

National Spherical Torus eXperiment Upgrade

Inner-PF Magnet Replacement WBS 1.01.03.01 & 1.01.03.01a

NSTX-U Recovery Project FDR – March 17-19, 2020

[Mike Kalish](#) - Cognizant Engineer

Last edit: 3/9/20

Outline

1. Overview

2. Scope

3. Requirements and Interfaces

4. Analysis/Prototyping

5. Chit Closure

6. Procurement, Fabrication, Installation, and Test

7. Risk - Project Risks and Design FMECA

8. Quality, Environmental, Safety, and Health

9. Summary

Overview - WBS 1.01.03.01 &.01A

(CDE-3A Scope)

WBS Title	Inner PF Replacement	WBS #	1.01.03.01 & .01A
Project Cog.	Mike Kalish	Assoc. Proj. Man.	Gary Swider
Design Scope	Design new inner-PF coils for NSTX-U		
Technical Impact of Scope	Coils provide primary capability to form a magnetic divertor on NSTX-U		
Design Status	FDR completed on 3/30/2018: review link chits: link calculations: link drawings: link SoW/Tech Spec: link		
Fabrication Status	Six solenoid coils of three types being fabricated at Sigmaphi in France; Of the six two have been wound and are awaiting epoxy impregnation (VPI). Two more are in the process of winding		
Installation Status	Coils will be installed in slings as part of the Machine Core Structures Scope		

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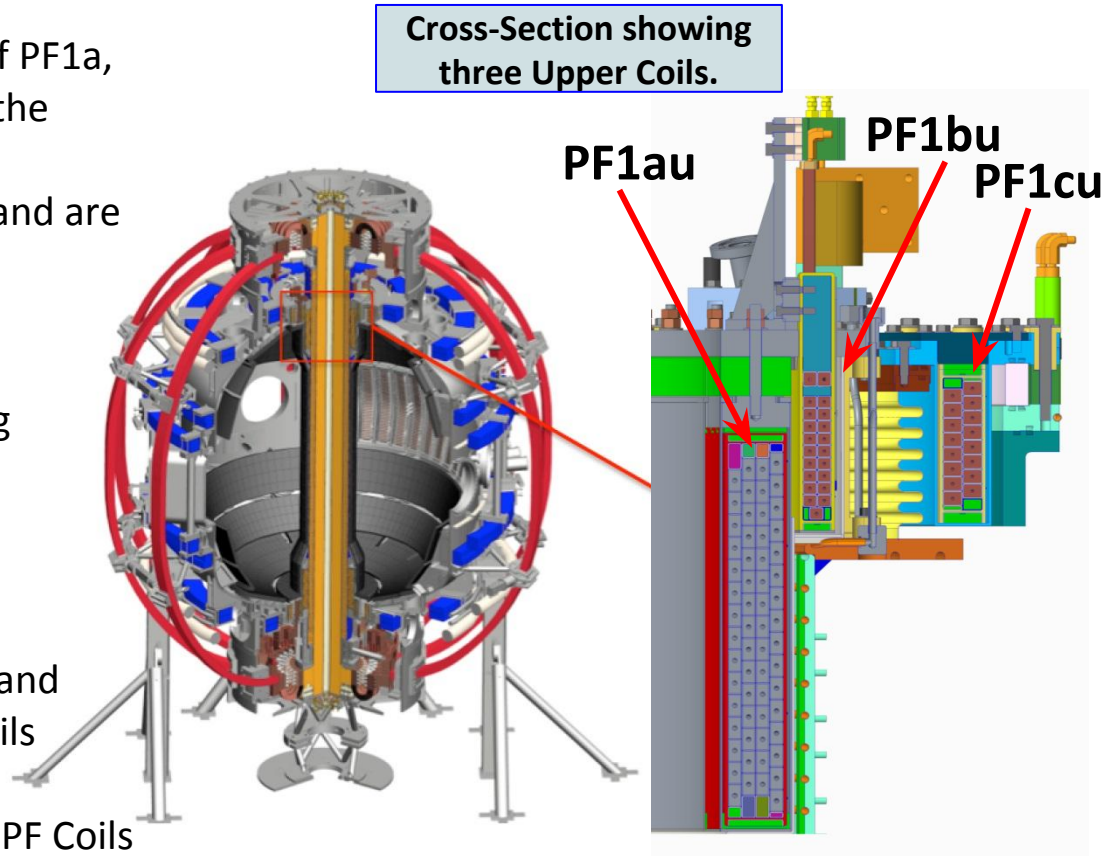
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Inner PF Coils - Scope

