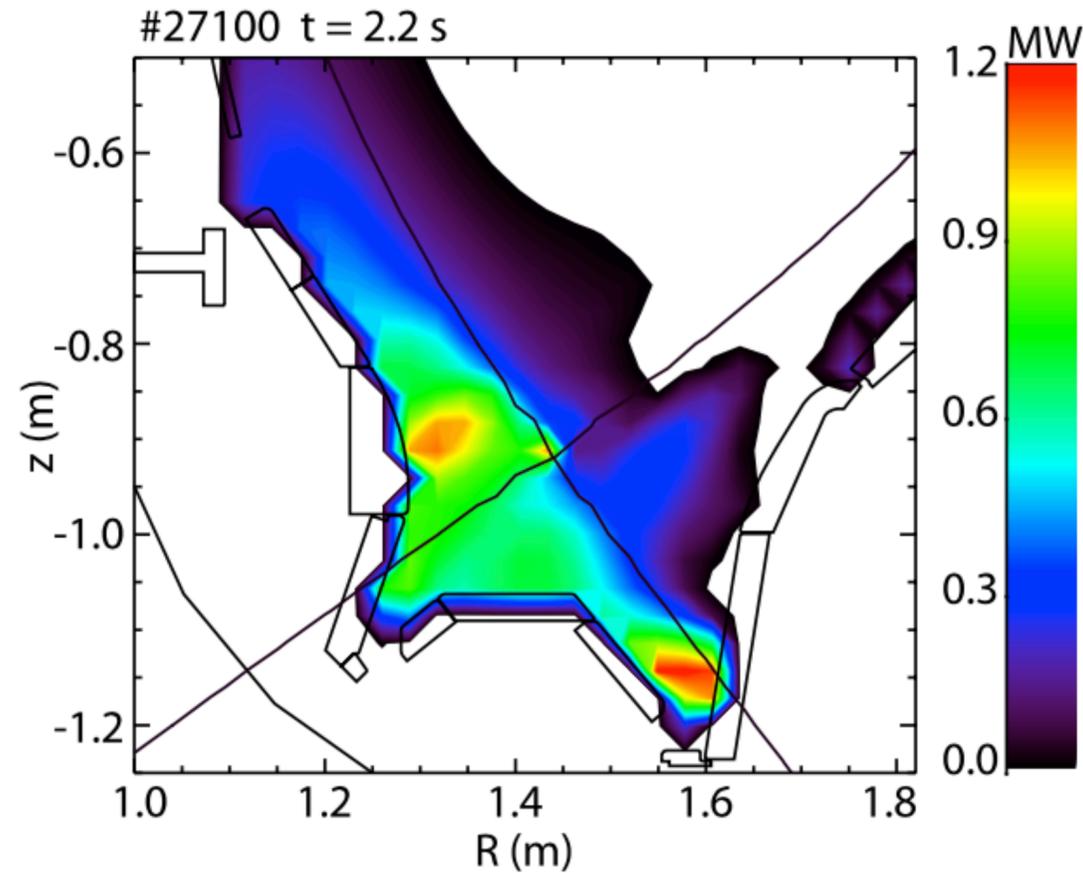
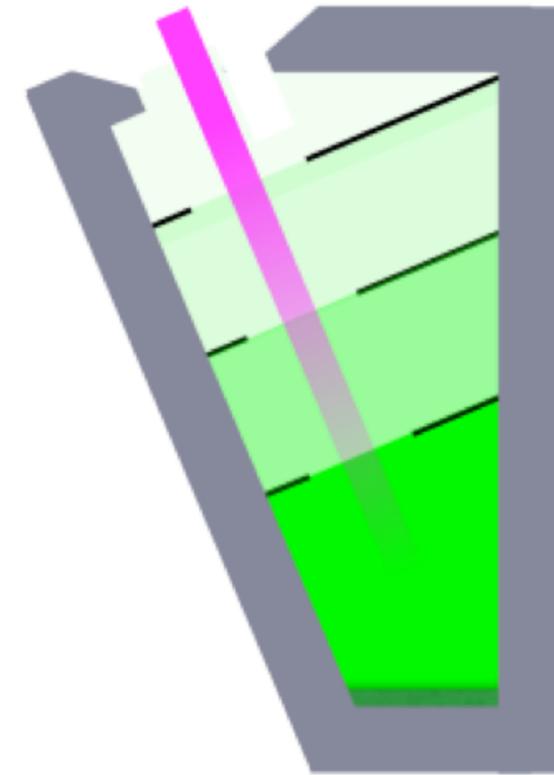


A New Scaling for Divertor Detachment



Detachment onset in ASDEX-U
Potzel et al., Nuc. Fusion 2014

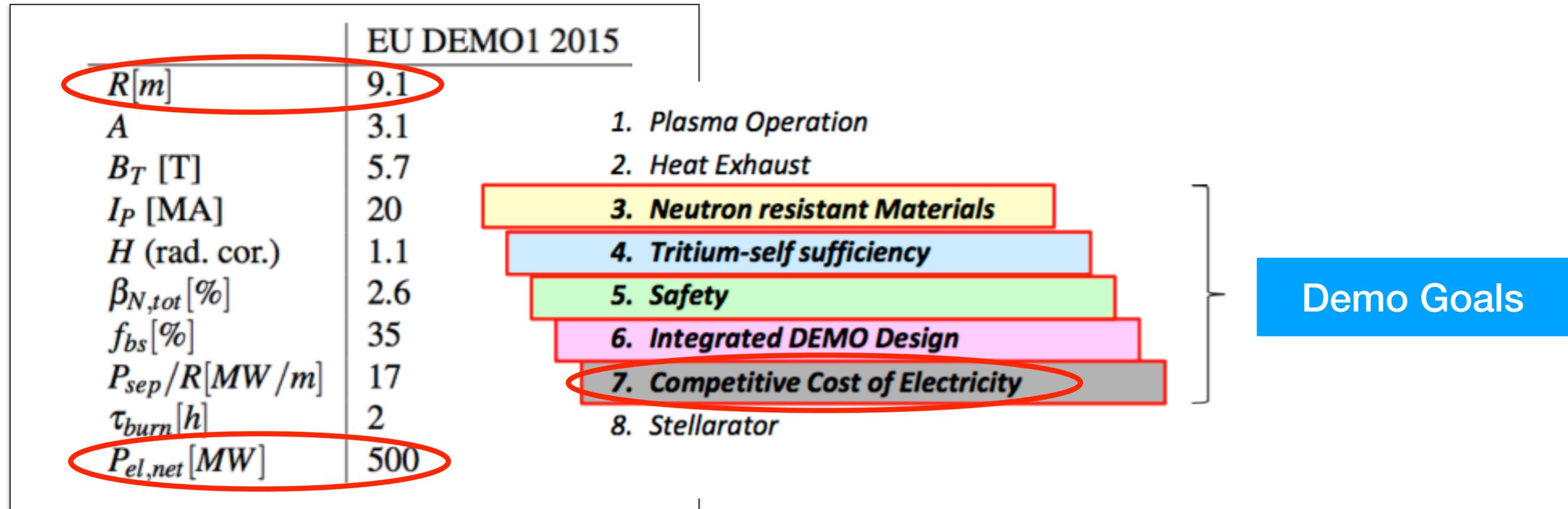


Lithium Vapor Box Divertor
R. Goldston et al., NME, 2017

R. Goldston,
M. Reinke,
J. Schwartz
PPCF 2017

M. Reinke
NF 2017

EU Demo1 is Large & Low Power



R. Wenninger et al., EPS 2015

How can this even *point to* a reasonable COE?

