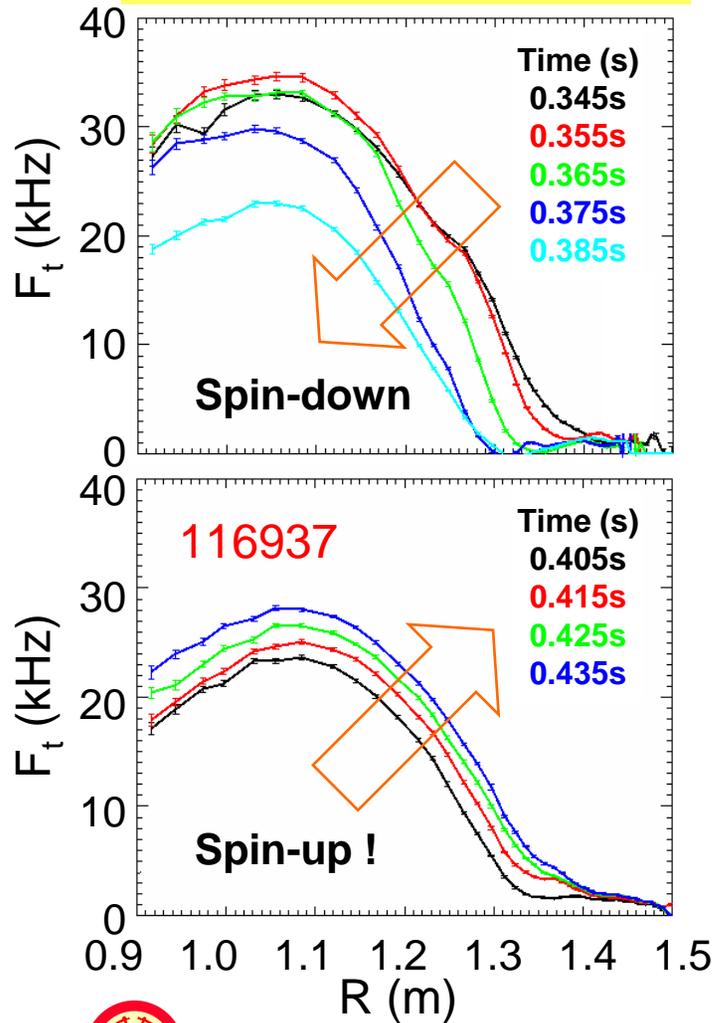
February 8, 2006

Naka, Japan

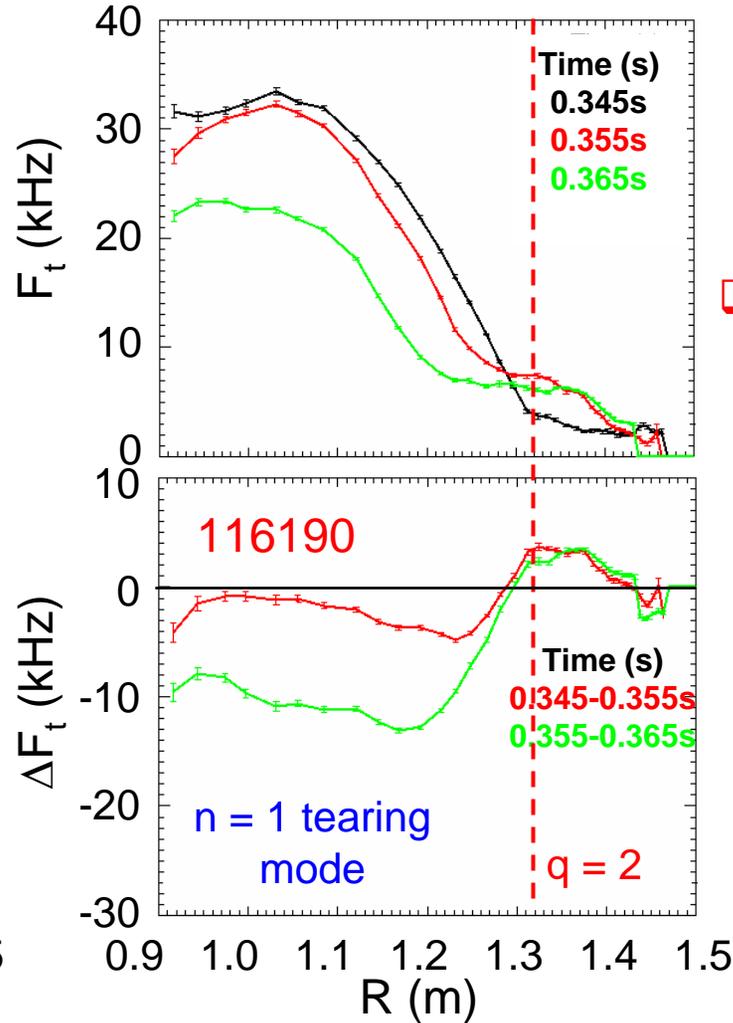
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U Tokyo
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Ioffe Inst
TRINITI
KBSI
KAIST
ENEA, Frascati
CEA, Cadarache
IPP, Jülich
IPP, Garching
U Quebec

