

## CHI Research on NSTX-U

W-S. Lay<sup>1</sup>, R. Raman<sup>1</sup>, T.R. Jarboe<sup>1</sup>, B.A. Nelson<sup>1</sup>,  
D. Mueller<sup>2</sup>, F. Ebrahimi<sup>2</sup>, M. Ono<sup>2</sup>, S.C. Jardin<sup>2</sup>, G. Taylor<sup>2</sup>

<sup>1</sup>University of Washington, Seattle, WA USA

<sup>2</sup>Princeton Plasma Physics Laboratory, Princeton, NJ, USA

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R. Fonck, J. Reusch, M. Bongard & the PEGASUS Team

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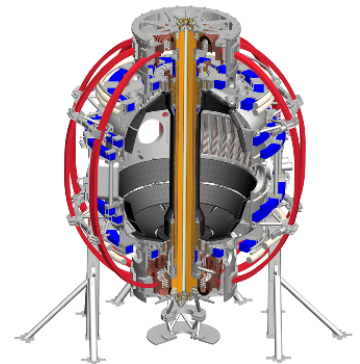
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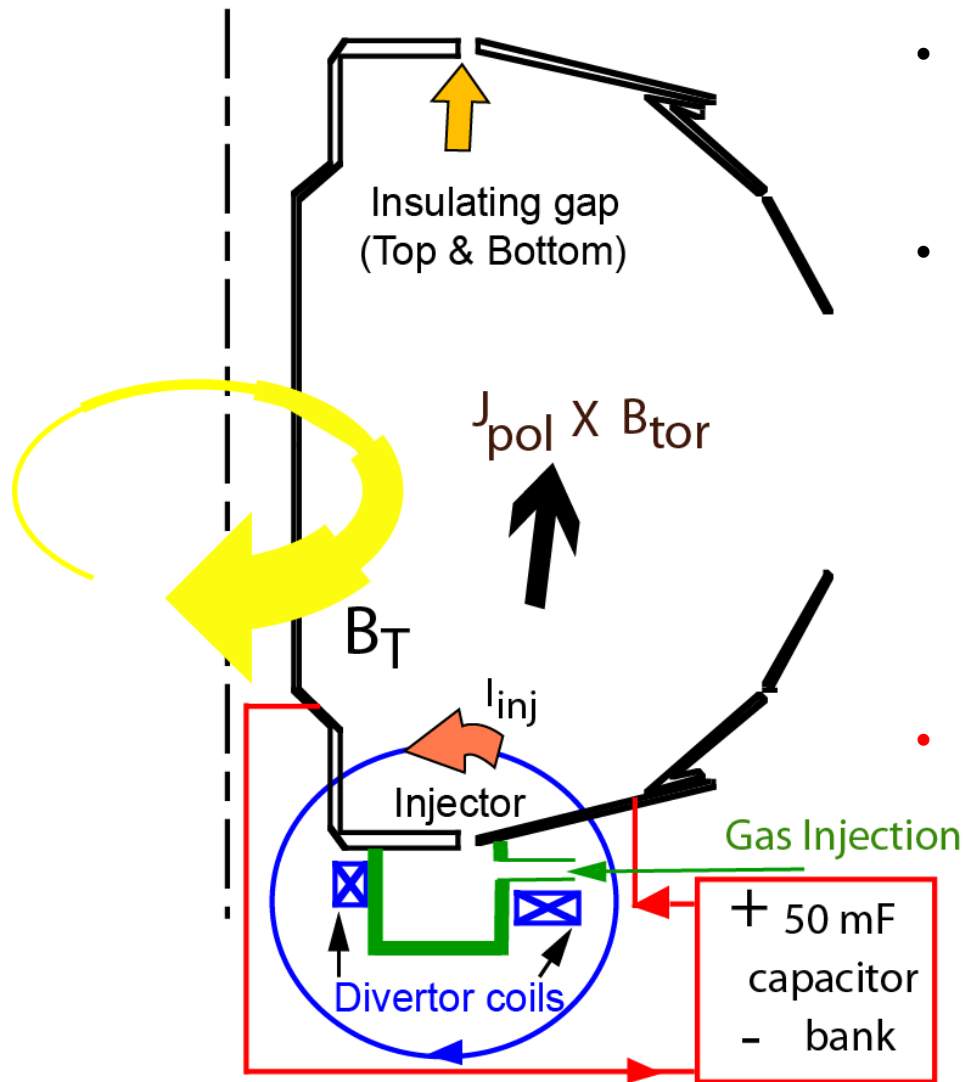
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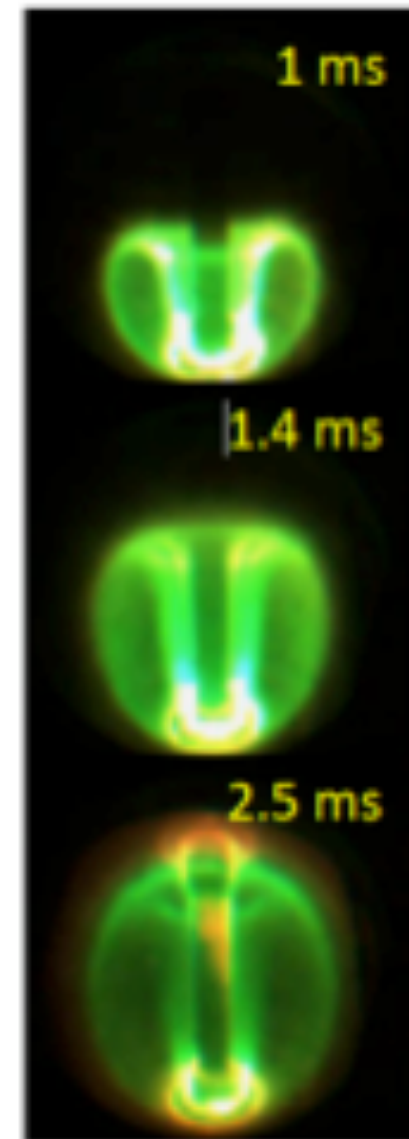
# Objectives of Transient CHI Research