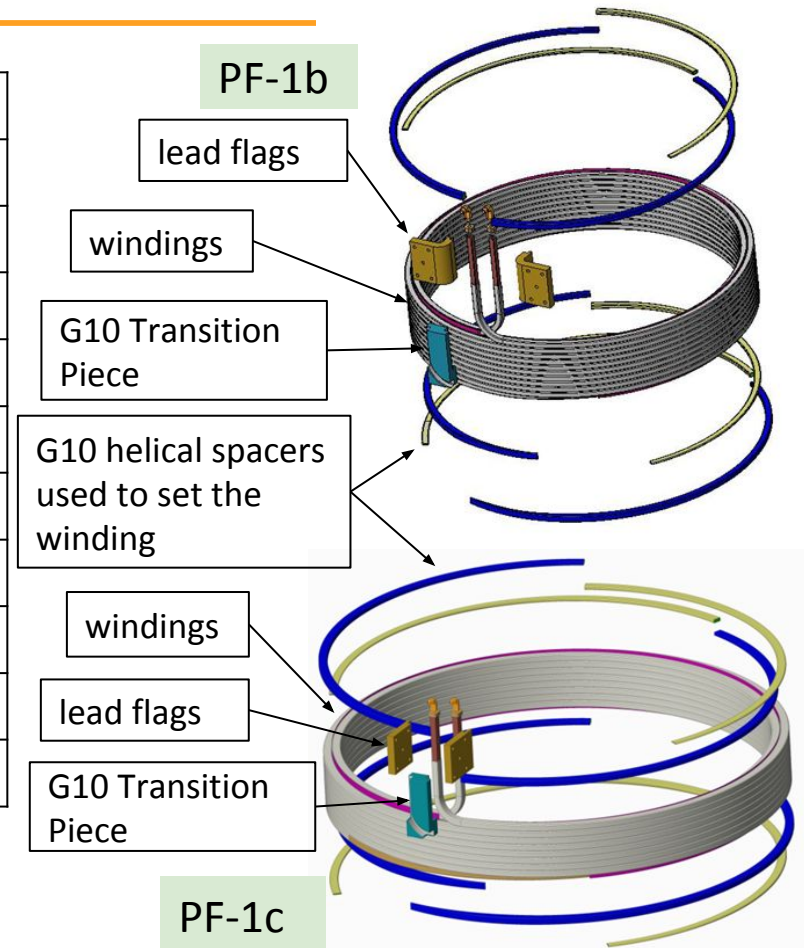
- There are six Inner PF Coils, a pair each of PF1a, PF1b and PF1c at the top and bottom of the center stack.
- All Inner PF Coils have been redesigned, and are being fabricated, tested and replaced
- Completed scope (sunk cost) includes
 - designing a prototype PF1a coil
 - fabricating, testing and evaluating four PF1a prototypes (3 at vendors, 1 at PPPL).
 - designing new Inner PF production coils
 - fabricating conductor, insulation and other materials for production coils
- Remaining scope includes
 - completing fabrication of 6 Inner PF Coils
 - testing those six coils



Inner PF Coils - Design Parameters

		PF-1a	PF-1b	PF-1c
Coil Terminal to Terminal Voltage	kV	2.03	2.03	2.03
Current	kA	19.7	20.0	20.2
# of Layers		4	2	2
# of Turns		61	20	16
Turn-to-Turn Voltage	V	33	101	127
Turn-to-Turn Safety Factor		2168	709	567
Layer-to-Layer Voltage	V	1013	2026	2026
Layer-to-Layer Safety Factor		76	38	38
Max Turn-to-Ground Voltage	V	2026	4052	4052
Turn-to-Ground Safety Factor		54	27	27

Temperature limit and pre-load chosen to limit thermal strains to acceptable values



Insulation Design Has High Dielectric Standoff

Layer to Layer Voltage Standoff

Maximum Layer to Layer voltage PF1b and PF1c
Dielectric strength

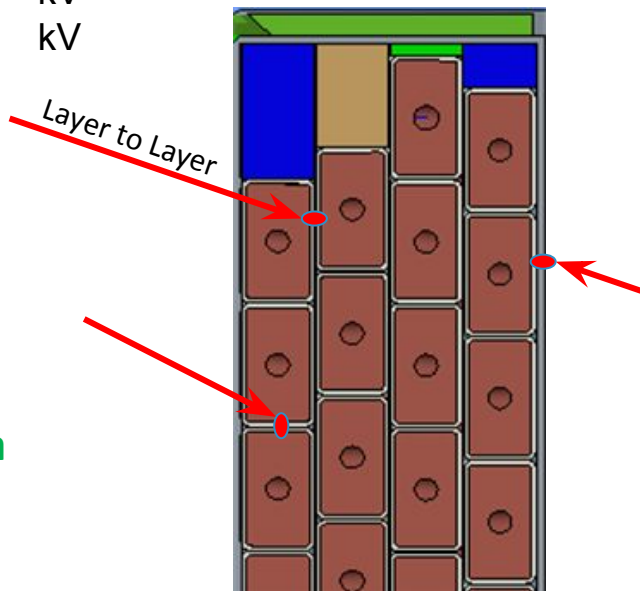
Safety factor PF1a	76
Safety Factor PF1b	38
Safety Factor PF1c	38

Turn to Turn Voltage Standoff

Safety Factor is 2168 for PF1a
Safety Factor is 709 for PF1b
Safety Factor is 567 for PF1c

Could not induce failure in any coil at max limit of test equipment:
= 20kV for layer to layer testing
= 55kV for conductor to gnd testing

2.03	kV
77	kV



Turn to Ground Voltage Standoff

Maximum Turn to Ground voltage PF1b and PF1c
Dielectric strength

Safety Factor PF1a	54
Safety Factor PF1b	27
Safety Factor PF1c	27

4.05	kV
110	kV

Charge question: 1

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Requirements Defined and Met

