

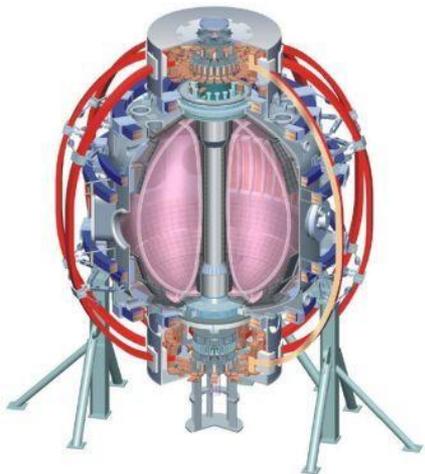
# Divertor surface temperature measurements with a high-speed camera and NIR filters

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*and the NSTX Research Team*

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November 8, 2010**



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# Abstract

IR band-pass filters ( $>720$  nm or  $>900$  nm) were used with a Phantom v7.3 high-speed camera to try to measure the surface temperature of plasma facing components and the Liquid Lithium Divertor (LLD) in NSTX. The present camera looks through an upper port with a view of more than half of the lower divertor. With several megawatts of RF heating power, the observed surface temperature increased by  $\sim 700$  °C in a localized region magnetically connected to the RF antenna. Such a wide-angle, high-speed (up to  $10^4$  fps) IR system could also evaluate the thermal response to transient events such as ELMs and disruptions, which can cause large, uneven heat loads over a wide area of the divertor. The rise/fall time during power transients and emission spectroscopy diagnostics were used to help distinguish plasma IR line emission from surface blackbody emission. The entire system has been calibrated with a blackbody source from 350 to 700 °C.

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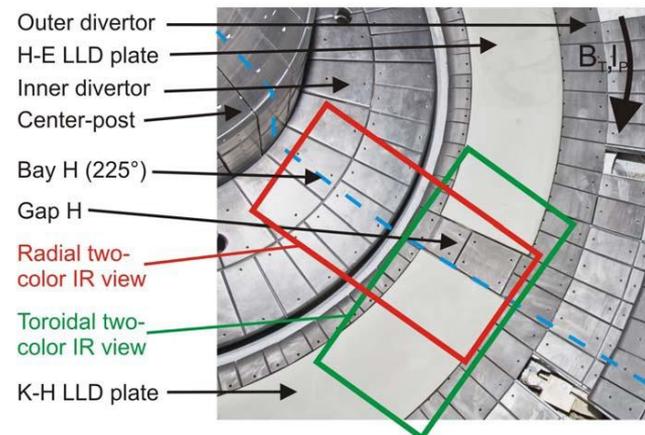
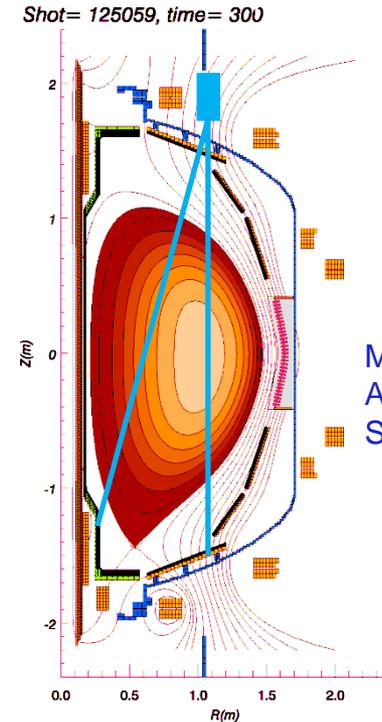
# Motivation for NIR high-speed camera on NSTX

- Want to measure temperature of divertor over wide area
  - Will hot spots reach melting point on liquid lithium divertor (LLD)?
  - Full coverage needed for next-generation devices with high-Z divertors in which any melting can contaminate plasmas
- Can we measure surface temperature with a visible camera and near-infrared (NIR) filter?
- Several potential advantages
  - LLD cameras have FOV of >50% of lower divertor
    - Much wider view than current NSTX IR cameras
    - Observe full toroidal impact of non-axisymmetric loads
  - Framing rate of ~50 kHz with full FOV
    - Up to 500 kHz with smaller FOV
    - Could image some transient events as they occur
- NIR background light could cause difficulties<sup>†</sup>

<sup>†</sup>Soukhanovskii, V.A. 2008. "Near-infrared spectroscopy for burning plasma diagnostic applications." *Rev. Sci. Instrum.* 79, 10F539.

# Existing ORNL infrared cameras on NSTX

- Two slow IR cameras
  - 30 Hz
  - 0.2 m – 1.2 m radial view
  - $\sim 15^\circ$  toroidal view
  - View upper (Bay G) and lower divertor (Bay I)
- A fast dual-band IR camera
  - 4-6  $\mu\text{m}$  and 7-10  $\mu\text{m}$  bands
  - $\sim 1-6$  kHz
  - $\sim 0.2$  m – 0.85 m radial view
  - $\sim 15^\circ$  toroidal view