1. Introduction to Transient CHI Start-up
2. Minimize non-inductive current ramp-up requirements
3. Simplify electrode configuration for ST-FNSF
4. CHI on QUEST
5. Planned configuration for CHI on PEGASUS
6. TSC Simulations
7. NIMROD Simulations
8. Conclusions

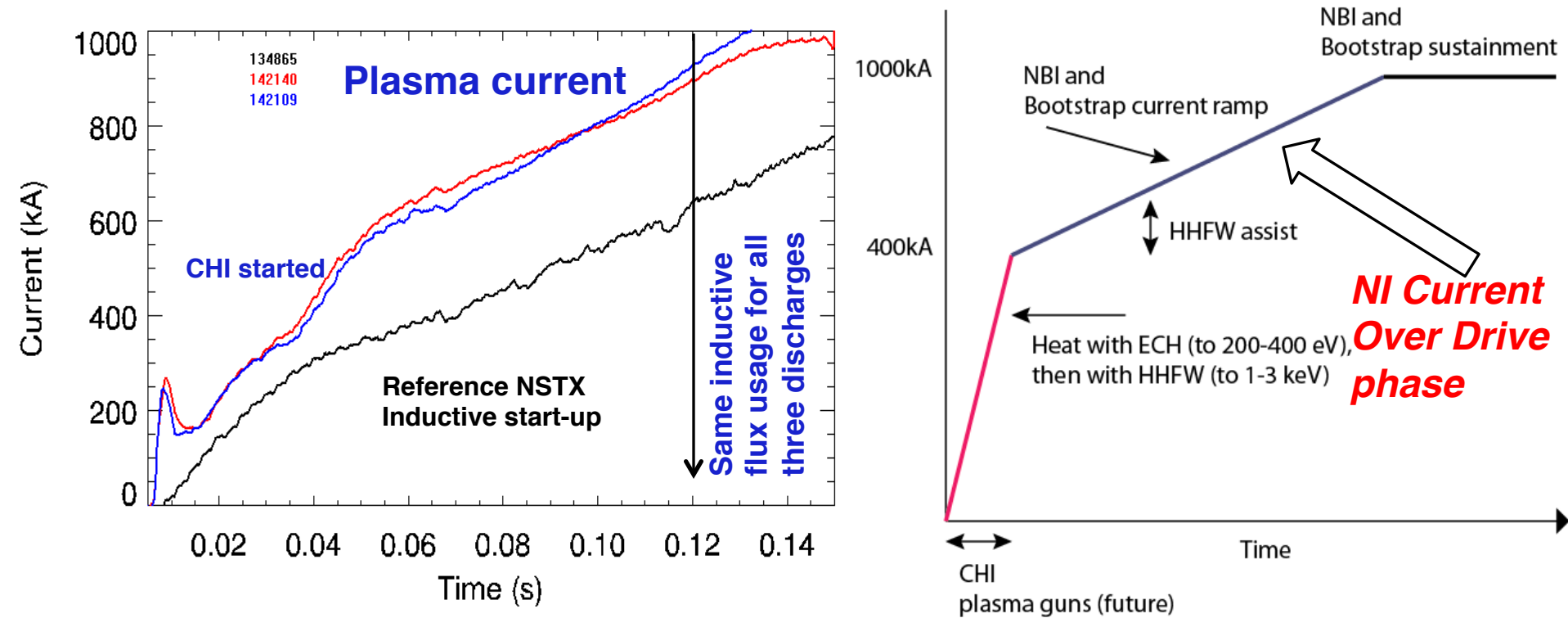
# Transient CHI on NSTX: The injected open flux closes in on itself to a relaxed state containing >70% of initial injected flux



- Transient CHI does not rely on dynamo current drive
- Thus, T-CHI is simpler, as one need not develop scenarios for current overdrive in a magnetic configuration that is constantly changing in time
- Can T-CHI produce most of the initial current needed during sustained operation in a reactor?



# Minimizing Non-Inductive Current Ramp-up Phase would Simplify Current Over Drive Needs in an ST-FNSF



- Transient Coaxial Helicity Injection (CHI) on NSTX
  - 200 kA start-up currents ramped to 1MA with inductive flux savings
  - Generating  $I_p \sim 1$  MA by CHI would eliminate the need for the difficult non-inductive current ramp-up step

## Externally Produced Toroidal Field makes CHI Efficient in an ST & Necessary for High Current Generation in an ST-FNSF

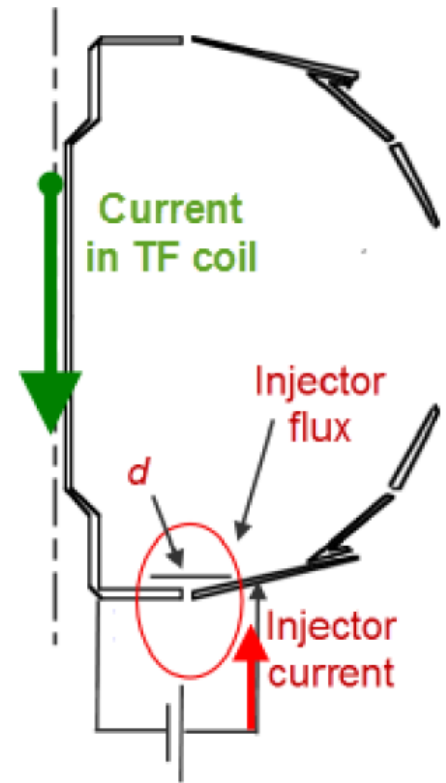
- Bubble burst current\*:  $I_{inj} = 2\psi_{inj}^2 / (\mu_o^2 d^2 I_{TF})$

$$\psi_{inj} = \text{injector flux}$$
 $d$  = flux foot print width
$$I_{TF} = \text{current in TF coil}$$