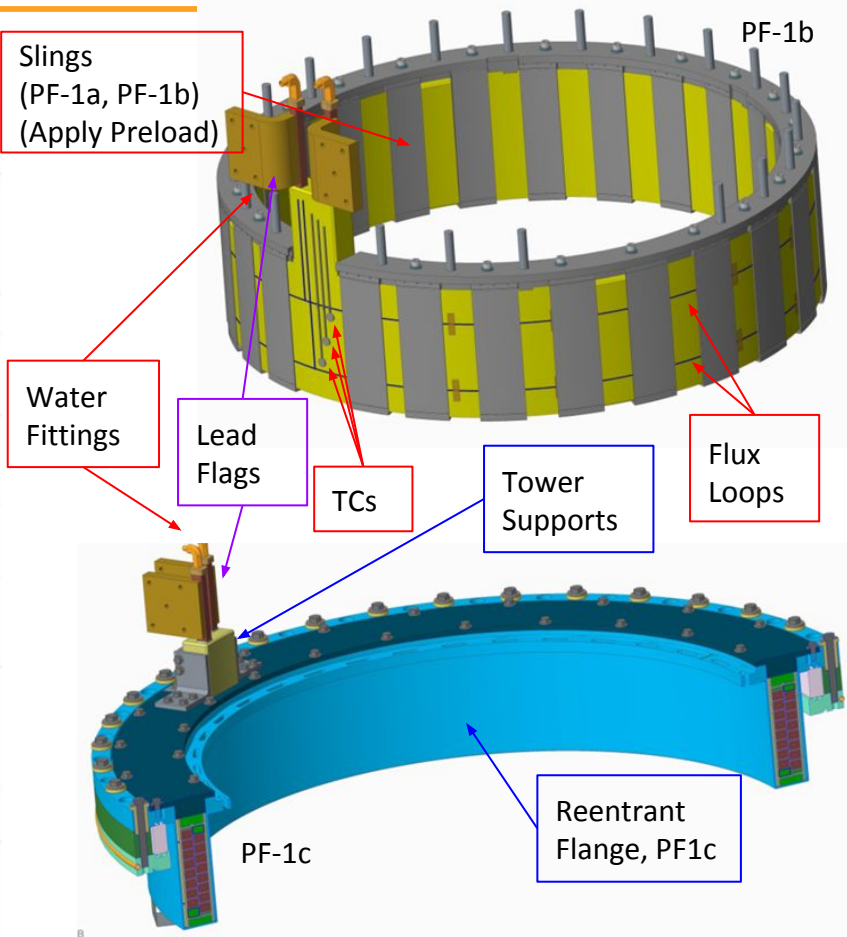
Source	Requirements	Comment	met
NSTX-U-RQMT-GRD-001	Waveform Specifications, Duty Cycle	Provides highest level requirements for 2 MA, 1 T, 10 MW, 5 second operation	✓
NSTX-CRIT-0001	Design Criteria	Provides the project definition of margin for loads vs. allowables	✓
NSTX-U-RQMT-SRD-002	Amp-Turn Capability For Each Coil	Requirements determined by physics goals for flexibility in shaping	✓
NSTX-U-RQMT-SRD-002	I ² t Limit For Each Coil	Constrained by physics needs and thermal stress limits	✓
NSTX-U-RQMT-SRD-002	Coil Centroids	Determined by required plasma shaping capability	✓
NSTX-U-RQMT-SRD-002	Design to facilitate turn-to-turn testing	Will utilize a mandrel-free construction method	✓
NSTX-U-RQMT-SRD-002	Diagnostic on Coils	Thermocouples and flux loops required	✓
NSTX-U-RQMT-SRD-002	High-pot requirements	2E+1 defined as the high pot voltage, including fault case	✓
NSTX-U-RQMT-SRD-002	Insulation Requirement	Safety factor of >10 required for ground and turn insulation	✓

Interfaces Defined in the SRD and Accommodated by Design

Interface Table from [NSTX-U-RQMT-SRD-002](#)

Table 7.6-1: Interfaces for the PF-1a coils (WBS 1.1.3.3.3)

Interfacing WBS	Interfacing System	Nature of Interface	Interface Boundary	Interface Description	Required Interface Documentation
1.3.2.1.2	High-Pressure NTC Cooling Water Distribution	Fluid	connection between i) hose w/ fitting and ii) and fitting on the coil	Hose connections at coil leads; cold water cools outer layers first	P&ID, Mechanical Design Drawing
1.7.3.4.2	Center stack coil thermocouples	Diagnostic	Surface of ground insulation	thermocouples applied to surface of coil	Mechanical Drawing
1.1.3.4	Bus Bar Systems and Bus Tower	Electrical Power	Flat surface of the coil flags.	Solid bus bars connect to the coil terminal	Calculation, Mechanical Design Drawing
1.1.3.4	Bus Bar Systems and Bus Tower	Structural	Flat surface of the coil flags.	Solid bus bars connect to the coil terminals, supporting part of bus bar run	Calculation, Mechanical Design Drawing
1.1.3.3.6	Center Stack Casing	thermal	At surface of coil	microtherm blanket provides thermal isolation between coils and casing	Mechanical drawing, Calculation
1.1.3.3.11	PF-1a Support Structure	Structural	At surface of coil support structures	Coil leads are supported as they extend from the winding pack	Mechanical drawing, Calculation
1.1.3.3.11	PF-1a Support Structure	Structural	Surface of ground wall insulation	Inner-PF coils are supported against all loads by the CS assembly. Pre-load is applied to the coils by the coil supports.	Calculation, Mechanical Design Drawing
1.4.1.2.2	Mirnov and Flux Loop System	Diagnostic	Inner Poloidal Field Coil Ground Insulation Surface	Poloidal Flux Loops mounted on Inner Poloidal Field Coils	Mechanical Drawing
1.1.3.3.10	Vertical Target Cooling System	spatial	at the surface of the heat transfer tubes	heat transfer tubes need to allow the PF-1a coil to fit through with sufficient clearance for alignment.	Mechanical Drawing



Details of Interfaces Defined in Interface Control Documents

System 1	System 2	ICD Link	Exposition
Magnets	Center Stack Assembly	link	Defines interfaces between the inner-PF coils and the center stack assembly
Magnets	Diagnostics	link	Defines interfaces between the inner-PF magnets and diagnostics such as flux loops and thermocouples
Magnets	Cooling Systems	link	Defines interfaces between the inner-PF magnets and the cooling water systems
Magnets	Power Systems	link	Defines interfaces between the inner-PF magnets and the Power Systems
Magnets	Operations and Systems Safety	link	Defines interfaces between the magnets and the Power Systems via a light curtain