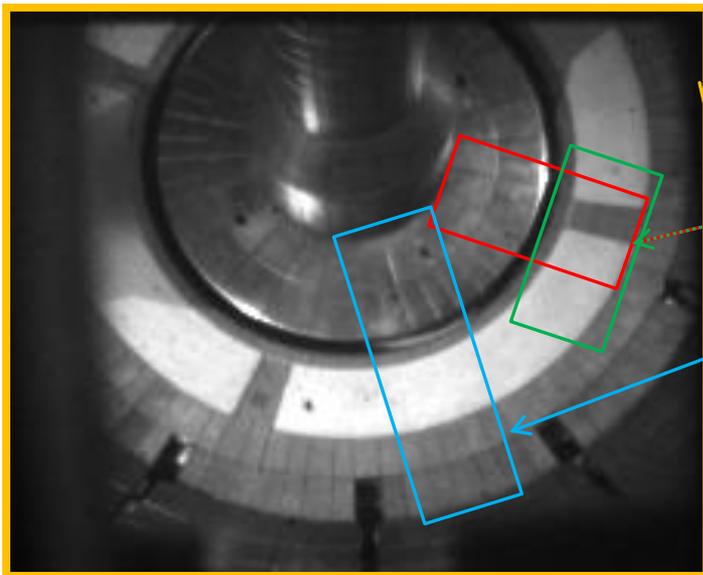
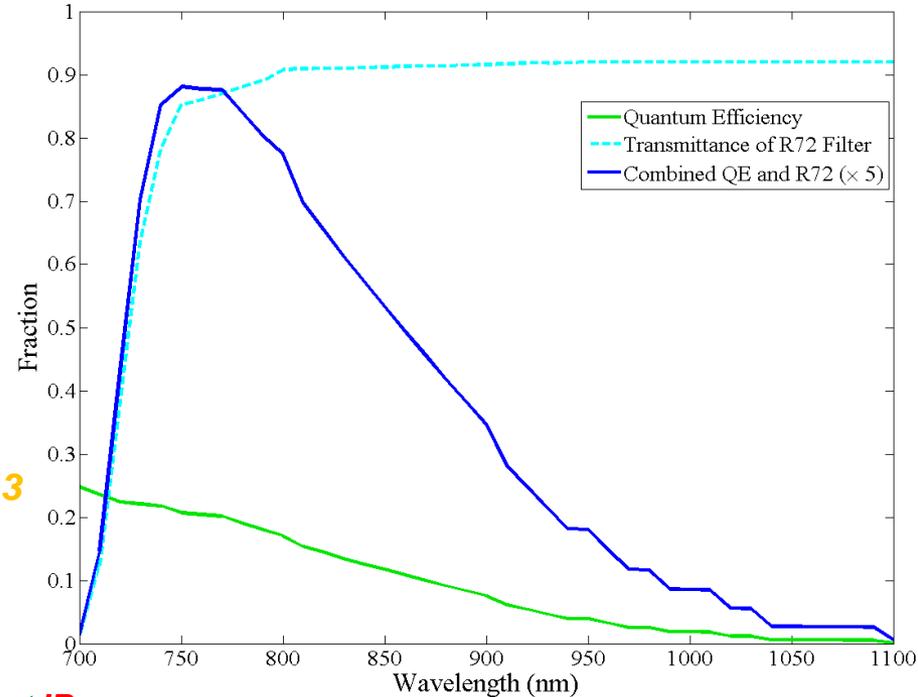


A. McLean.  
5/10/2010.  
PPPL Physics Meeting.

# High-speed camera with NIR filter

- Phantom v7.3
  - Capable of 1  $\mu\text{s}$  exposures
  - FOV: majority of the lower divertor
  - Low spectral responsivity beyond 1100 nm

Response of Phantom v7.3 with 720 nm Filter



Phantom 7.3  
Bay J

Dual-Band Fast IR  
Bay H

Slow IR  
Bay I

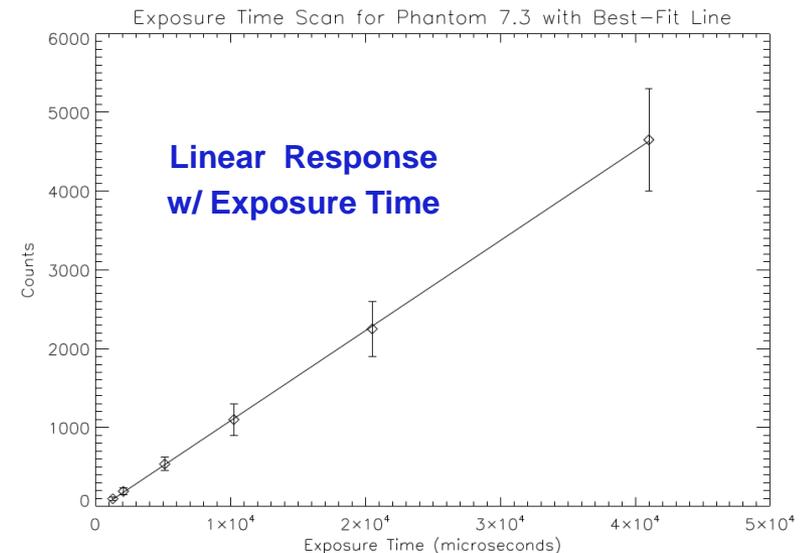
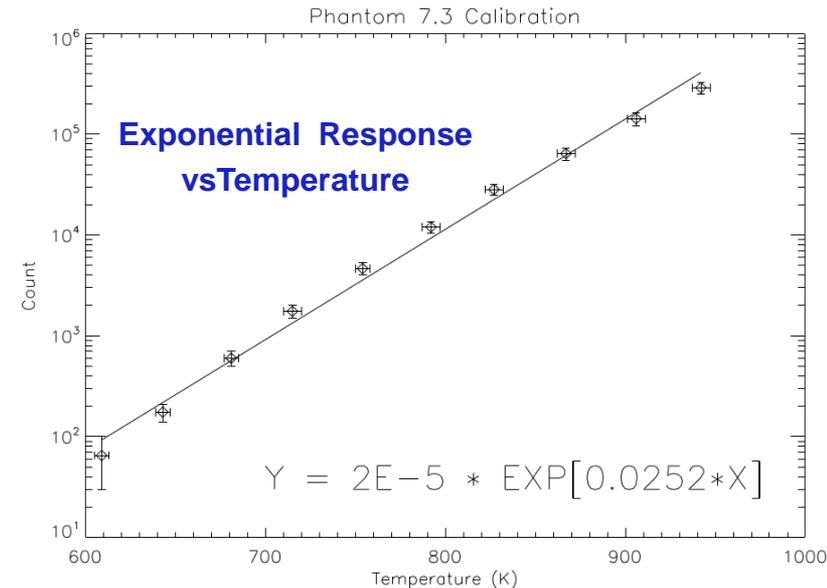
Modified from  
F. Scotti.