Attention placed on studying non-resonant rotation damping physics

non-resonant damping



resonant damping



□ Non-resonant

□ Global profile control by pulsing the applied field

□ Resonant

□ Local $J \times B$ torque can explain damping by tearing modes

□ Outward momentum transfer across rational surface

□ Leads to rigid rotor core



Neoclassical toroidal viscosity (NTV) theory tested as non-resonant damping mechanism

Torque balance:
$$-\rho R^2 \left(\frac{\partial \Omega_\phi}{\partial t} \right) = T_{\vec{J} \times \vec{B}} + T_{\text{NTV}}$$

measured computed
 (Set = 0 here - tearing modes avoided.)

$$T_{\text{NTV}} = K \cdot \left[R \frac{\pi^{1/2} p_i}{v_{t_i}} \Omega \varepsilon^2 \frac{1}{B_t^2} q \sum_{n,m \neq 0} \frac{\mu_{ps1} n^2 (b_r^{nm})^2}{C_v + \mu_{ps1} |m - nq|} + T_{\text{NTV}}^{m=0} \right]$$

factor $T_i^{1/2}$ profiles collisionality

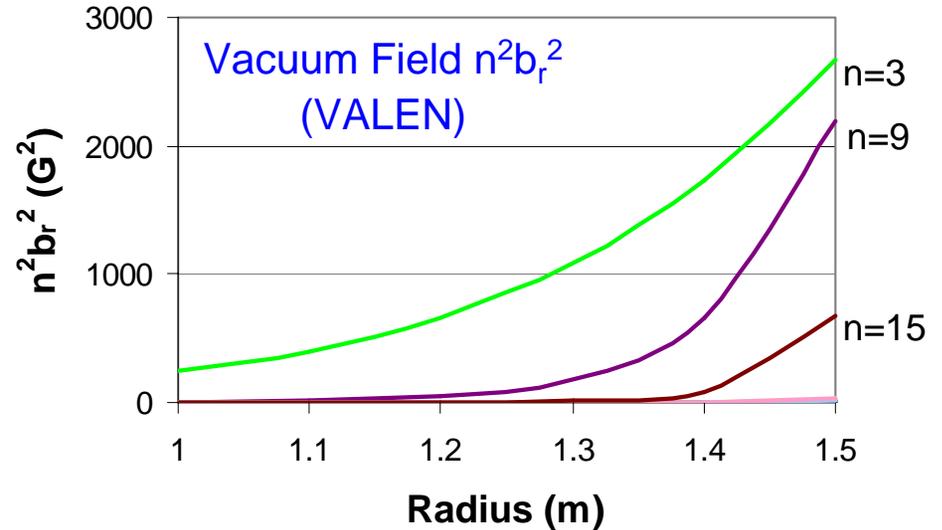
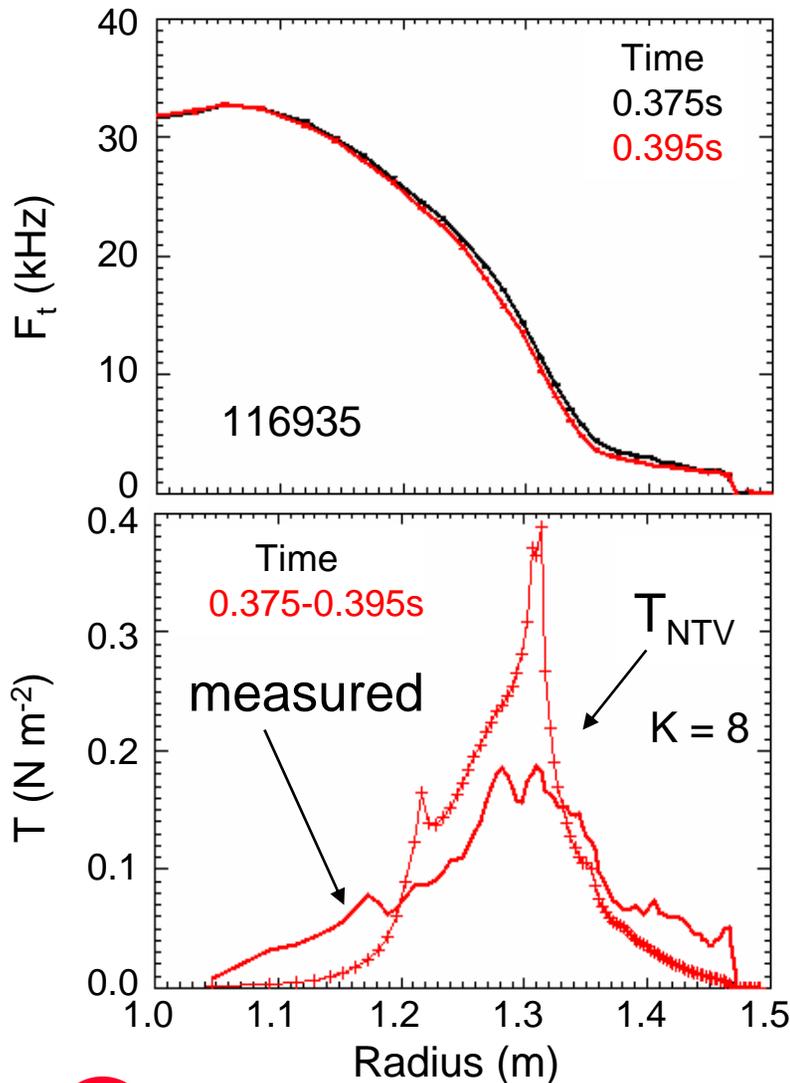
$$\mu_{ps1} = 1.365 \quad C_v = \frac{2\sqrt{\pi}}{3} \frac{2v_{ii}}{v_t/Rq}$$