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Comprehensive Calculations

Verify Design will Meet Requirements

Physical Quantity	Calculation #	Content
Forces on Coil lead from Bus Bars	NSTX-U-CALC-55-04	<u>Inner PF Coil Leads and Bus Bar Analysis</u> : Verifies coil lead design with Bus Bar interface loads
PF-1cL Coil, Leads and Busbar	NSTX-U-CALC-131-001	<u>Calculation of PF1c Lower Coil</u> : Verifies design of the PF-1cL Coil Leads and Bus bar
PF-1cU Leads and Busbars	NSTX-U-CALC-131-002	<u>Calculation of PF1c Upper Leads and Busbar</u> : Verifies design of the PF-1c Upper lead tower
Loads on coils due to Electro-Magnetic forces	NSTX-U-CALC-133-23	<u>Inner PF Coil Electromagnetic Analysis</u> : Provides EM loads on the conductors, for the full range of operating conditions.
Fatigue Stress and Crack Propagation	NSTX-U-CALC-133-24	<u>Inner PF Fatigue and Fracture Mechanics</u> : Verification of design with respect to number of required pulses with worst case assumptions for flaws
Insulation Physical Properties	NSTX-U-CALC-133-25	<u>Calculation of Insulation and Coil Winding Pack Orthotropic Properties for Analysis</u> : Determination of insulation properties to to be used for inputs in analysis
Thermal Strains and Stress	NSTX-U-CALC-133-27	<u>Inner PF Coil Thermal Analysis</u> : Evaluates the thermal stresses and strains associated with thermal excursions due to the resistive heating and the differential layer to layer cooling
PF1 Loads on Leads due to Electro-Magnetic forces	NSTX-U-CALC-133-28	<u>Summary of Loads for PF1 Leads and Busbar</u> : Evaluates the loads on the PF1 busbar connections and provides interface loads for evaluation of coils stresses

Prototype Coils Evaluated Vendors and Validated Design



- The four prototypes provided a basis to evaluate vendor quality, both the process and final product.
- The coil prototyping and testing effort was designed to validate improvements made in design and manufacturing that were based on lessons learned.
- The prototype evaluation demonstrated that the new design has generous margins with respect to preventing a repeat of the initial layer to layer electrical coil failure. The evaluation included:
 - Mechanical Inspection, metrology and hydrostatic testing
 - Low power, high voltage, and high power tests
 - Coil sectioning for visually examined
 - Turn-to-turn and turn-to-ground insulation of sectioned coils successfully tested

Extensive Electrical Testing Program For Prototype



- Low power electrical testing (high pot, megger, surge testing, impedance)
- High power tests (2 coils) simulating NSTX-U operation, successfully completed
- Low power electrical tests repeated and no change observed in coil properties after high power testing
- Coils sectioned, visually examined to confirm good VPI
- High voltage testing performed on turn-to-turn and turn-to-ground insulation of both halves of sectioned coil demonstrated high Safety Factor, $SF=150$ min Turn to Turn, $SF=20$ min Layer to Layer with no breakdown
- High voltage testing was successfully repeated after Corona testing to validate long term durability of insulation


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All Chits Have Been Closed

Chits closed following FDR

Chit Resolution Report: [Report Link](#)

 **National Spherical Torus eXperiment Upgrade**

**Chit Resolution Report
For Inner PF Coils**

NSTX-U-REC-096-01

Prepared By:

Michael Kalish

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Date: 2019/01/22 16:40:31
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Approved By:

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Responsible Engineer

Approved By:

Yuhu Zhai

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Date: 2019/01/23 11:53:23 +05'00'

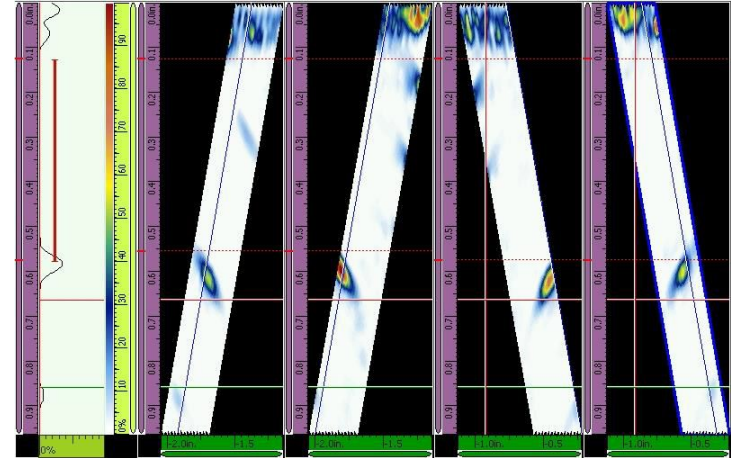
Project Engineer

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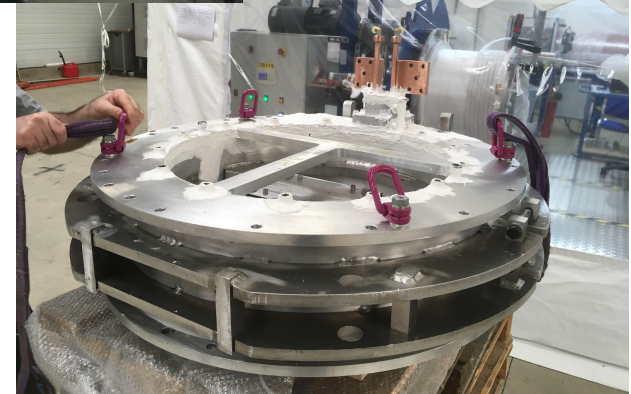
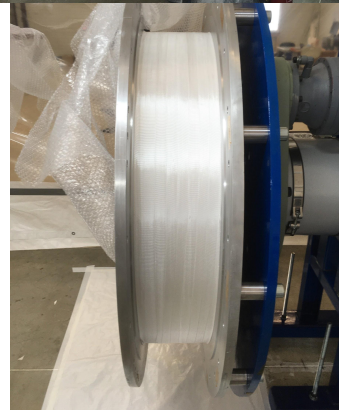
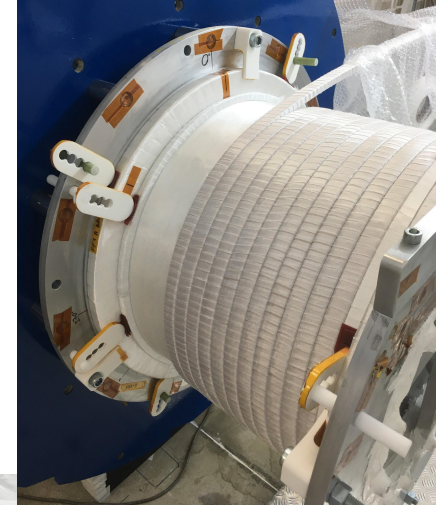
Fabrication