**Injector current**      **Toroidal flux**

$I_P = I_{inj} (\psi_T / \psi_{inj})$

- Current multiplication increases with toroidal field
  - Favorable scaling with machine size
  - Increases efficiency (10 Amps/Joule in NSTX)
  - Smaller injector current to minimize electrode interaction

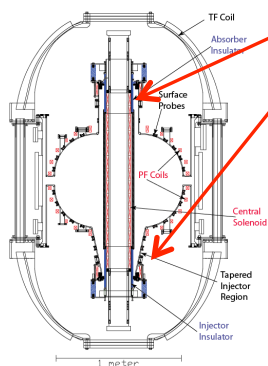


**Closed flux current magnitude is proportional to injector flux, and this must be maximized while minimizing the injector current**

\* T.R. Jarboe, *Fusion Tech.* 15, 7 (1989)

# CHI Insulator On NSTX and HIT-II are part of Vessel Vacuum Boundary

**HIT-II and NSTX use two toroidal insulators to insulate the inner vessel from the outer vessel components**

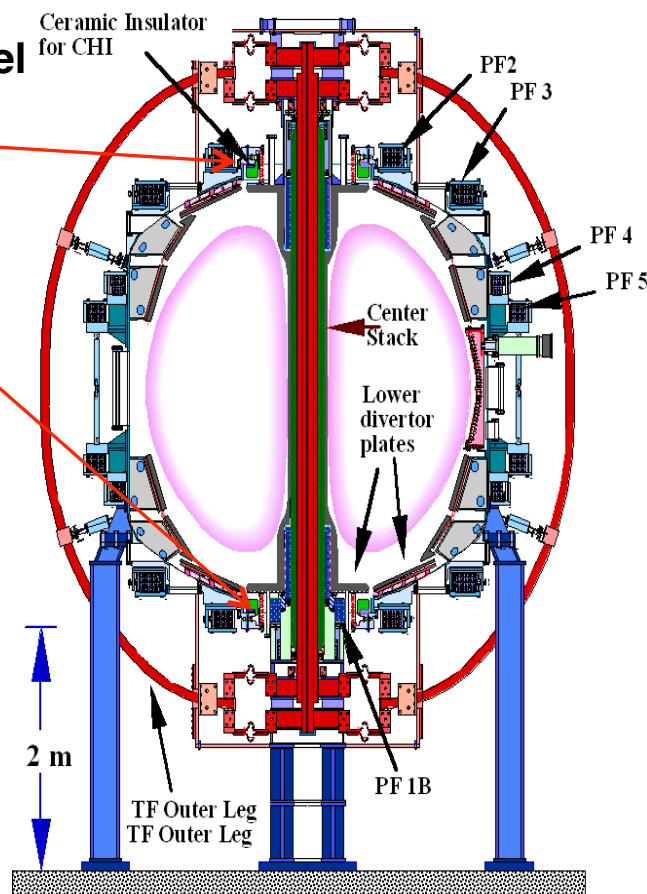


**Devices approximately to scale**

## **Concept exploration device HIT-II**

- Built for developing CHI
- Many close fitting fast acting PF coils
- 4 kV CHI capacitor bank
- 16 mWb injector flux, produced  $I_p = 100$  kA