Damping caused by kinked field

K.C. Shaing, Phys. Fluids 29 (1986) 521.; E. Lazzaro Phys. Plasmas 9 (2002) 3906.

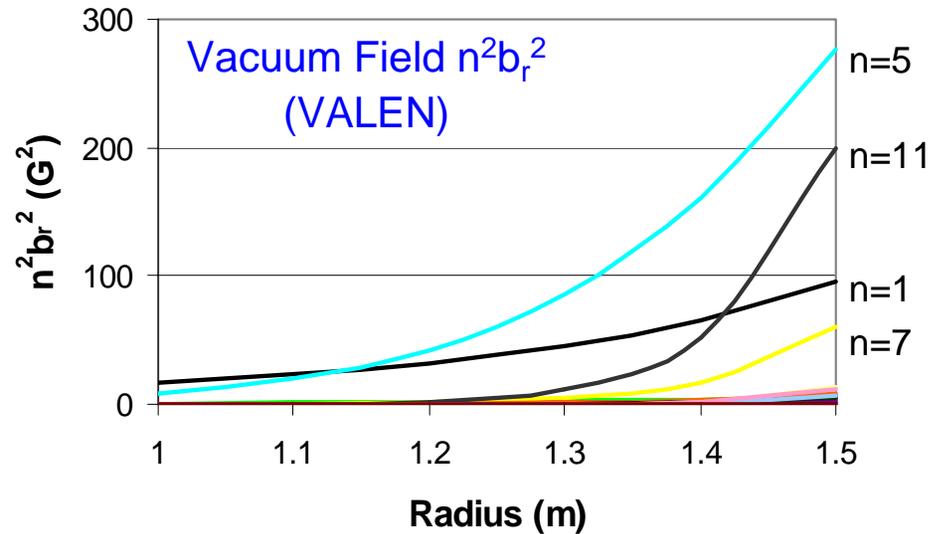
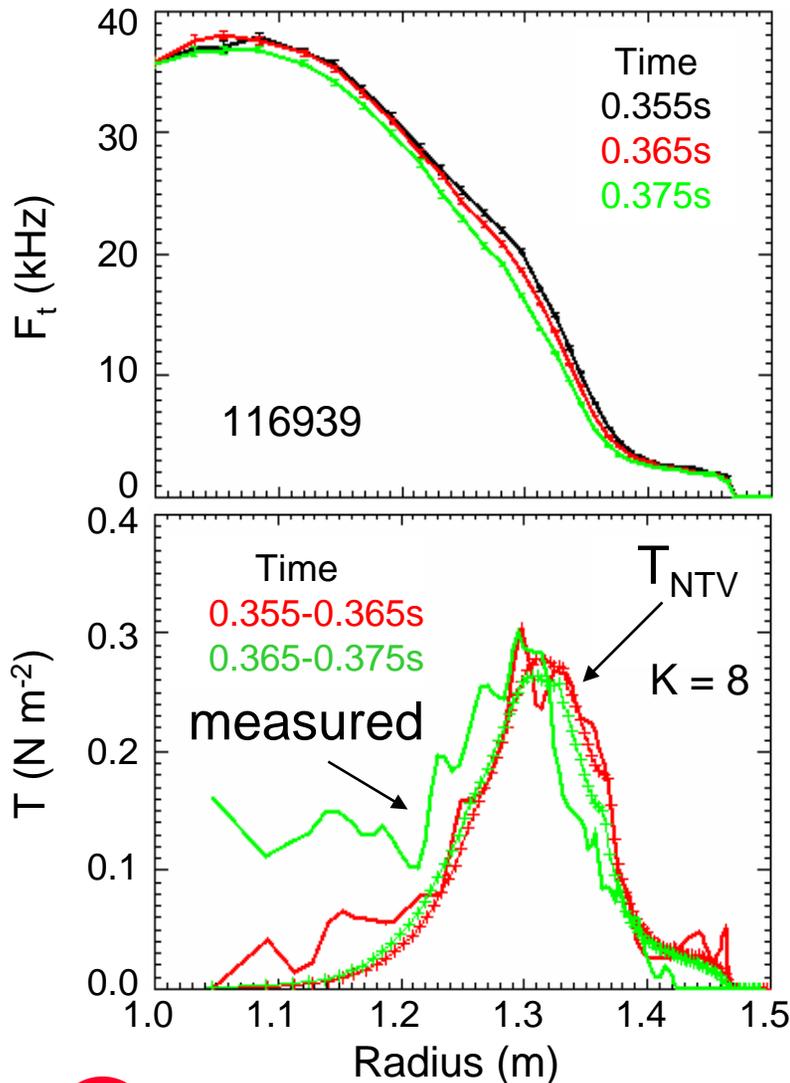
Applied field alone yields moderate, global rotation damping