The Problem is Power Handling

Reasonable cost
steady-state
fusion power plant.



Add impurity seeding.
Decrease fusion power.

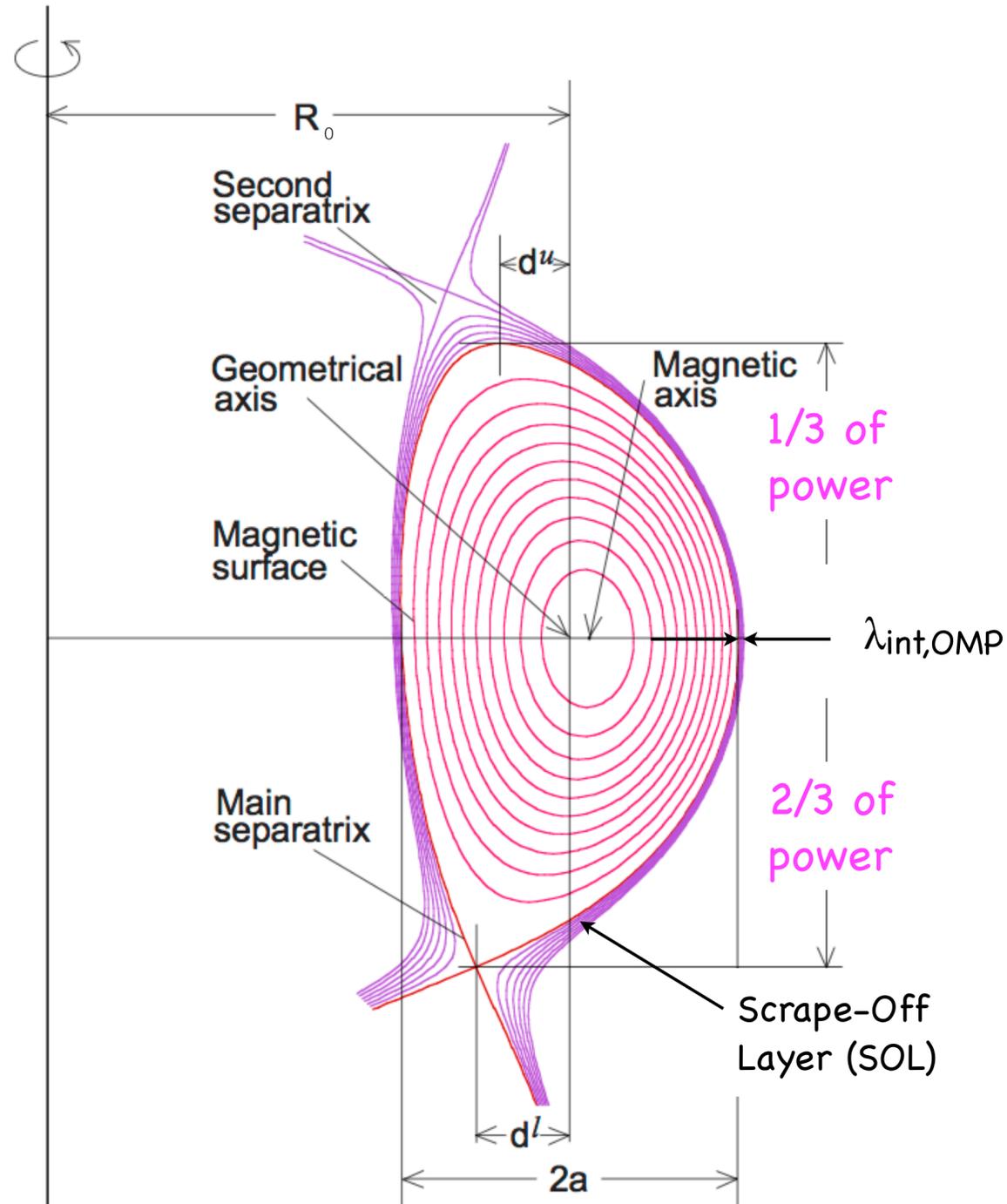


Increase size & I_p .
Accept pulsed operation.



We need to understand this problem!

Parallel Heat Flux is too High



$$\hat{q}_{\parallel} \sim \frac{2P_{SOL}/3}{2\pi(R_0 + a)\lambda_{int,OMP}} \frac{B}{B_{p,OMP}}$$

... because $\lambda_{int,OMP}$ is too low.

IR Data are Well Fit with “Eich Function”