**NSTX plasma is ~30 x plasma volume of HIT-II**

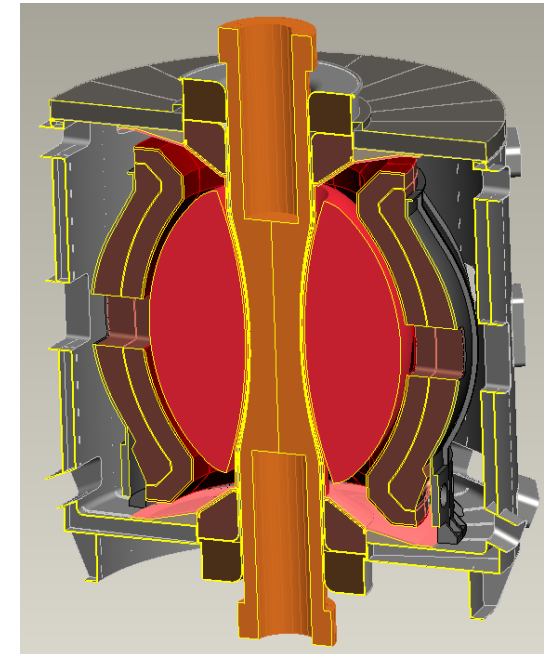
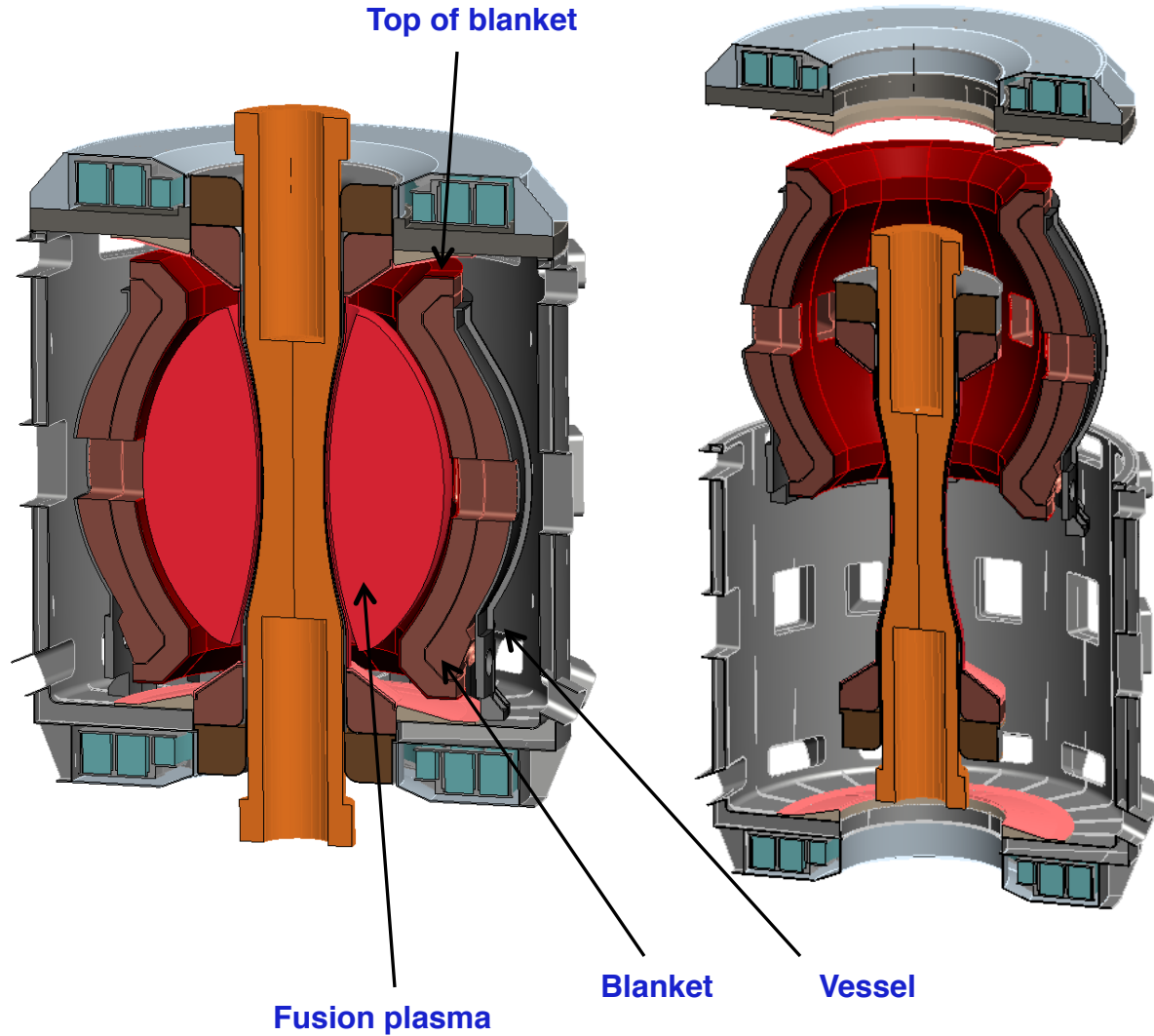