- $n = 3$ DC field (800A)
- Damping reduced at large R due to reduction in T_i
- $n=1-15$ field components included
- Resonant denominator in NTV theory might be overemphasized
- Function of collisionality



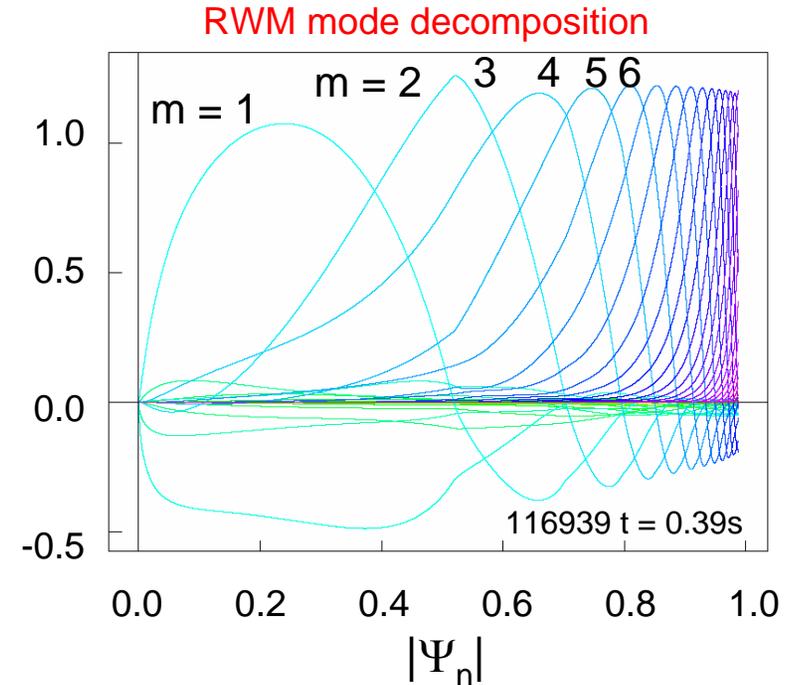
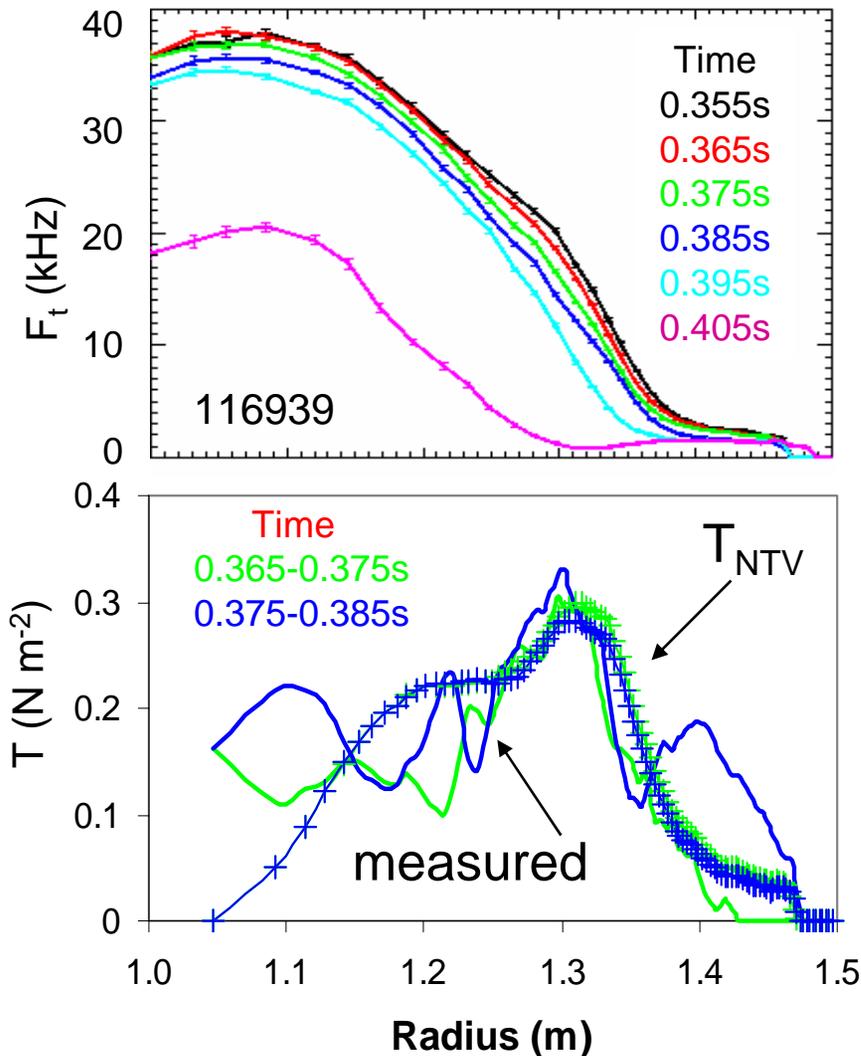
RFA enhances, broadens rotation damping