## • Filters

- Hoya R72 ( $>720$  nm)
- Hoya RM90 ( $>900$  nm)

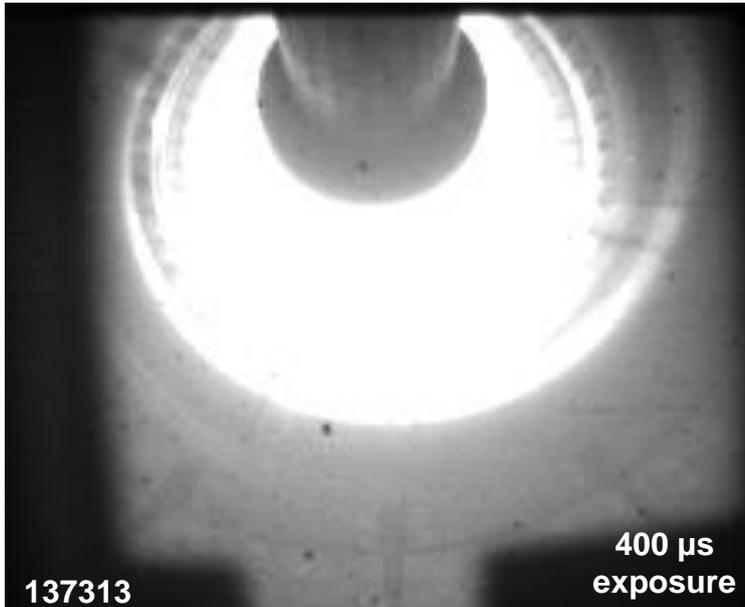
# Benchtop calibration of system

- Calibration
  - 720 nm filter
  - all available optics (filter, lenses, and fiber)
  - 41 ms exposure time
  - 335 °C to 670 °C
- Linear variation w/ exp. time
- Corrections for emissivity or other *in situ* effects difficult to account for
  - Conditions change over time
  - Can't periodically calibrate *in situ* as vessel under vacuum throughout run

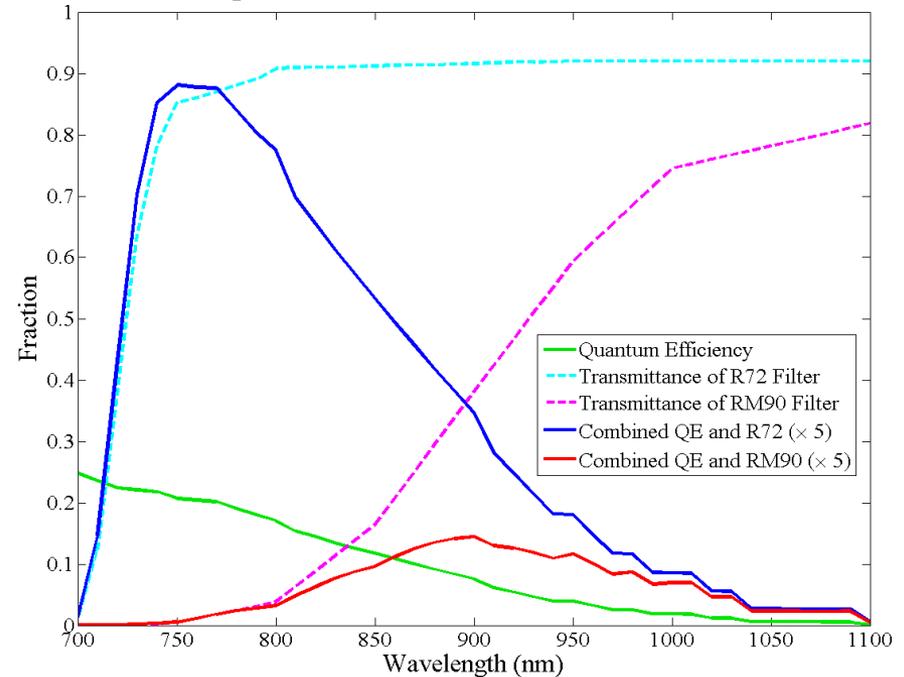


# Change to a higher cutoff filter

720 nm



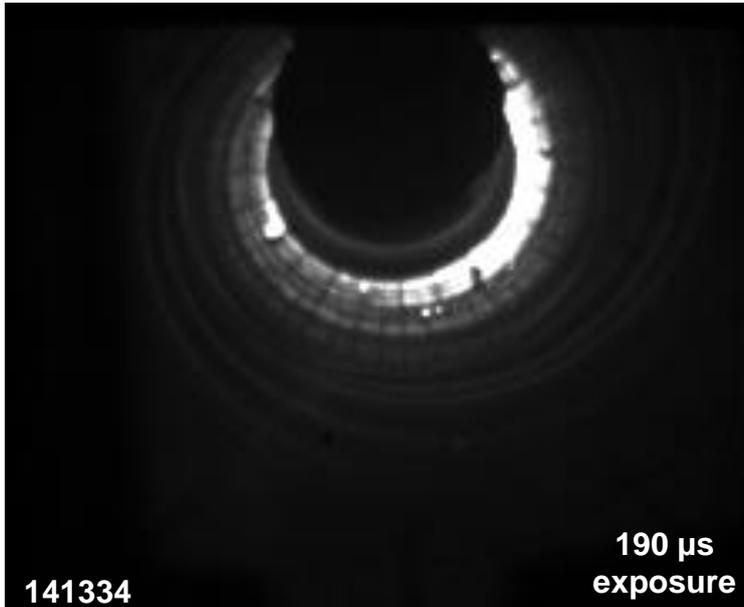
Response of Phantom v7.3 with NIR Filter



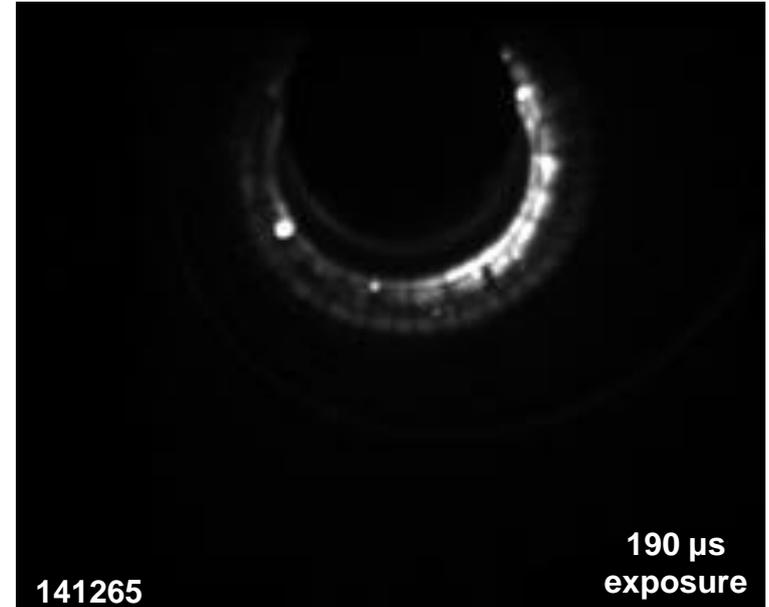
- Potential reduction in background with 900 nm filter w/o losing much thermal light
- Calibration curve modification necessary
  - Currently corrected using blackbody theory
  - Second benchtop calibration may be performed in the future