- Long lead items fabricated in advance and provided at award of contract
 - G11 Filler Pieces provided
 - Conductor purchased from Luvata in Finland 100% UT Inspection
 - Conductor sand blasted and primed by ICAS / Tratos in Italy
 - Co-wound glass / Kapton tape assembled and fully inspected at PPPL



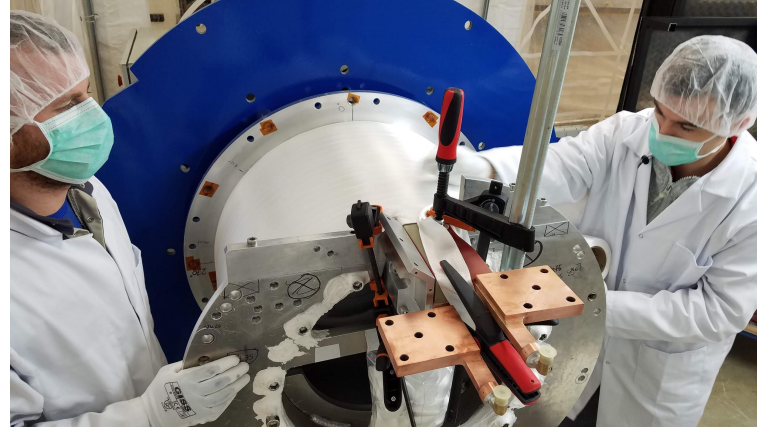
Fabrication

- Fabrication proceeding at Sigmaphi
- Sigmaphi rented a dedicated building for our project
- Two clean rooms established for two winding lines
- Contract requires team of 2 technicians per winding line along with dedicated supervising engineer

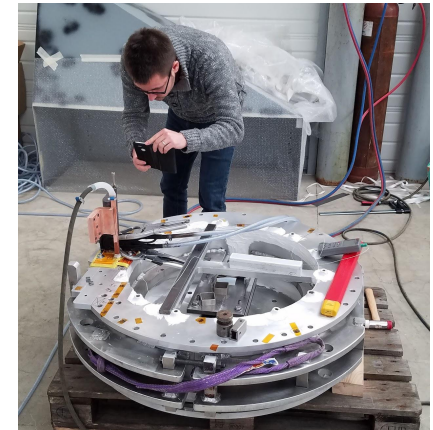
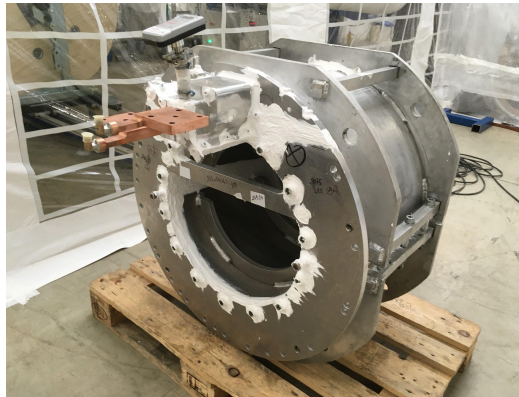


Fabrication

- Of six coils two are wound and in their molds preparing for Vacuum Impregnation
- Two more coils are in the process of being wound
- Sigmaphi bought new equipment dedicated to our project including a new oven, mixing tank and electrical testing equipment
- There have been schedule delays due to issues with Sigmaphi subcontractors but quality has been maintained



Video
Winding
PF1A
Coil
[LINK](#)



NCRs and ECNs During Coil Fabrication To Date

- **NCRs**
 - 4096: Solder for water fitting met European chemistry standard instead of ASTM standard, no impact, accept as is
 - 4077: Small deviations in sizes of G11 filler pieces, no impact, accept as is

- **ECNs**
 - 8298: Change in reference dimensions on G11 Filler pieces to allow for fabrication from 3D models, fix dimension to center flag hole, rotate one water fitting on PF1b
 - 8321: Change in measurement requirement while winding for sigmaphi to determine where the center turn is to more accurately locate the flag

Risk Classification: A-1 4096

Disposition: ☐ Rework ☐ Repair ☒ Use As Is ☐ Return to Vendor ☐ Scrap

The solder certification meets the European standard instead of the ASTM Standard. The difference is insignificant and has does not negatively effect the solder joint. Furthermore the prototype was made using this solder qualifying it for use on the production coils.