- $n = 1$ DC field (800A)
- $n=5$ torque larger than $n=1$ torque ($n^2 b^2$ scaling)
- $n=1-15$ components included
- Broadening damping profile



RWM eigenfunction can explain broader damping

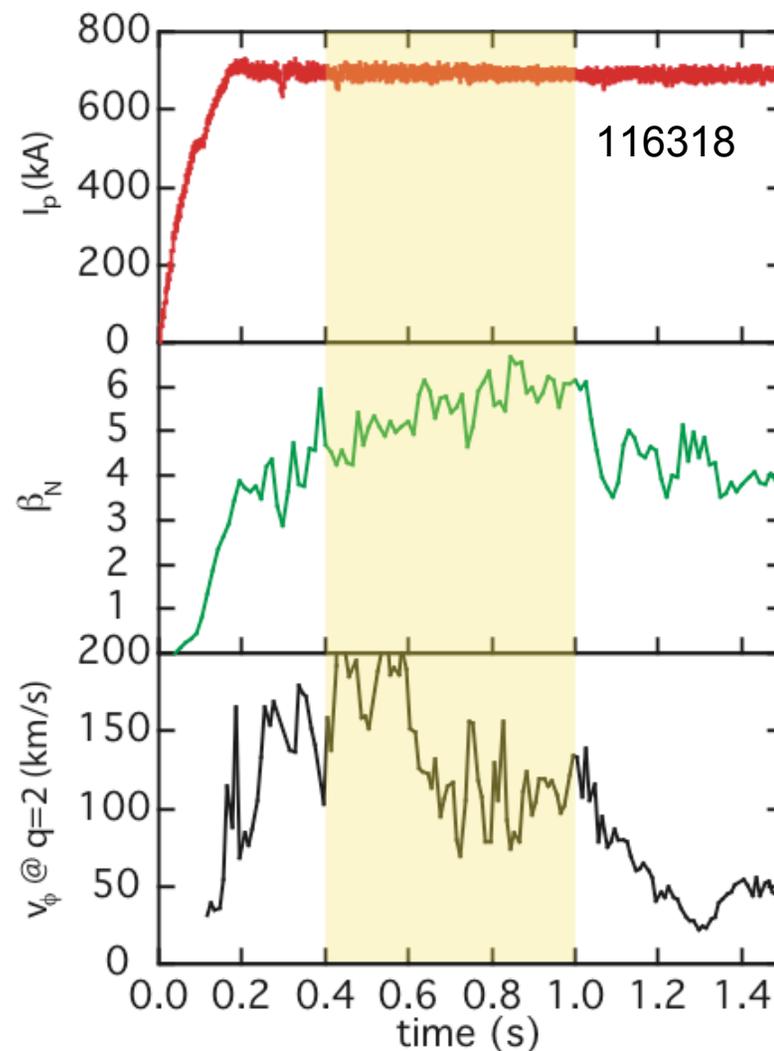
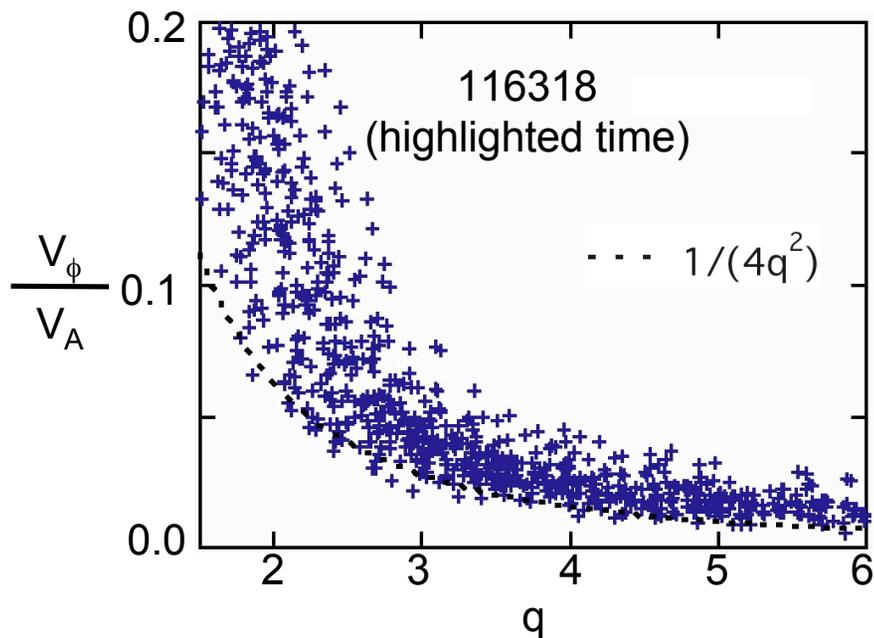


- DCON $n = 1$ ($m = -12$ to 26)
RWM calculated eigenfunction
- No-wall boundary condition
- Need to evaluate with-wall boundary condition; inclusion of measured $n = 2$ component