# Comparison of filters' signal/noise ratios

720 nm



900 nm

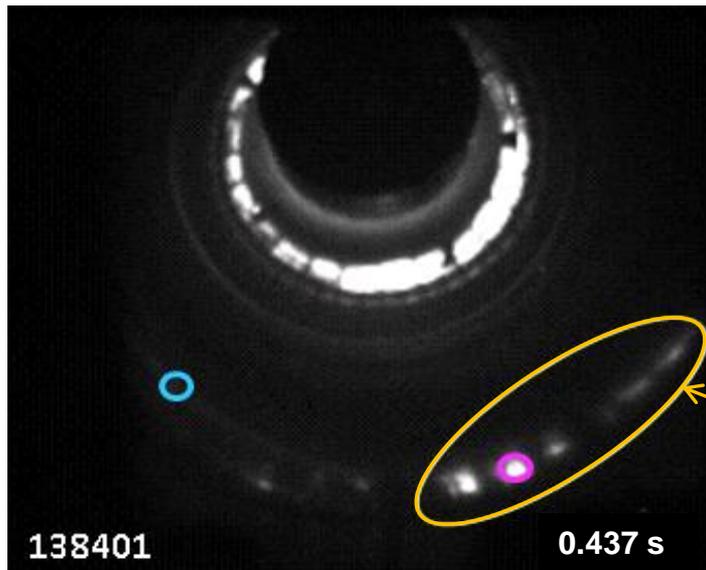


- Clear reduction in amount of light observed for nearly identical shots
- Blackbody curves tell you expected decrease, but this changes with temperature (and thus location)
- Requires data w/ both filters with same shot for best results
  - Second camera w/ both filters and overlapping view available
  - Analysis of data from both cameras with both filters currently underway

# Heating of the divertor by HHFW (1)

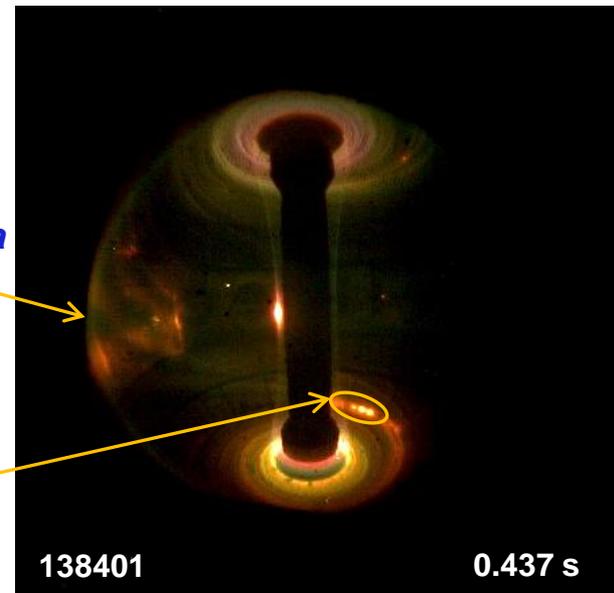
- RF power coupled to SOL plasma
- Hot streak magnetically connected to antennae
- Hot spots on the order of  $10 \text{ cm}^2$
- Previous data showed heat flux  $\sim 3 \text{ MW/m}^2$  †
- Data recorded for 17 shots with 2-3 MW RF power and 2 MW NBI heating on 6/9/10 using 900 nm filter

† Taylor, G. et al. Nov. 5, 2009. "Advances in High Harmonic Fast Wave Physics in NSTX." 51<sup>st</sup> APS DPP Meeting. Atlanta, GA.