Actions to Minimize Recurrence:
N/A. It is acceptable to continue using this material

For rework or repair, fill in cost to PPPL: \$ Total: No Cost

Dispositioned By	Mike Kalish	<small>Digitally signed by Mike Kalish Date: 2020.02.10 20:05:26 -05'00'</small>
QA/QC Concurrence	Kevin Cortes	<small>Digitally signed by Kevin Cortes Date: 2020.02.10 22:08:11 -05'00'</small>
Responsible Engineer (A-1, A-2, & A-3)	Steve Raftopoulos	<small>Digitally signed by Steve Raftopoulos Date: 2020.02.11 08:21:54 -05'00'</small>
Technical Authority (A-1 & A-2)	G Douglas Loesser	<small>Digitally signed by G Douglas Loesser Date: 2020.02.11 08:33:14 -05'00'</small>
Other Concurrence (Specify Title)	Yuhu Zhai	<small>Digitally signed by Yuhu Zhai Date: 2020.02.12 13:53:27 -05'00'</small>
Project Engineer	Robert Ellis	<small>Digitally signed by Robert Ellis Date: 2020.02.12 14:29:21 -05'00'</small>
Chief Engineer		
QA/QC Verification of Completion	N/A	<small>F Malinowski 2020.02.12 14:42:21 -05'00'</small>
QA/QC Head Approval of Closure	Surendra N. Tiwari	<small>Digitally signed by Surendra N. Tiwari Date: 2020.02.12 14:50:18 -05'00'</small>

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Project Risks are Actively Being Managed

Risk	Score (1-81)	Open/Retired	Risk Retirement Event
If vendors cannot perform in the fabrication of PF1B and PF1C	28	RETIRED	
If the vendor quotes for production coils are higher due to their prototyping experience then the current basis of estimate will be low	25	RETIRED	Production coil contract award
If fabricated coils are damaged or lost in transit	21	OPEN	end of assembly
If a coil has an extreme exothermic reaction during fabrication	21	OPEN	Completion of Fabrication
If vendor(s) bid quotes for winding coil cannot meet currently assumed schedule	20	RETIRED	Award of coil contract
If vendors have performance issues that threatens either product quality or schedule in the fabrication of PF coils	20	OPEN	End of coil fabrication

Project Risks are Actively Being Managed

Risk	Score (1-81)	Open/Retired	Risk Retirement Event
If production coil fails pre- or post-vpi electrical acceptance tests	20	OPEN	Successful coil test
If the new Inner PF coils' terminals are in different locations than the original coils' terminals as determined by field fit	20	RETIRED	Completion of machine assembly
If the method to separate the prototype coils from their temporary winding mandrels causes damage to a coil	18	RETIRED	
If a coil is damaged during finished machining	18	RETIRED	Completion of Fabrication
If the production coil fails pre-vpi electrical tests	16	RETIRED	Coil install
If there is a failure in existing power system component(s) to support coil testing	16	OPEN	End of coil testing

Project Risks are Actively Being Managed

Risk	Score (1-81)	Open/Retired	Risk Retirement Event
If there are delays in awarding/completing conductor grit blast/prime	16	RETIRED	Award Completion
Evaluation of prototype coils delays	16	RETIRED	Evaluation Completion
If there is a PF Coil Shipping Delay	16	RETIRED	Receipt of coils
If foreign vendor surveillance is more challenging (multiple shifts, time-away limits,...), the lack of support may result in schedule delays.	16	RETIRED	Receipt of coils at PPPL
If less than three coil manufacturing facilities are available then we will not have parallel winding lines	15	RETIRED	Completion of procurement
If vendor quality decreases during production coils relative to prototype phase	15	RETIRED	Receipt of coils at PPPL

Project Risks are Actively Being Managed

Risk	Score (1-81)	Open/Retired	Risk Retirement Event
If coil is damaged during finished machining or assembly	15	OPEN	end of assembly
If all the prototype testing failed then we have to re-evaluate the design and the process	15	RETIRED	
M8-1 & M8-2, If a flaw in the design/analysis/fabrication of magnet system component is found.	15	OPEN	Completion of component testing
if the schedule does not account for cultural differences (international holidays, work week differences,...), then the schedule may be overly optimistic	15	RETIRED	Award Completion
Two prototype coils fail post-acceptance destructive tests	12	RETIRED	Coil install

Project Risks are Actively Being Managed

Risk	Score (1-81)	Open/Retired	Risk Retirement Event
If a vendor can not deliver due to unforeseen event in the middle of production then we will move production to another vendor and schedule will be increased	12	RETIRED	Receipt of coils at PPPL
If additional design risks to coils (CTD results etc.)	12	RETIRED	FDR
If problems occur with PF test stand during PF coil testing	12	OPEN	Completion of testing
If materials are damaged or lost in transit and we have to order more	12	RETIRED	receipt of coils
If the Polar Region structures design reviews reveal a problem for the coils	9	RETIRED	FDR for Machine Core Structures
PF-1A Proto tooling delayed	5	RETIRED	RETIRED

Project Risks are Actively Being Managed

Risk	Score (1-81)	Open/Retired	Risk Retirement Event
If vendor or several vendors can fabricate PF1A coil in addition to PF1b and PF1C	5	RETIRED	completion of fabrication
If we start the early grit/blast/prime effort	4	RETIRED	Award Completion
If PPPL consolidates coil winding vendors	3	RETIRED	Award Completion

FMECA - Inner PF Coils (I)