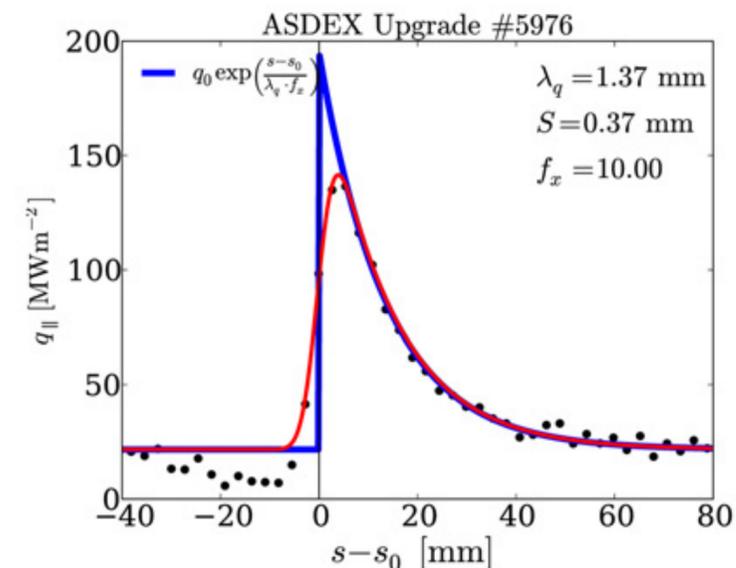
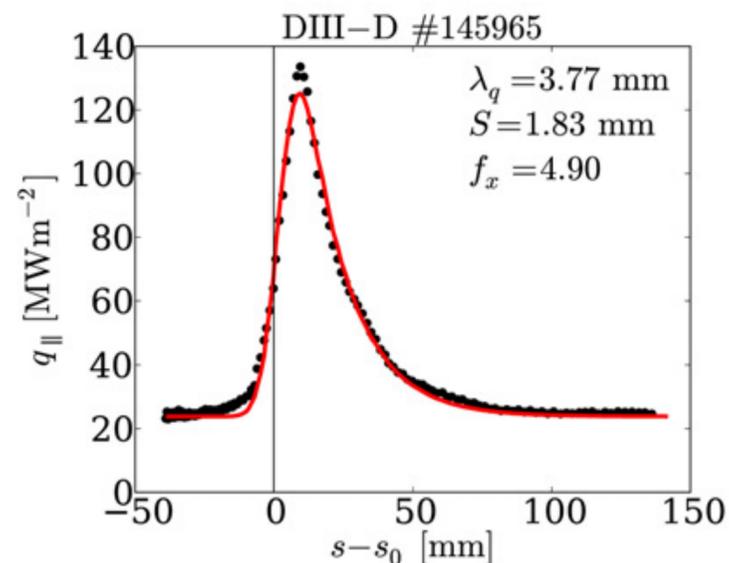
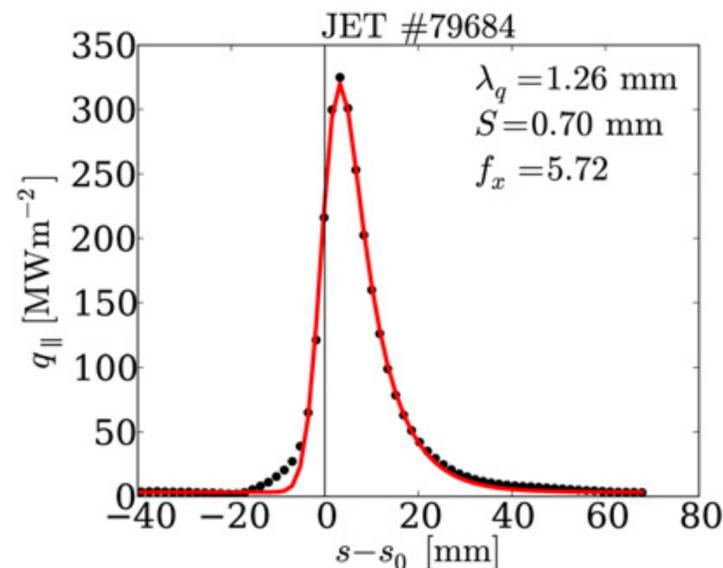
Convolve an exponential representing the near SOL, $\exp(-x/\lambda_q)$, with a Gaussian representing diffusive spreading as the plasma travels down the divertor leg, $\exp(-x^2/S^2)$.

$$q_{\parallel}(x) = q_{\parallel 0} \int_0^{\infty} \left[\exp\left(\frac{-x'}{\lambda_q}\right) \right] \left\{ \frac{1}{\sqrt{\pi}S} \exp\left[\frac{-(x-x')^2}{S^2}\right] \right\} dx'$$

$$= \frac{q_{\parallel 0}}{2} \exp\left[\left(\frac{S}{2\lambda_q}\right)^2 - \frac{x}{\lambda_q}\right] \operatorname{erfc}\left(\frac{S}{2\lambda_q} - \frac{x}{S}\right)$$