RF Antenna

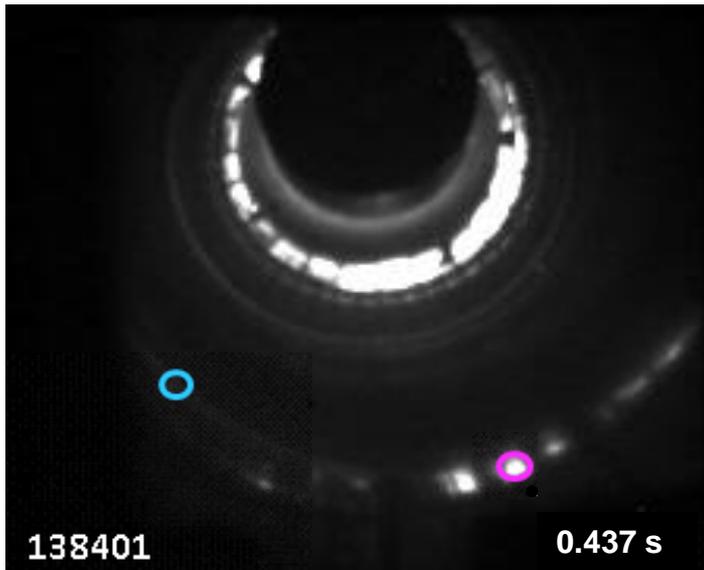
Hot Streak



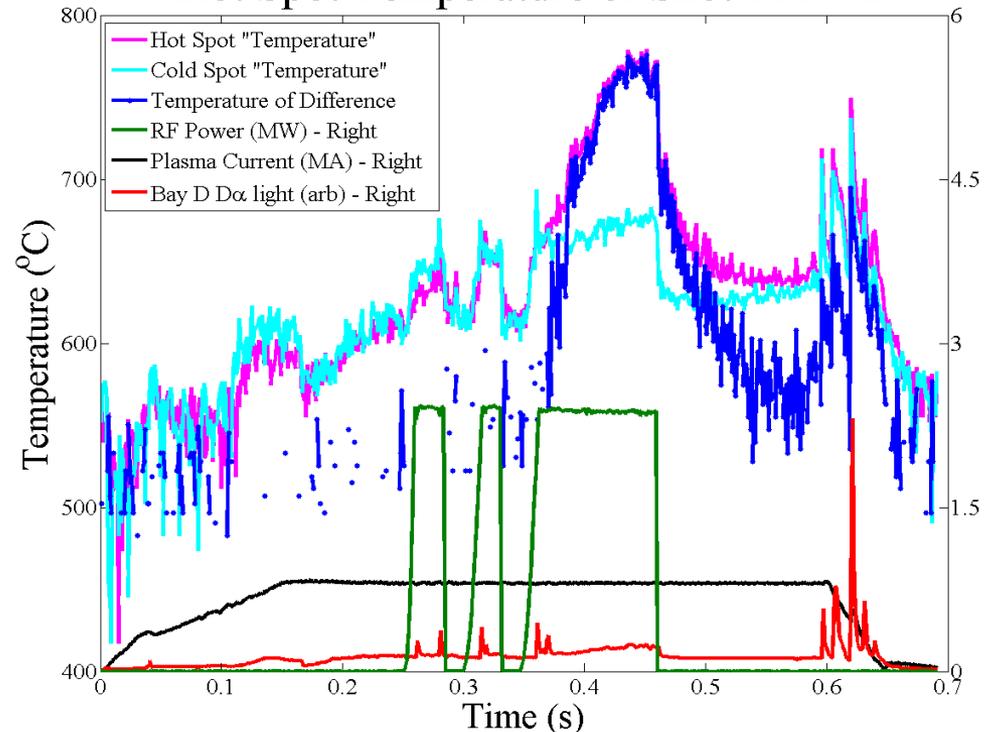
Bay B  
Miro

# Heating of the divertor by HHFW (2)

- Hot spot temperature determined from average counts inside pink circle
- Cold spot “temperature” and counts determined inside blue circle
  - Lies on the same plasma filament as pink circle
- Dark blue temperature determined from difference in counts
- Initial high “background equivalent temperature” before RF



Hot Spot Temperature of Shot 138401



# 1D Heat Diffusion Simulations

- Model

- Heat diffusion equation: 
$$\frac{\partial T}{\partial t} = D \frac{\partial^2 T}{\partial x^2}$$
- 1in. thick ATJ graphite tile
- Constant diffusivity ( $D = 0.34 \text{ cm}^2/\text{s}$ ) & conductivity ( $\kappa = 0.94 \text{ W/cm}^*\text{K}$ )
- Piecewise constant flux that increases during RF
- Zero flux out of tile

- Code

- Explicit Forward Time Centered Space (FTCS) finite difference

$$T_i^{n+1} = T_i^n + \frac{D\Delta t}{(\Delta x)^2} (T_{i+1}^n - 2T_i^n + T_{i-1}^n)$$

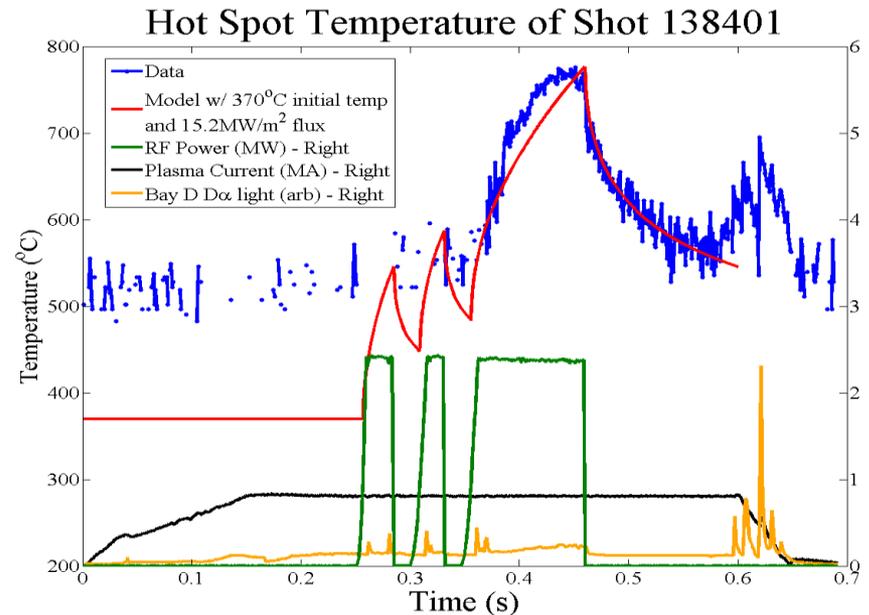
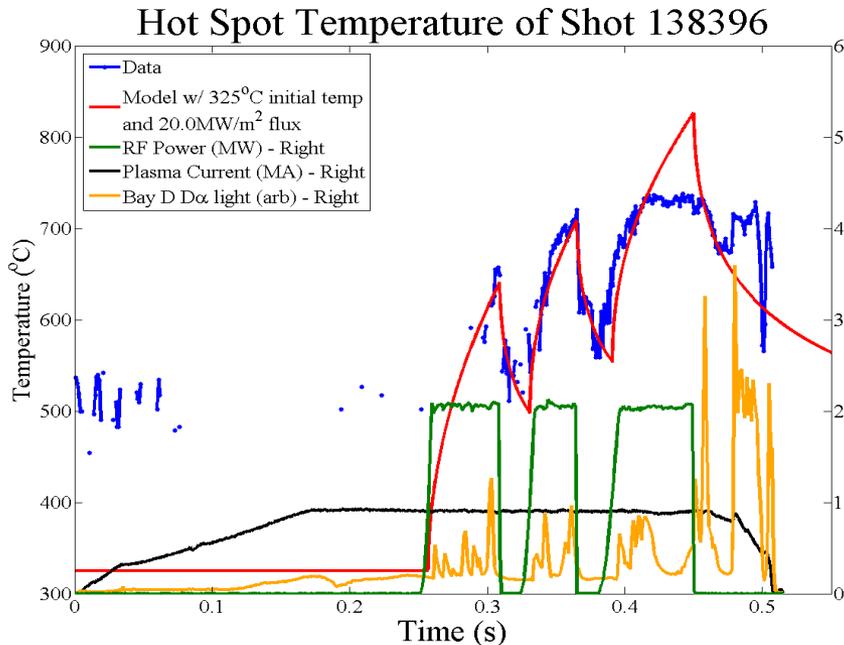
- Neumann boundary conditions