System	Failure Mode	Failure Cause	Failure Effect	R	Detection/ Mitigation System (1)	Detection/ Mitigation System (2)	Detection/ Mitigation System (3)	R_R
PF-1a Coils	Water leak at inlet	Fitting or hose failure	Potential loss of cooling; coil grounded; damage to coil leads or nearby components	12	FCPC Ground Fault Detection	CWS Flow and Temperature Instrumentation	Vessel and Diagnostic Grounds	6
PF-1a Coils	Water leak at outlet	Fitting or hose failure	coil grounded; damage to coil leads or nearby components	12	FCPC Ground Fault Detection	CWS Flow and Temperature Instrumentation	Vessel and Diagnostic Grounds	6
PF-1a Coils	Bending of coil lead flags	Excessive load on the leads	Failure of lead flags	12	DCPS Software	None	None	4
PF-1a Coils	Leads Bend	Excessive load away from the midplane is larger than preload	Damage to leads; may be severe up to a requiring replacement	12	DCPS Software	None	None	4
PF-1b Coils	Arc to ground at coil terminals	Water leak or item falling across leads; transient over-voltage condition	Damage to leads; may be severe up to a requiring replacement	12	FCPC Ground Fault Detection	None	None	2
PF-1b Coils	Water leak at inlet	Fitting or hose failure	Potential loss of cooling; coil grounded; damage to coil leads or nearby components	12	FCPC Ground Fault Detection	CWS Flow and Temperature Instrumentation	Vessel and Diagnostic Grounds	6

FMECA - Inner PF Coils (II)

System	Failure Mode	Failure Cause	Failure Effect	R	Detection/ Mitigation System (1)	Detection/ Mitigation System (2)	Detection/ Mitigation System (3)	R_R
PF-1b Coils	Water leak at outlet	Fitting or hose failure	coil grounded; damage to coil leads or nearby components	12	FCPC Ground Fault Detection	CWS Flow and Temperature Instrumentation	Vessel and Diagnostic Grounds	6
PF-1b Coils	Excessive resistive heating of connection at coil/bus work interface	Loss of preload of bolted connections	Damage to electrical faces of coil	12	None	None	None	4
PF-1b Coils	Bending of coil lead flags	Excessive load on the leads	Failure of lead flags	12	DCPS Software	None	None	4
PF-1b Coils	Leads Bend	Excessive load away from the midplane is larger than preload	Damage to leads; may be severe up to a requiring replacement	12	DCPS Software	None	None	4
PF-1c Coils	Blockage of coil cooling channel	debris	coil temperature ratchets, damaging insulation	12	CWS Flow and Temperature Instrumentation	None	None	2
PF-1c Coils	Water leak at inlet	Fitting or hose failure	Potential loss of cooling; coil grounded; damage to coil leads or nearby components	12	FCPC Ground Fault Detection	CWS Flow and Temperature Instrumentation	Vessel and Diagnostic Grounds	4
PF-1c Coils	Water leak at outlet	Fitting or hose failure	coil grounded; damage to coil leads or nearby components	12	FCPC Ground Fault Detection	CWS Flow and Temperature Instrumentation	Vessel and Diagnostic Grounds	4

FMECA - Inner PF Coils (III)

System	Failure Mode	Failure Cause	Failure Effect	R	Detection/ Mitigation System (1)	Detection/ Mitigation System (2)	Detection/ Mitigation System (3)	R_R
PF-1c Coils	Bending of coil lead flags	Excessive load on the leads	Failure of lead flags	12	DCPS Software	None	None	4
PF-1a Coils	Arc to ground at coil terminals	Water leak or item falling across leads; transient over-voltage condition	Damage to leads; may be severe up to a requiring replacement	8	FCPC Ground Fault Detection	None	None	2
PF-1a Coils	Arc across coil terminals	Water leak or item falling across leads; transient over-voltage condition	Damage to leads; may be sufficiently severe to require replacement	8	Shorted Turn Protection System	None	None	2
PF-1a Coils	Excessive resistive heating of connection at coil/bus work interface	Loss of preload of bolted connections	Damage to electrical faces of coil	8	None	None	None	4
PF-1a Coils	Internal coil turn-to-turn failure	Insulation failure due to manufacturing error; transient over-voltage condition	Coil is inoperative, coil must be replaced	8	None	None	None	8
PF-1b Coils	Arc across coil terminals	Water leak or item falling across leads; transient over-voltage condition	Damage to leads; may be sufficiently severe to require replacement	8	Shorted Turn Protection System	None	None	2

FMECA - Inner PF Coils (IV)

System	Failure Mode	Failure Cause	Failure Effect	R	Detection/ Mitigation System (1)	Detection/ Mitigation System (2)	Detection/ Mitigation System (3)	R_R
PF-1b Coils	Internal coil turn-to-turn failure	Insulation failure due to manufacturing error; transient over-voltage condition	Coil is inoperative, coil must be replaced	8	None	None	None	8
PF-1c Coils	Arc to ground at coil terminals	Water leak or item falling across leads; transient over-voltage condition	Damage to leads; may be severe up to a requiring replacement	8	FCPC Ground Fault Detection	None	None	2
PF-1c Coils	Arc across coil terminals	Water leak or item falling across leads; transient over-voltage condition	Damage to leads; may be sufficiently severe to require replacement	8	Shorted Turn Protection System	None	None	2
PF-1c Coils	Excessive resistive heating of connection at coil/bus work interface	Loss of preload of bolted connections	Damage to electrical faces of coil	8	None	None	None	4
PF-1c Coils	Internal coil turn-to-turn failure	Insulation failure due to manufacturing error; transient over-voltage condition	Coil is inoperative, coil must be replaced	8	Shorted Turn Protection System	None	None	8

FMECA - Inner PF Coils (V)

System	Failure Mode	Failure Cause	Failure Effect	R	Detection/ Mitigation System (1)	Detection/ Mitigation System (2)	Detection/ Mitigation System (3)	R_R
PF-1a Coils	Blockage of coil cooling channel	debris	coil temperature ratchets, damaging insulation	4	CWS Flow and Temperature Instrumentation	None	None	2
PF-1a Coils	Ground Wall insulation failure	Mechanical damage during maintenance or operations; inadvertent over-voltage condition during operations or testing	Excessive current to ground, or arcing, during operations; may degrade over time; may mandate replacement	4	FCPC Ground Fault Detection	None	None	4
PF-1a Coils	Magnet ground insulation failure	slings develop resonance or large displacement with EM forces, and start slapping against the magnet insulation	leakage through ground insulation, may mandate major repair or replacement	4	FCPC Ground Fault Detection	None	None	4
PF-1a Coils	Ground insulation degradation	Excessive heat from bakeout due to issue with manufacture or installation of the microtherm insulation	Coil cannot pass high pot testing, excessive leakage current, coil may need to be replaced	4	Center Stack Coil Thermocouples	None	None	4