$$\Rightarrow \lambda_{int} \approx \lambda_q + 1.64S$$

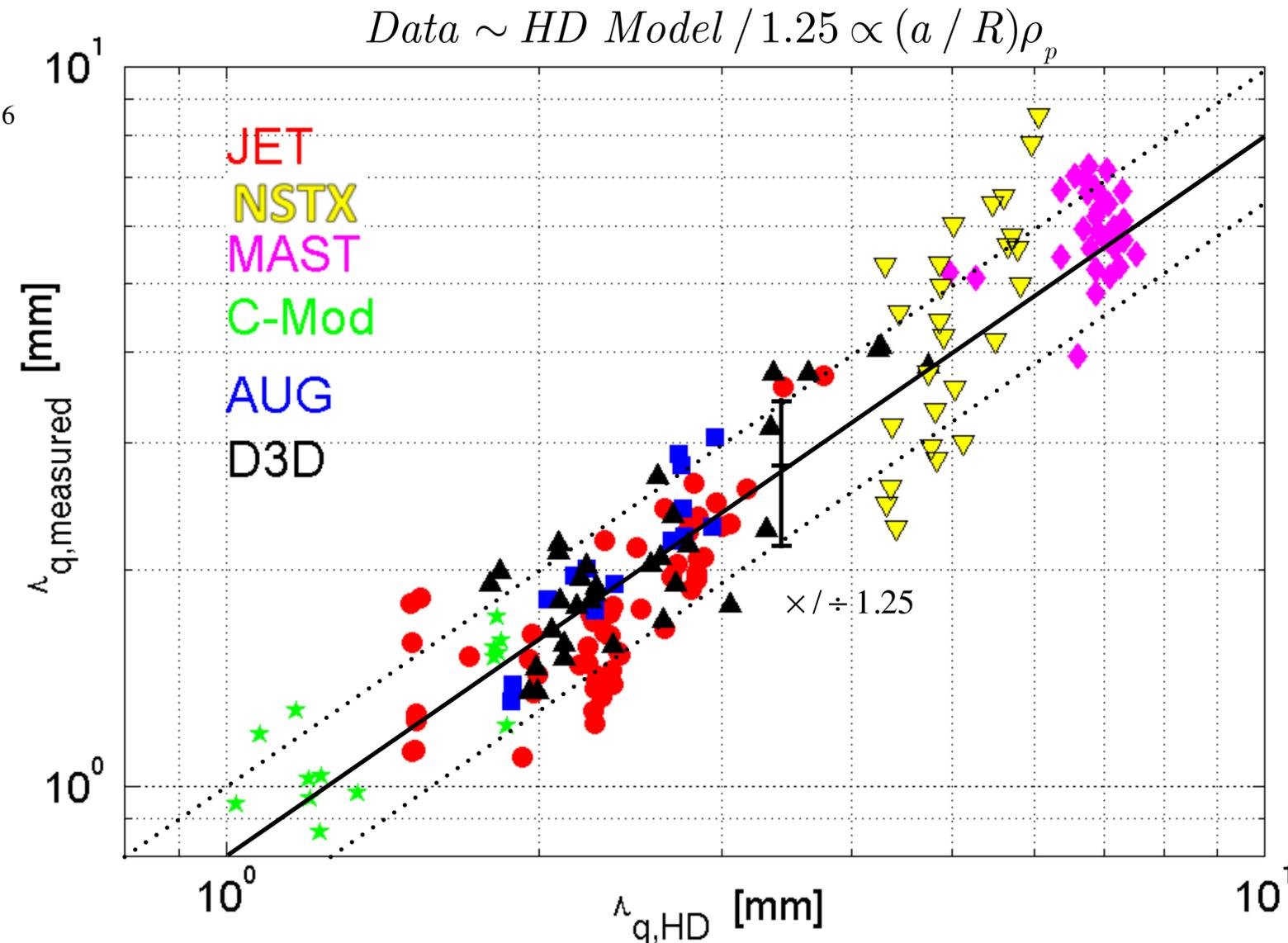
M. Makowski et al.
PoP 2012



T. Eich et al.,
NF 2013

Heuristic Drift (HD) Model Fits λ_q Data Well

$$\lambda = 5671 \cdot P_{\text{SOL}}^{1/8} \frac{(1 + \kappa^2)^{5/8} a^{17/8} B^{1/4}}{I_p^{9/8} R} \left(\frac{2\bar{A}}{(1 + \bar{Z})} \right)^{7/16} \times \left(\frac{Z_{\text{eff}} + 4}{5} \right)^{1/8} \text{ all units SI}$$



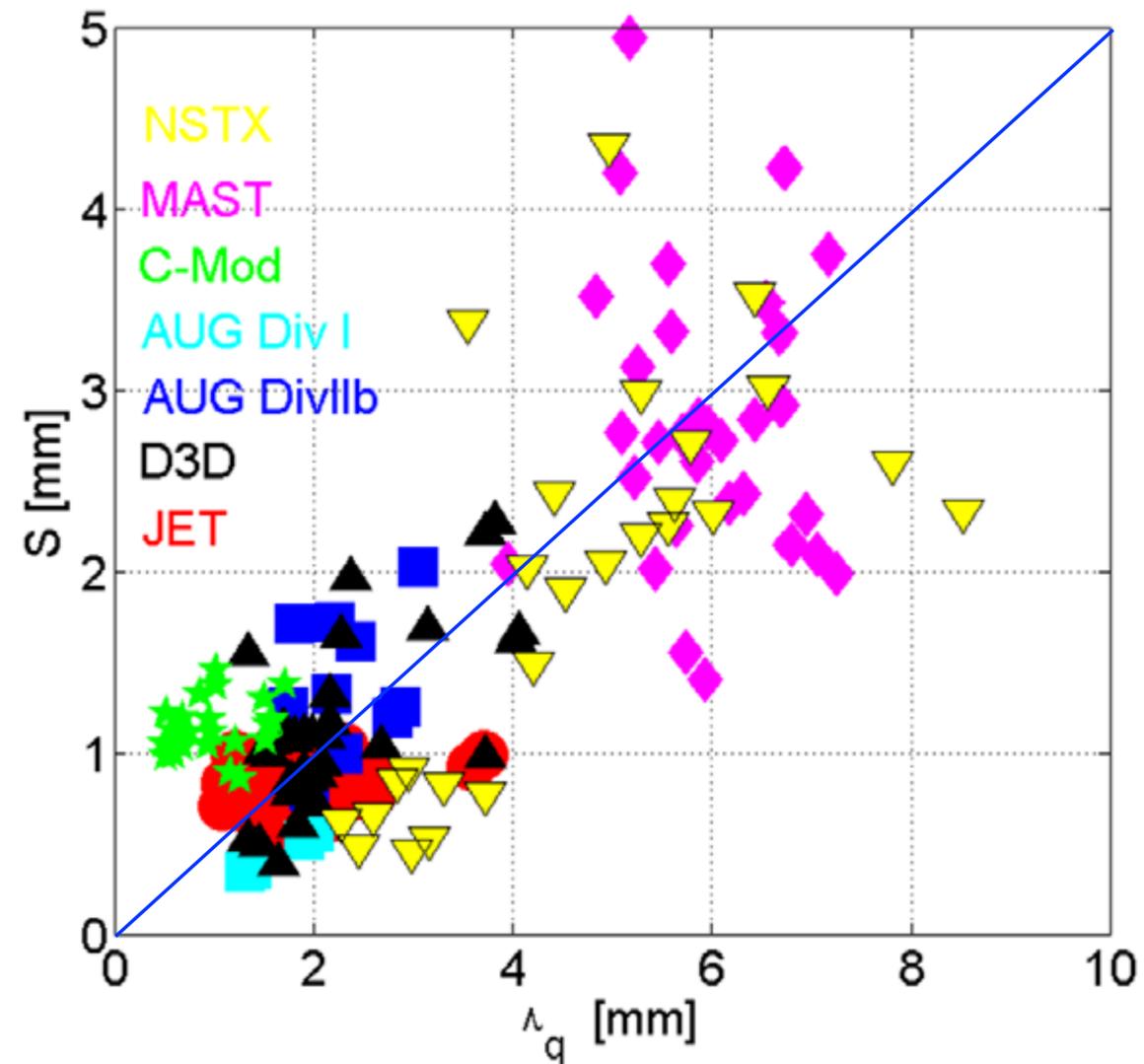
R. Goldston
JNM 2015

λ_q scales with intensive variables $T, B, a/R$, not with system size.