- Top of tile: 
$$T_0^n = T_1^n + \frac{F^n \Delta x}{\kappa}$$

- Bottom of tile: 
$$T_N^n = T_{N-1}^n$$

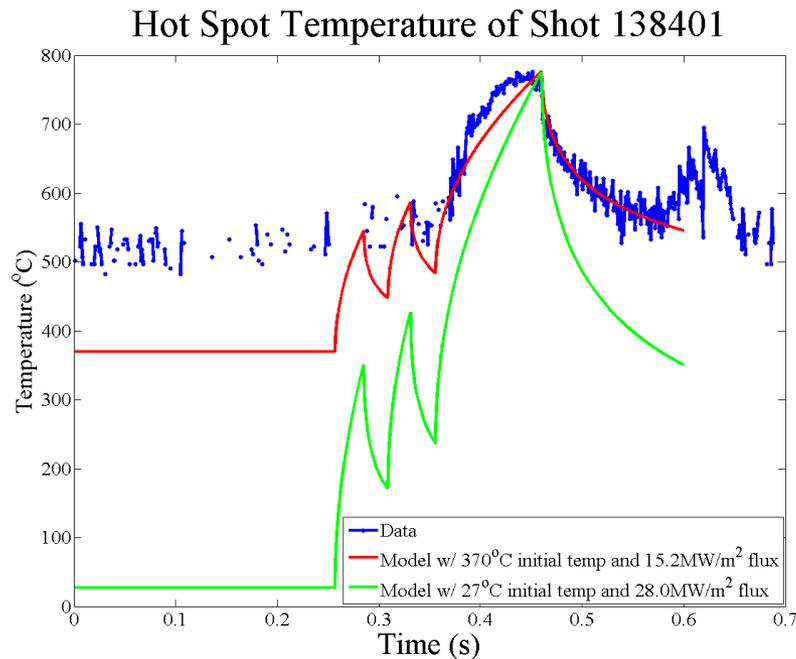
# Results with flux only during RF

- Temperature profile fit well by thermal rise during RF
  - Time dependence of temperature rise and fall
  - Magnitude of relative peaks
- 15-20 MW/m<sup>2</sup> flux
  - Generally matches measurement from ORNL Slow IR camera
- ~320 °C initial temperature seems unrealistic

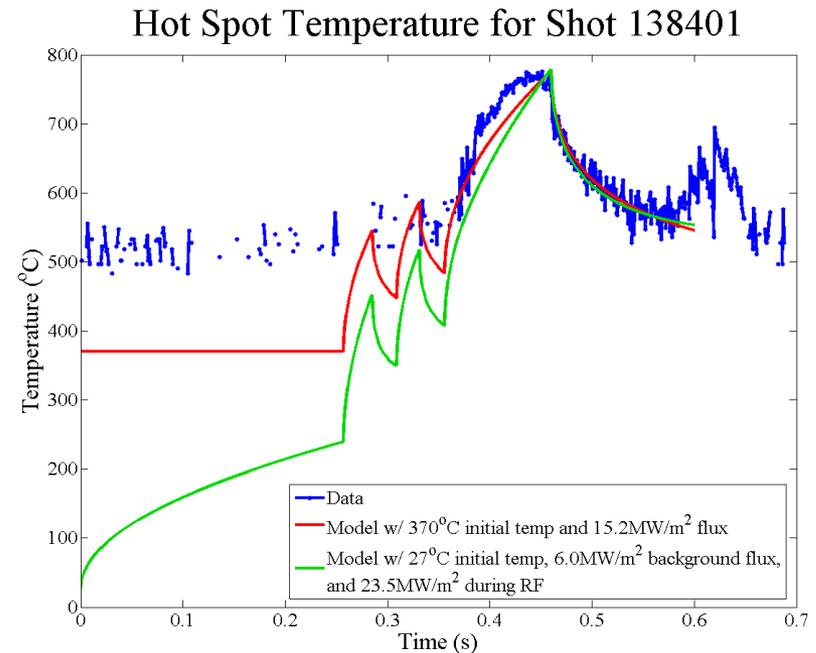


# Results from low initial temperature simulations

- Zero background flux
  - Large 28 MW/m<sup>2</sup> flux needed to reach peak temp
  - Model's rise/fall time too fast



- Constant background flux
  - 6.0 MW/m<sup>2</sup> background flux a little large
  - 23.5 MW/m<sup>2</sup> flux during RF also a little large