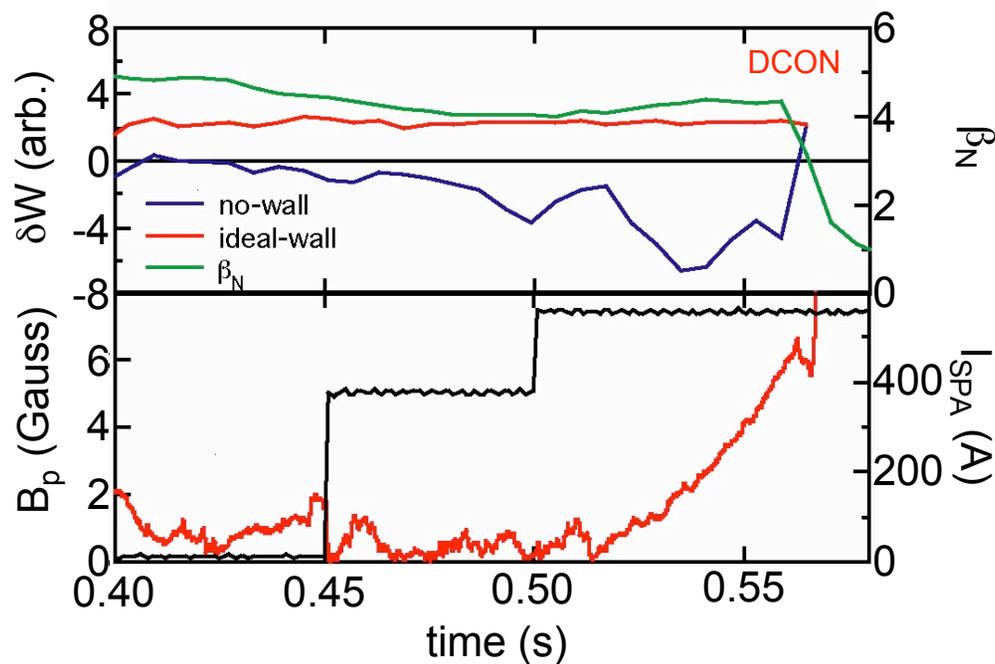
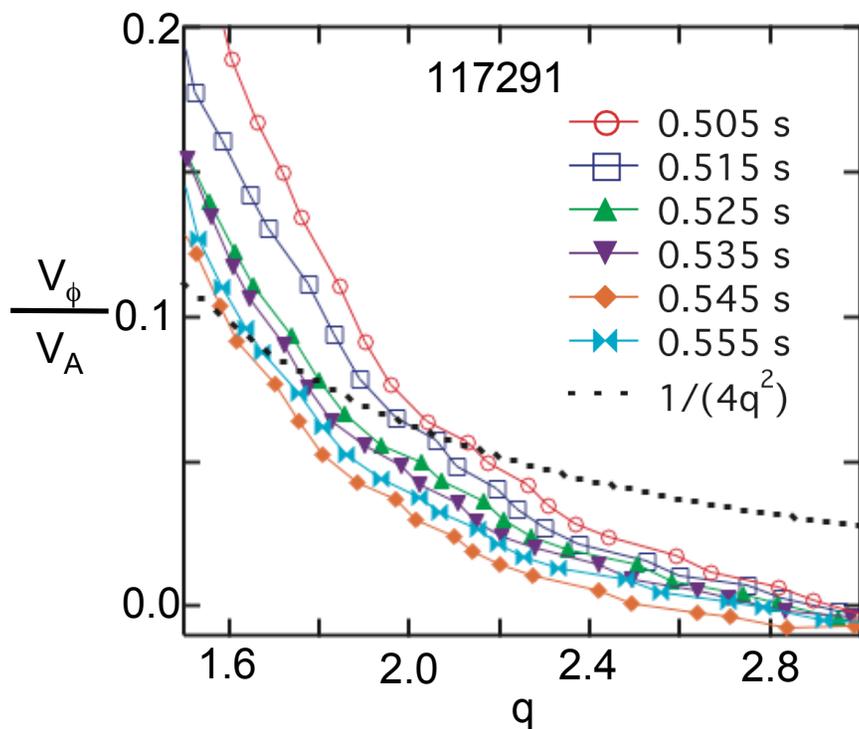
High Toroidal Rotation Across Entire Profile Allows Sustained High β_N

- Entire rotation profile stays high during high- β period
 - Alfvén speed normalization & q dependence from drift-kinetic theory
- Trend observed in numerous discharges



Rotation on Higher Order Rational Surfaces Not Required for RWM Stabilization

- Plasma remains RWM stable with near zero rotation outside $q = 3$
 - Stable with near zero rotation outside $\psi_N = 0.62$
 - growth coincides with low rotation inside of $q = 2$