Ignoring dependence on $T^{1/2}$, $\lambda_q \propto (a/R)/B_p$

Projects to ITER, Demo $\lambda_q \sim 1 \text{ mm!}$

S appears to scale with λ_q



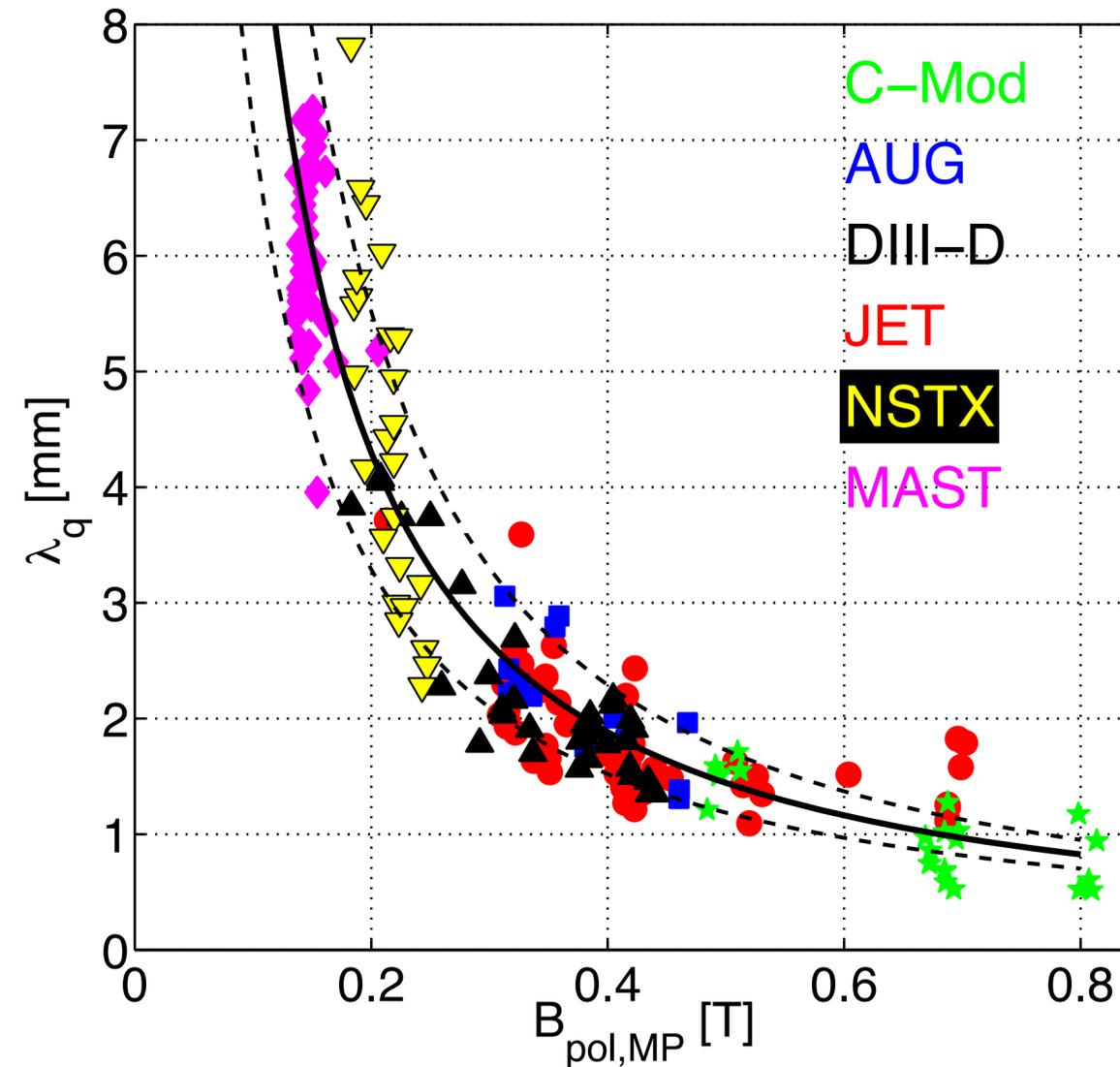
T. Eich et al.
NF 2013

$$S \approx 0.5 \lambda_q \Rightarrow \lambda_{int,OMP} \approx 1.8 \lambda_q$$

S provides no relief, unless trends change dramatically.

The Problem can be Expressed Simply

$$\hat{q}_{\parallel} \approx \frac{2P_{SOL}/3}{2\pi(R_0 + a)\lambda_{int,OMP}} \frac{B}{B_{p,OMP}}$$



T. Eich et al.
NF 2013

If $\lambda_{int,OMP}$ scales $\sim \propto 1/B_p$ the q_{\parallel} problem scales $\sim \propto PB_t/R$.

But we also need to know how the solution scales!

Lengyel Model for Cooling due to Impurities

- Parallel heat flux is reduced by impurity cooling:

$$q_{\parallel} = \kappa_0 T_e^{5/2} \frac{dT_e}{dz} \quad \frac{dq_{\parallel}}{dz} = n_e n_z L_z = n_e^2 c_z L_z; \quad c_z \equiv \frac{n_z}{n_e}$$

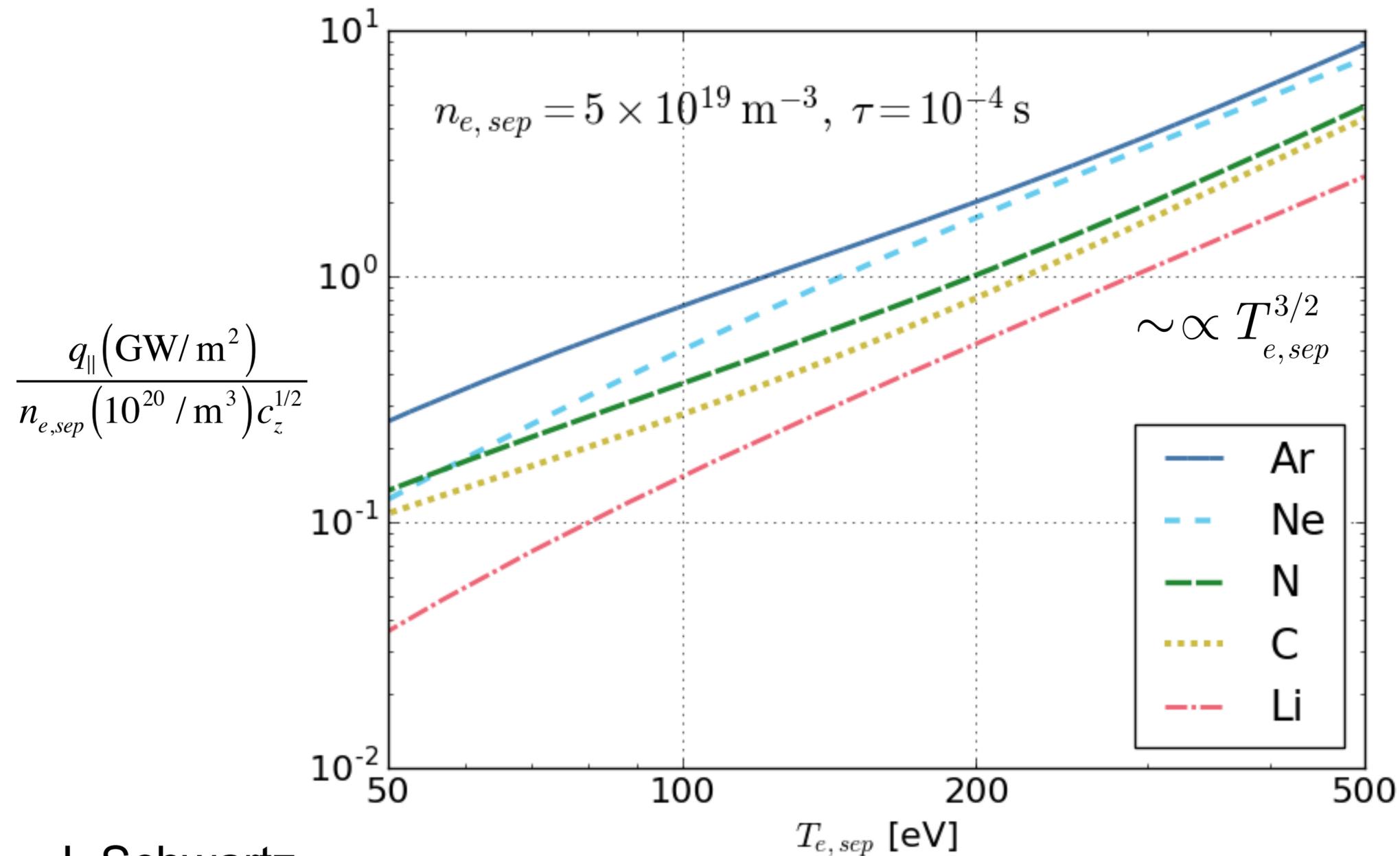
- Multiply these two equations together: $\frac{1}{2} \frac{dq_{\parallel}^2}{dz} = n_e^2 c_z L_z \kappa_0 T_e^{5/2} \frac{dT_e}{dz}$