## **Proof-of-Principle NSTX device**

- Built with conventional tokamak components
- Few PF coils
- 1.7 kV CHI capacitor bank
- 50 mWb injector flux, produced  $I_p = 200$  kA

# ST FNSF Configuration

( $R_{\text{maj}} = 1.7\text{m}$ ,  $A=1.5$ ,  $B_T = 3\text{T}$ ,  $I_p = 10\text{MA}$ )



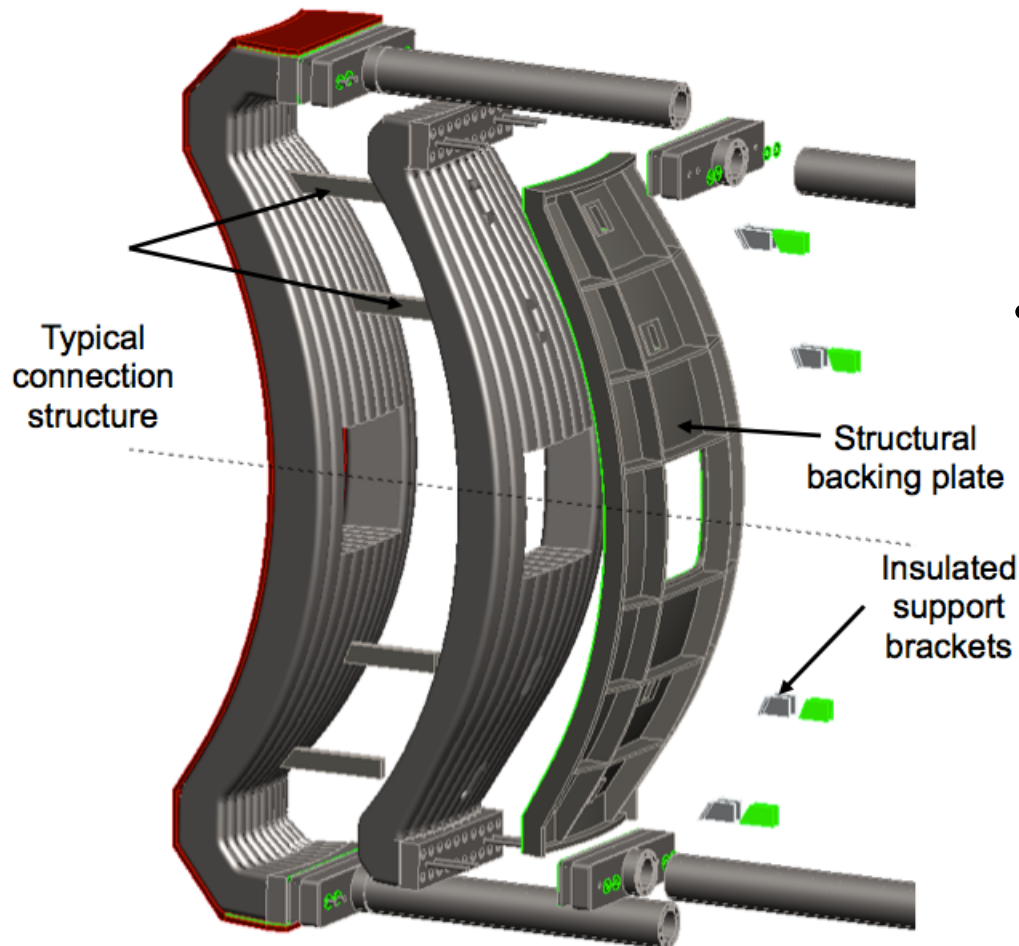
3-D Neutronics model



# CHI Design Studies for ST-FNSF have Identified Two Designs with > 2MA Start-up Current Generation Potential

## Concept – I (NSTX-like)

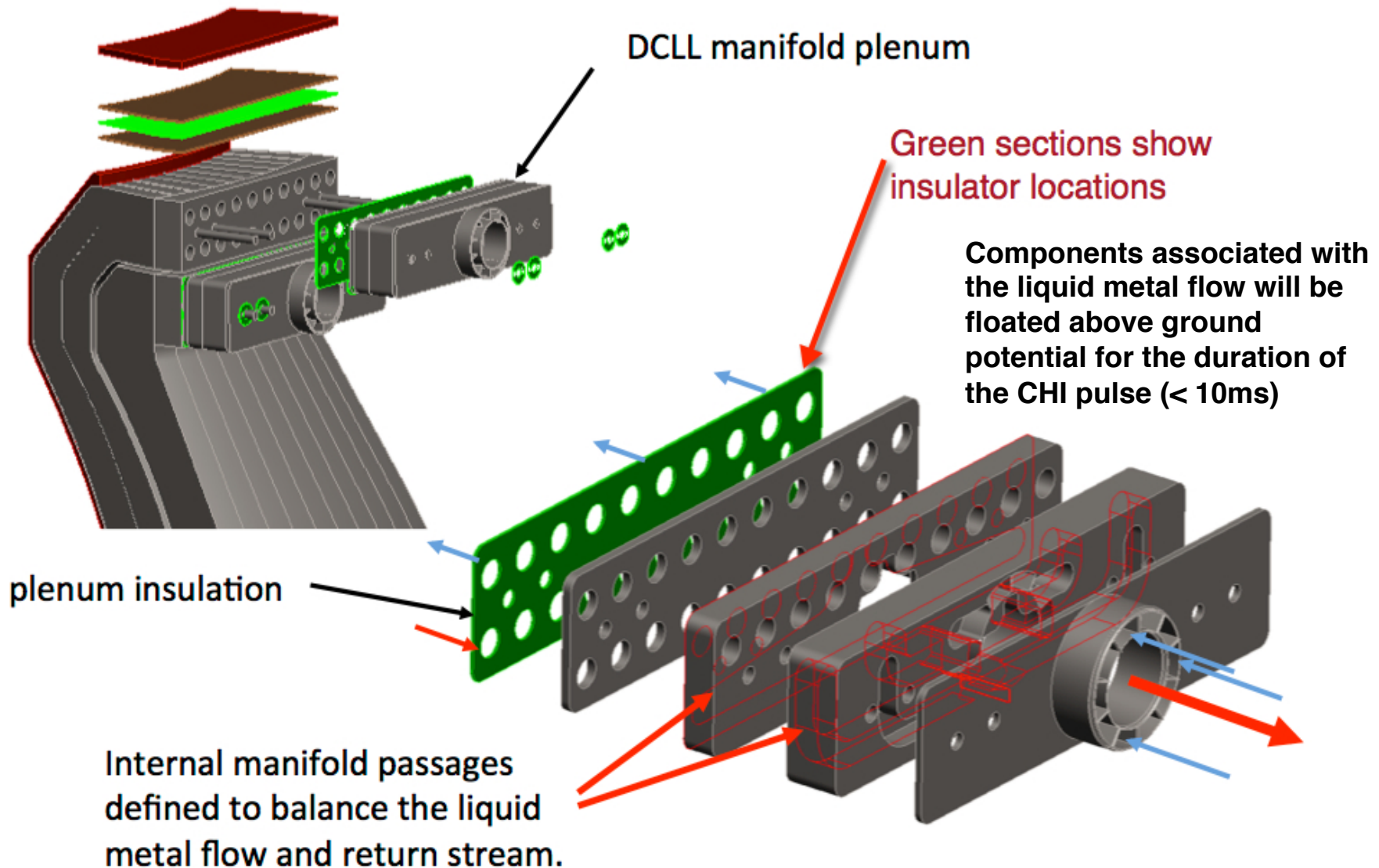
\*Blanket modules and piping insulated from rest of vessel