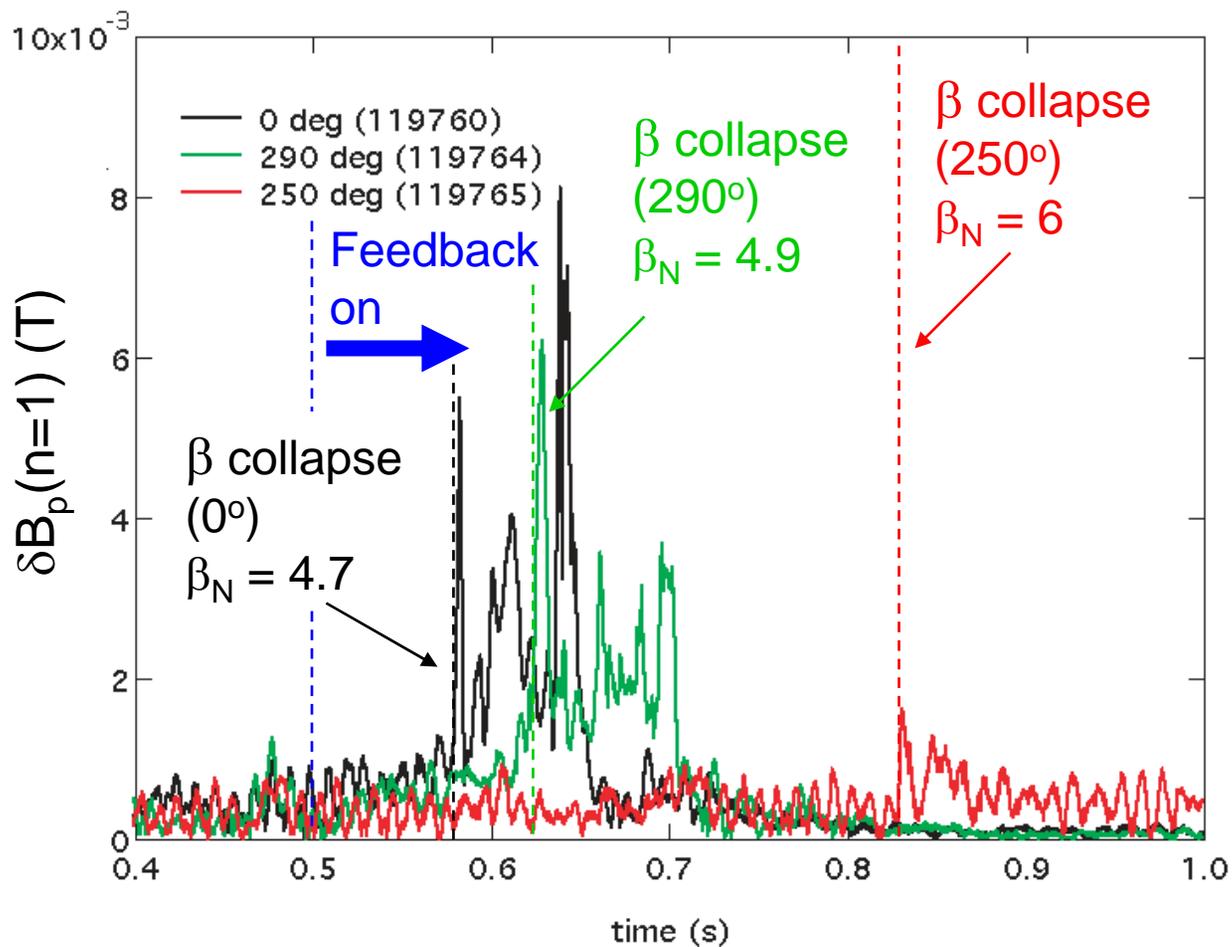


XP615: Active Stabilization of the Resistive Wall Mode at Low Aspect Ratio

□ Goals (Part I):

- Operate new RWM feedback system on 0.9–1.0 MA DND target
 - All aspects of RWM control system / RWM sensors worked well.
 - Good target plasmas with wide $n=1$ free window; high β_N up to 6.
 - Both locked/rotating RFA/RWM were observed/tracked by feedback.
- Vary RWM feedback phase/gain to show control system influence
 - $I_p = 1.0$ MA target showed “best” phase $< \sim 270^\circ$
 - $I_p = 0.9$ MA target more conclusive / finer scan; best phase = 225°
 - “Best” phase depends on whether mode is rotating or not
- Reduce plasma rotation with $n = 3$ braking to excite RWM if needed
 - RFA observed / RWM excited without braking in most cases
 - $I_p = 0.9$ MA target with phase = 250° , 225° required braking to excite mode

Setting RWM feedback relative phase in the range $\sim 250^\circ$ superior for longer pulse, higher β_N vs. $\sim 0^\circ$



Phase scan

- Varied through 360° , finer scan in 270° range; 225° appears to be “best”
- $n = 3$ braking required to generate RWM when phase set to most favorable settings

NSTX Experiment Summary



- Found non-static error field from $\text{OH} \times \text{TF}$ interaction
 - Data suggests $m=0$ EF component dominates
 - Similar to Lazzaro's observations on JET w/ NTV model?