- Integrate dz and assume $p_e = n_e T_e = \text{const.}$ along B .

$$\Delta q_{\parallel}^2 = \int_{T_{det}}^{T_{sep}} 2n_e^2 c_z L_z \kappa_0 T_e^{5/2} dT_e = 2 \left(n_{e,sep} T_{e,sep} \right)^2 \int_{T_{det}}^{T_{sep}} c_z L_z \kappa_0 T_e^{1/2} dT_e$$

- Assume $c_z = \text{const.}$ $\frac{\Delta q_{\parallel}}{n_{e,sep} c_z^{1/2}} = \left(2T_{e,sep} \int_{T_{det}}^{T_{sep}} c_z L_z \kappa_0 T_e^{1/2} dT_e \right)^{1/2}$

Use ADAS to Evaluate Lengyel Integral



- Includes finite lifetime non-coronal radiation
- Assume nearly all of P_{sep} must be dissipated to achieve detachment at a few eV.
- $q_{||}$ that can be detached scales as $n_{e,sep} c_z^{1/2} T_{sep}^{3/2}$
- Note that per electron, lithium is comparable to nitrogen.

NEW: Bring in Greenwald Density & Spitzer T_{sep}

- So far we have something very simple: $q_{\parallel, det} \sim \propto n_{e, sep} T_{e, sep}^{3/2} c_z^{1/2}$

- Assume Greenwald density scaling & Spitzer electron thermal conduction:

$$n_{e, sep} \propto f_{GW, sep} \frac{\langle B_p \rangle}{a} (1 + \kappa^2)^{1/2} \quad T_{e, sep} \propto (q_{\parallel} \ell_{\parallel}^* q_{cyl} R_0)^{2/7} \quad \ell_{\parallel}^* \equiv L_{\parallel} / (\pi q_{cyl} R_0)$$

- Multiply first equation by R_0 and substitute for $n_{e, sep}$ and $T_{e, sep}$.

$$R_0 q_{\parallel} \propto f_{GW, sep} \frac{R_0}{a} \langle B_p \rangle (1 + \kappa^2)^{1/2} (q_{\parallel} \ell_{\parallel}^* q_{cyl} R_0)^{3/7} c_z^{1/2} \Rightarrow c_z \propto \frac{(R_0 q_{\parallel})^{8/7}}{f_{GW, sep}^2 (\ell_{\parallel}^* q_{cyl})^{6/7} \left(\frac{R_0}{a}\right)^2 \langle B_p \rangle^2 (1 + \kappa^2)}$$

- OOPS, we had before, very roughly, $q_{\parallel} \propto PB/R \Rightarrow$ *Strong P scaling, no size scaling!*

Now Bring in HD λ_q to get $R_0 q_{||}$

- Using HD model for λ_q , with its implicit Spitzer model for $T_{e,sep}$:

$$q_{||} R_0 \propto \frac{P}{\lambda_{q,HD}} \frac{B_t}{B_p} \propto P_{sep}^{7/8} B_t^{3/4} \langle B_p \rangle^{1/8} \frac{R_0}{a} (1 + \kappa^2)^{-1/16} \left(\frac{\bar{A}}{1 + \bar{Z}} \right)^{-7/16} (\ell_{||}^*)^{-1/8}$$

- Substitute this into the result from the last slide:

$$c_z \propto \frac{P_{sep} B_{t,0}^{6/7} \left(\frac{\bar{A}}{1 + \bar{Z}} \right)^{-1/2}}{f_{GW,sep}^2 \left(\frac{R_0 q_{cyl}}{a} \right)^{6/7} \langle B_p \rangle^{13/7} (1 + \kappa^2)^{15/14} \ell_{||}^*}$$

- Lots of terms cancel:

$$c_z \propto \frac{P_{sep}}{\langle B_p \rangle \ell_{||}^* (1 + \kappa^2)^{3/2} f_{GW,sep}^2} \left(\frac{1 + \bar{Z}}{\bar{A}} \right)^{1/2}$$

- If you take into account the solution as well as the problem, the difficulty scales as P/B_p not as PB_t/R .
- No wonder making the machine larger doesn't help.
- Surprisingly, you want higher field, not larger size.