FMECA - Inner PF Coils (VI)

System	Failure Mode	Failure Cause	Failure Effect	R	Detection/ Mitigation System (1)	Detection/ Mitigation System (2)	Detection/ Mitigation System (3)	R_R
PF-1b Coils	Blockage of coil cooling channel	debris	coil temperature ratchets, damaging insulation	4	CWS Flow and Temperature Instrumentation	None	None	2
PF-1b Coils	Ground Wall insulation failure	Mechanical damage during maintenance or operations; inadvertent over-voltage condition during operations or testing	Excessive current to ground, or arcing, during operations; may degrade over time; may mandate replacement	4	FCPC Ground Fault Detection	None	None	4
PF-1b Coils	Magnet ground insulation failure	slings develop resonance or large displacement with EM forces, and start slapping against the magnet insulation	leakage through ground insulation, may mandate major repair or replacement	4	FCPC Ground Fault Detection	None	None	4
PF-1b Coils	Ground insulation degradation	Excessive heat from bakeout due to issue with manufacture or installation of the microtherm insulation	Coil cannot pass high pot testing, excessive leakage current, coil may need to be replaced	4	Center Stack Coil Thermocouples	None	None	4

FMECA - Inner PF Coils (VII)

System	Failure Mode	Failure Cause	Failure Effect	R	Detection/ Mitigation System (1)	Detection/ Mitigation System (2)	Detection/ Mitigation System (3)	R_R
PF-1c Coils	Ground Wall insulation failure	Mechanical damage during maintenance or operations; inadvertent over-voltage condition during operations or testing	Excessive current to ground, or arcing, during operations; may degrade over time; may mandate replacement	4	FCPC Ground Fault Detection	None	None	4
PF-1c Coils	Ground insulation degradation	Excessive heat from bakeout transferred through the PF-1c can	Coil cannot pass high pot testing, excessive leakage current, coil may need to be replaced	4	Center Stack Coil Thermocouples	None	None	4
PF-1a Coils	Delamination of turn to turn insulation	gradual loss of sling preload	Motion of conductors in the matrix of the insulation	0	None	None	None	0
PF-1a Coils	A gouge develops in the magnet's top surface	A burr, or machining ridge, digs into the top surface of the magnet during magnet radial expansion	produces weakened thermal/electrical insulation in one spot	0	None	None	None	0
PF-1b Coils	Delamination of turn to turn insulation	Mechanical (thermal, EM) during operations	Motion of conductors in the matrix of the insulation	0	None	None	None	0

FMECA - Inner PF Coils (VIII)

System	Failure Mode	Failure Cause	Failure Effect	R	Detection/ Mitigation System (1)	Detection/ Mitigation System (2)	Detection/ Mitigation System (3)	R_R
PF-1b Coils	A gouge develops in the magnet's top surface	A burr, or machining ridge, digs into the top surface of the magnet during radial expansion	produces weakened thermal/electrical insulation in one spot	0	None	None	None	0
PF-1c Coils	Delamination of turn to turn insulation	Mechanical (thermal, EM) during operations	Motion of conductors in the matrix of the insulation	0	None	None	None	0
PF-1c Coils	During radial expansion of the PF1c magnet, a gouge develops in the magnet's top surface	A burr, or machining ridge, on the mounting flange digs into the PF1c magnet	produces weakened thermal/electrical insulation in one spot	0	None	None	None	0

40 FMs, all but three mitigated to acceptable level.

Key mitigations

- DCPS to limit loads to the design basis
- FCPC ground fault monitors
- Shorted turn protection system
- Cooling water interlocks

Internal turn-to-turn faults challenging to defend as “extremely unlikely” ($<10^{-4}$ /yr) given history of fusion program with magnets. Flagged as “unlikely”

Outline

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3. Requirements and Interfaces
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8. Quality, Environmental, Safety, and Health
9. Summary

QA & Fabrication Oversight / ES&H

- Extensive prototyping effort qualified vendors and provided trial run for QA oversight
- PPPL QA & PPPL Engineering attend on-site Manufacturing Readiness Review
- Resident PPPL Engineering is on site for coil manufacturing
- Local subcontracted QA Engineers assure on-site PPPL QA presence.
- Resident Engineering representative is supplemented by visits from cognizant engineer
- The oversight plan for the production coils is a dramatic increase in PPPL presence compared to the oversight provided during the original PF1 fabrication
- PPPL representatives may stop work when required to resolve quality or safety issues
- Steps are taken to ensure coil fabrication does not subject employees to hazards at Sigmaphi
 - Work hazards at External Vendors mitigated with vendor oversight training and use of Job Hazard Analysis
 - Subcontract requires site-specific safety plans for PPPL workers.
 - During Prototype production PPPL stopped work at a vendor and removed personnel in response to potential safety issues returning only after confirmation issues were resolved

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Summary

- Requirements have been met through design and analysis and then verified with prototyping and testing
- Interfaces are considered in the design and documented in the ICDs.
- All chits related to the inner-PF replacement job are closed
- Risks are mitigated through:
 - Inner-PF prototype program to prove and refine manufacturing techniques and down select the highest quality manufacturer
 - Prototype testing and inspection
 - On-site presence during manufacturing
 - Extensive testing of final coils
- Safety practices such as JHA extended to work at external vendors