- Increased discharge duration using EFC at high- β_N
 - Attempting Dynamic EF Correction (DEFC, i.e. feedback)
 - Will compare “predictive” EFC to DEFC
- NTV theory consistent with observed flow damping from RFA and RWM
- First systematic attempts at RWM feedback using low-rotation target starting today

Desired code capabilities – a partial list



- Error field correction:
 - Rely on rotational stabilization of RWM to access β above NW limit
 - Requires minimization of flow damping
 - Need to know plasma response to EF and torque from 3D fields
- Need self-consistent “free-boundary” plasma response to non-axisymmetric fields – above and below no-wall limit
 - VMEC – useful below no-wall limit
 - How do plasma boundary and internal field respond to shifted/tilted TF?
 - Extend NMA code (DCON + VACUUM) to include coil + plasma eigenfunctions including ideal wall response (Chance/Chu)
 - Need plasma response above no-wall limit - wall stabilization from rotation
 - Need internal B-field structure for flow-damping from non-resonant NTV and resonant JxB torque from islands
 - Have DCON B-norm already for NTV (Zhu, Sabbagh)
 - Working on other B-components + singular currents from DCON (J.K. Park)
 - MARS-F – has 3D fields/coils, rotation, resistive wall, etc.
 - Working on benchmarking field calculations against DCON (me + JK Park)