We Should not Have Been Surprised

- Ignoring temperature variation

$$P_{rad} \propto c_z n_e^2 V \Rightarrow c_z \propto \frac{P_{sep}}{n_{sep}^2 \lambda_{HD} R a \ell_{\parallel}^* (1 + \kappa^2)^{1/2}}$$

- The HD model and the Greenwald density are

$$\lambda_{HD} \propto \frac{a}{R B_p} \quad n_{sep}^2 \propto f_{GW}^2 \frac{B_p^2}{a^2} (1 + \kappa^2)$$

- Giving the familiar result:

$$c_z \propto \frac{P_{sep}}{B_p \ell_{\parallel}^* (1 + \kappa^2)^{3/2} f_{GW}^2}$$

Lorentz center

Taming the Flame
Divertor Detachment Control in Tokamaks

Workshop: 19 - 23 September 2016, Leiden, the Netherlands

Scientific Organizers

- Raffaele Albanese, UNFI Naples
- Marco de Baar, DIFFER Eindhoven
- Tony Donné, EUROfusion
- Piero Martin, U Padova
- Maarten Steinbuch, TU Eindhoven

Invited Speakers

- Marco Ariola, Parthenope U Naples
- Rob Goldston, PPPL Princeton
- James Harrison, CCFE Culham
- Egemen Kolemen, Princeton U
- Emmanuel Witrant, UJF Grenoble

The Lorentz Center is an international center for scientific workshops. Its aim is to organize workshops for researchers in an atmosphere that fosters collaborative work, discussions and interactions. For registration see: www.lorentzcenter.nl

The workshop focuses on methods for divertor detachment control to prevent damage to the components during the power exhaust of a fusion plasma. Image: The Iron Rolling Mill, Adolph Menzel (1875). Poster design: Supernova Studios, NL.

Universiteit Leiden, FOM, STW, DIFFER, EUROfusion, NWO, Lorentz center

www.lorentzcenter.nl

Credit Where Credit is Due Dept.

Matt Reinke & I arrived at the “Taming the Flame” Lorentz Workshop in Sept. 2016, already looking into these ideas. We worked together and improved each other’s thinking. See his paper in NF, 2017.

How Serious is This Problem?

| | C-Mod | ASDEX-U | JET | ITER | FNSF (A=4) | EU Demo1 |
|---|----------|----------|----------|----------|------------|----------|
| P_{sep} | 3.83 | 10.7 | 14 | 100 | 96 | 154.7 |
| B_t | 5.47 | 2.5 | 2.5 | 5.3 | 7.0 | 5.7 |
| R_0 | 0.7 | 1.6 | 2.9 | 6.2 | 4.5 | 9.1 |
| P_{sep}/R | 5.5 | 6.7 | 4.8 | 16.1 | 21.3 | 17.0 |
| $P_{sep}B_t/R$ | 29.9 | 16.7 | 12.1 | 85.5 | 149.3 | 96.9 |
| I_p | 0.82 | 1.2 | 2.5 | 15 | 7.5 | 20 |
| a | 0.22 | 0.52 | 0.90 | 2.00 | 1.13 | 2.94 |
| K_{95} | 1.51 | 1.63 | 1.73 | 1.80 | 2.10 | 1.70 |
| $\langle B_p \rangle$ | 0.58 | 0.34 | 0.39 | 1.03 | 0.81 | 0.98 |
| q_{cyl} | 3.78 | 3.16 | 2.79 | 2.42 | 3.55 | 2.62 |
| n_{GW} | 5.39E+20 | 1.44E+20 | 9.82E+19 | 1.19E+20 | 1.89E+20 | 7.39E+19 |
| Projected c_N for detachment from AUG | 1.0% | 4.0% | 4.1% | 10.1% | 8.6% | 18.8% |

Pretty serious.

Parallel Connection Length May be a Useful Knob

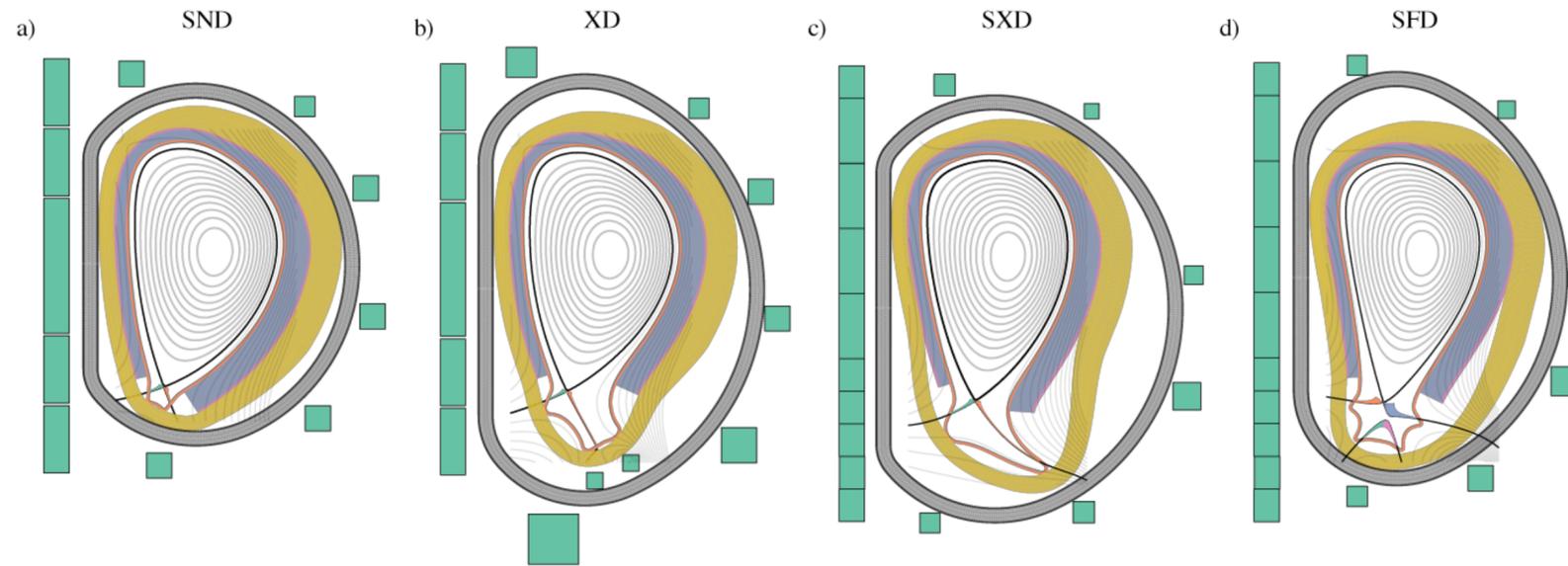


Fig. 6: (a) Reference configuration and alternative configurations including (b) an X divertor, (c) a Super-X divertor and (d) a snowflake divertor.