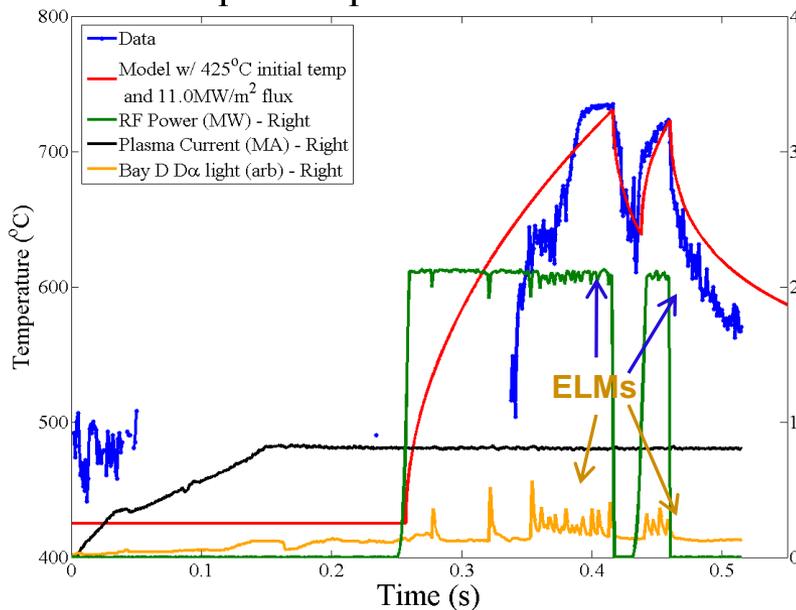


# Some odd thermal signatures

## Shot 138394:

### Rise delayed after RF

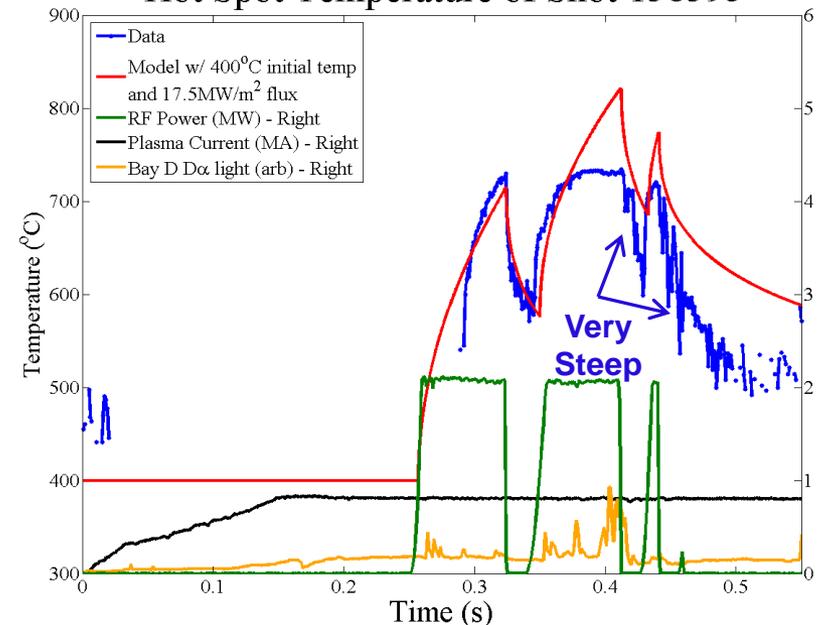
Hot Spot Temperature of Shot 138394



## Shot 138395:

### Rise/fall too steep

Hot Spot Temperature of Shot 138395



- Possible causes

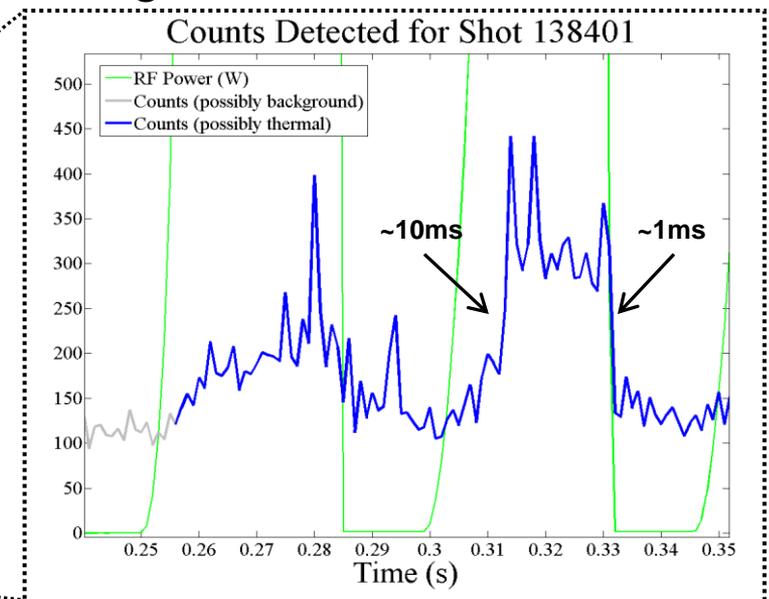
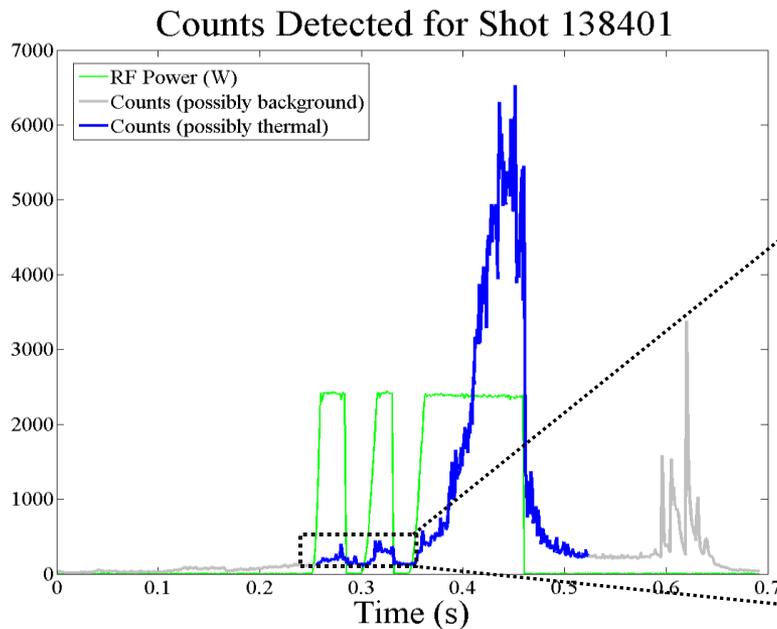
- Movement of “RF strike point” could cause delay?
- ELMs?
- Additional background light?