H. Reimerdes
???

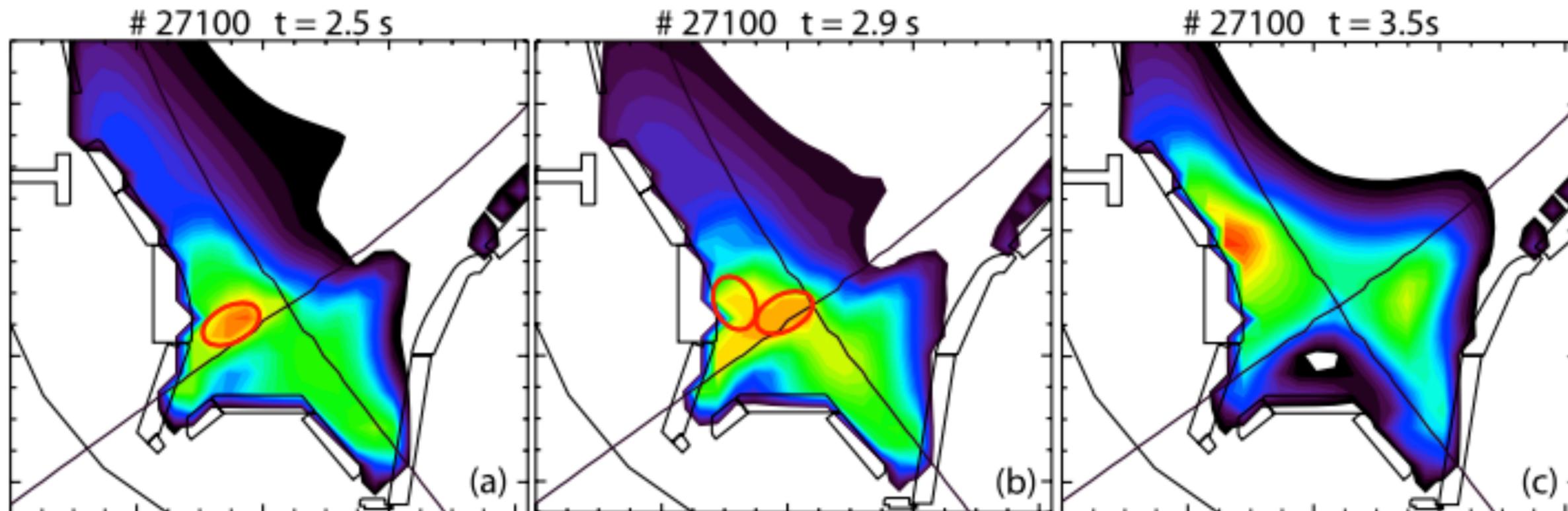
$$c_z \propto \frac{P_{sep}}{B_p \ell_{||}^* (1 + \kappa^2)^{3/2} f_{GW}^2}$$

| | | SND | XD | SXD | SFD | Limit |
|-----------------|--|------|------|------|------|-------|
| Costs | Max $\Sigma I_{PF} $ (Ma turns) | 160 | 194 | 164 | 174 | |
| | Total $I_{PF, internal}$ (MA turns) | - | 10 | - | - | |
| | Max. force on single coil $F_{z, PF}$ (MN) | 145 | 301 | 451 | 439 | <450 |
| | Max. CS separation force $F_{z, CS}$ (MN) | 130 | 244 | 284 | 329 | <350 |
| | Flux swing (Vs) | 330 | 340 | 297 | 215 | |
| | Norm. TF coil volume V_{TF}/V_{plasma} | 2.9 | 3.6 | 4.2 | 3.8 | |
| Benefits | $L_{ , outer}$ ($r_u=3mm$) (m) | 114 | 146 | 158 | 245 | |
| | $f_{x,t}/f_{x,min}$ | 1 | 1.43 | 1 | 1 | |
| | R_t/R_x | 1.04 | 1.14 | 1.34 | 1.19 | |

c_z down x2

Detachment Tends to Run up to the X-Point

S. Potzel et al.
NF 2014

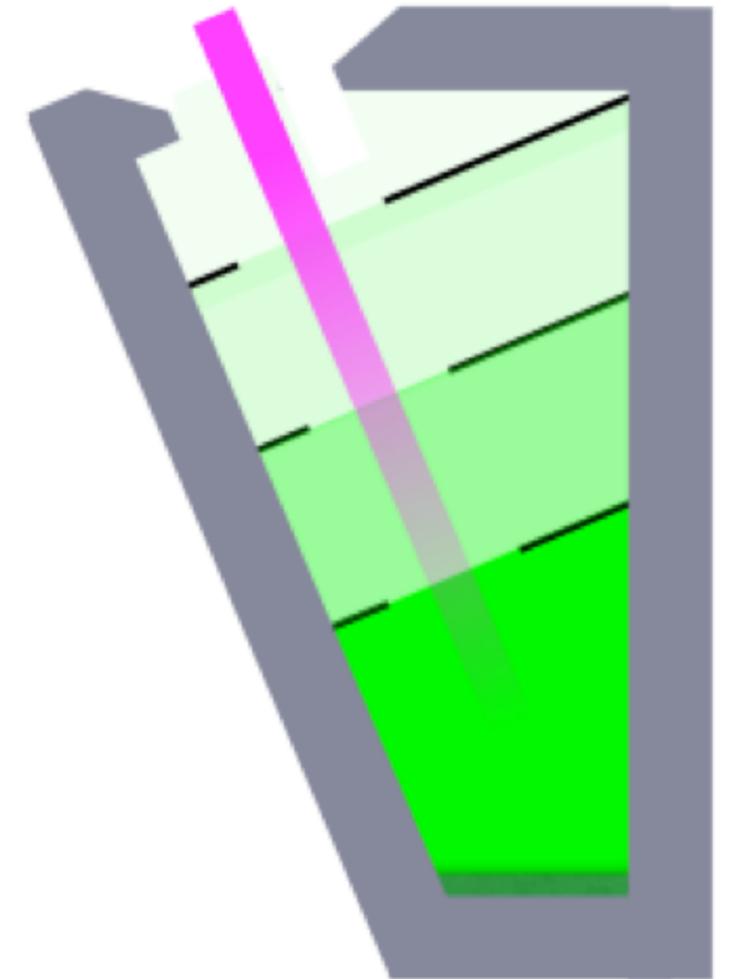


This exposes the core to impurity influx.

Lithium Vapor Box Should Provide Stable Detachment

- Multiple boxes are used to provide differential pumping.
- Lithium recirculates via capillary action (like a heat pipe)
- Bottom box provides enough lithium to detach.
 - Higher boxes are cooler, less dense.
- Plasma detachment should be very stable.

Picture of vapor calculation with efflux calculation from Eric.



Conclusions

- Attempting to achieve ITER-like $q_{||} \propto PB/R$ drives Demo designs to large size and low power.
- The difficulty-of-detachment parameter is more likely P/B_p
 - We should perform numerical and laboratory experiments to test this hypothesis.
 - This is further motivation for compact high-field designs.
- Enhancing the divertor leg length should reduce the impurity content required for detachment.
- Detachment stability can be assured by localizing the impurity influx, as in a Vapor Box Divertor.