# Sources & time dependence of background

- Several possible sources
  - Plasma line emission
  - Bremsstrahlung
  - Reflection from breakdown filament (measured to be small)

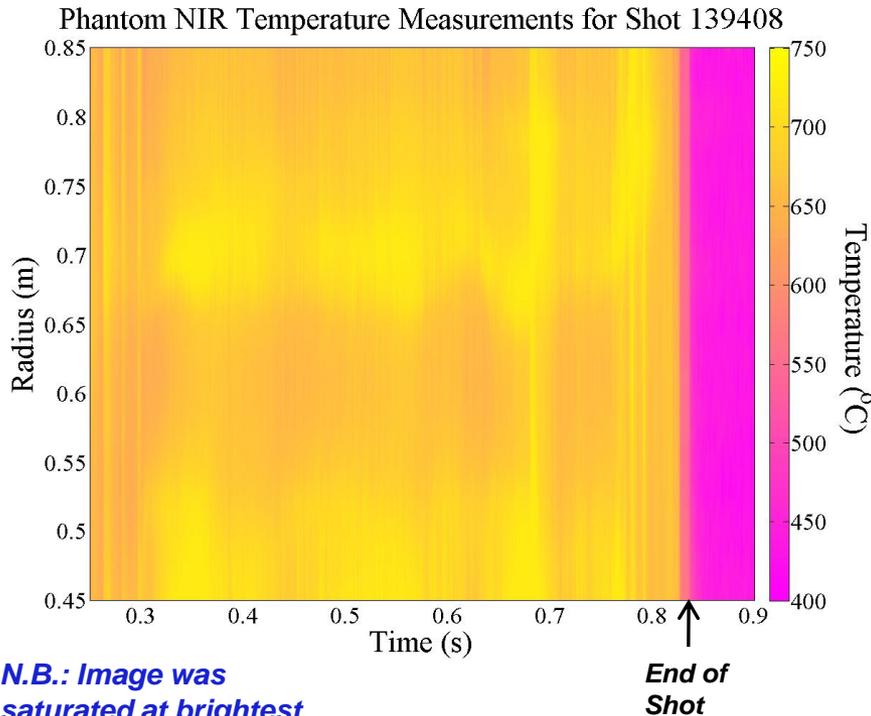
- Signal before RF is 1-10% of signal during RF

- Increases during RF?
- Rise/fall times seem too fast for heating



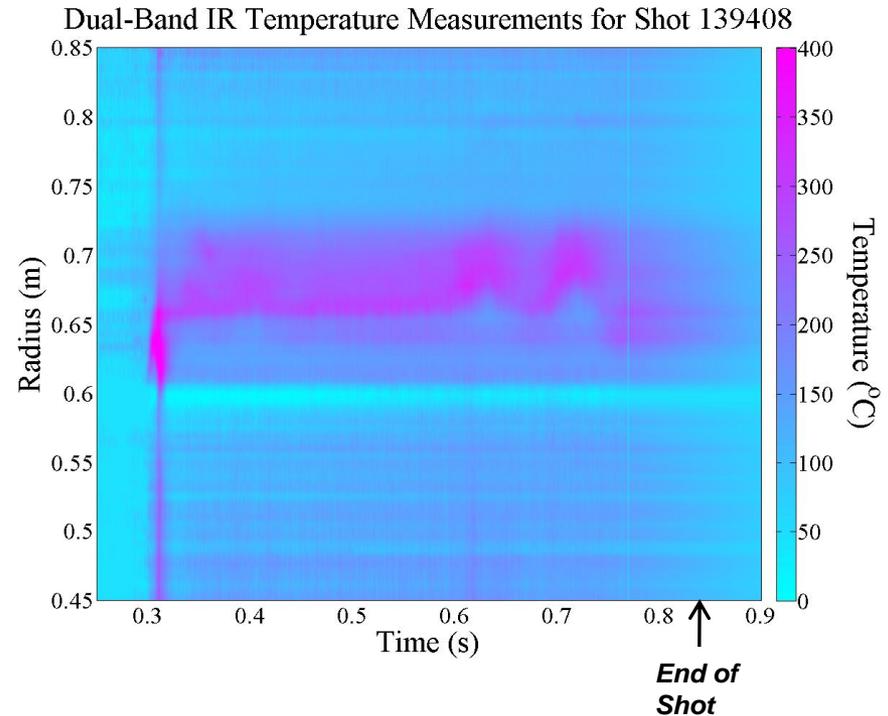
# Comparison of Measurements to ORNL Dual-Band IR Camera (1)

## Phantom v7.3 w/ 900 nm Filter and 990 $\mu$ s exposure time



*N.B.: Image was saturated at brightest locations.*

## ORNL dual-band camera [†]



[†] Unpublished data from A.G. McLean. Received 10/8/2010.

- Same shot and approximate location
- No RF Heating
- Strike point on LLD (between 0.65 m to 0.85 m)
- CHI gap:  $\sim$ 0.6 m

# Comparison of Measurements to ORNL Dual-Band IR Camera (2)

- Phantom measurement compared to dual-band
  1. During shot,  $\sim 400$  °C hotter
  2. Spatial variation much smaller ( $\Delta T \sim 150$  °C vs.  $\Delta T \sim 300$  °C)
  3. Steeper drop as shot ends ( $\Delta T \sim 150$  °C in 10 ms v.  $>100$  ms)
  4. Strike point visible in both
  5. Dual-band temperatures below measurable range for Phantom system at this exposure time
- Plasma light likely responsible
  1. Additional counts raise measured temperature
  2. If plasma light dominates, spatial variation in temperature would only be a small correction:  $\text{Temp} \sim \log(\text{counts})$
  3. Disappearance at end of shot would lead to steep drop
  4. Strike point should be bright in plasma light as well

# Summary & Conclusions

- High-speed Phantom cameras with NIR filters are capable of measuring temperature as demonstrated during calibration.
- *In situ*, background light (likely due to plasma line emission) produces a background equivalent temperature between 500 °C and 700 °C.
- Temperature of RF heated hot spots in excess of 700 °C have been measured with this system.

# Future Work

- Better determination and/or elimination of background
  - Use CI filter on Phantom 7.3 camera to determine level of line emission background
  - Use narrow band-pass filter in region where there are few emission lines
    - Reduction of counts by a factor of 10-100 *should* be okay, but will restrict measureable temperature range
    - Band TBD by V.A. Soukhanovskii's NIR spectrometry results
- Improved thermal model necessary?
  - Explain the temperature rise before RF needed for best fit
  - Include effects of impurity buildups on tiles (esp. lithium)
- More extensive comparison with slow & fast IR cameras observed heat flux
- Study transient heating due to ELMs/disruptions