- On NSTX and NSTX-U entire inner vessel is electrically isolated from outer vessel
  - Injector flux connects inner divertor plate to outer divertor plate and outer vessel regions
- In ST-FNSF concept – I, entire blanket structure is electrically insulated from entire vessel
  - Injector flux connects lower portion of vessel to the lower portion of the blanket assembly
  - For CHI, the blanket is analogous to the inner vessel in NSTX/NSTX-U



# Concept – I Requires All Piping to be Electrically Insulated

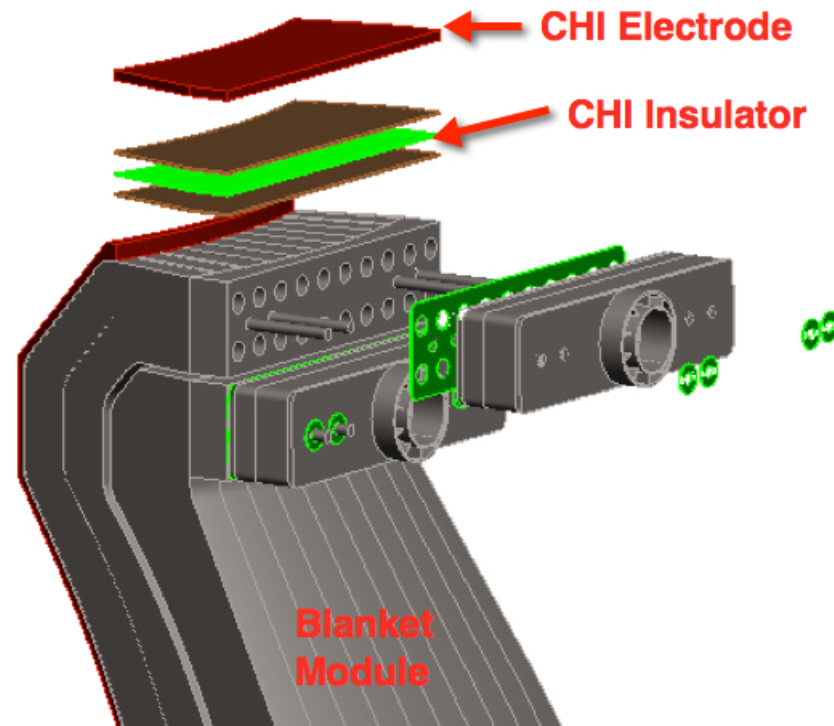


## Concept – II is simpler, but Requires Additional Experimental Tests

- On DIII-D a Ring-Electrode was installed inside the vessel
  - Injector flux connects parts of the DIII-D vessel to the ring electrode
  - Concept successfully used to sustain 1kV voltages for over 1s with MA plasma present
- In ST-FNSF concept – II, a toroidal ring electrode is placed on top of the upper blanket section, insulated from the blanket using a insulator plate
  - Injector flux connects upper portion of vessel to the electrode plate on the upper portion of the blanket assembly
  - Because the insulator is largely shielded from direct neutron streaming, insulator dose issues should not be a problem, as noted by the 3-D neutronics calculation

### Concept – II (DIII-D/QUEST-like)

Toroidal electrode on top of blanket structure, analogous to CHI ring electrode previously used on DIII-D

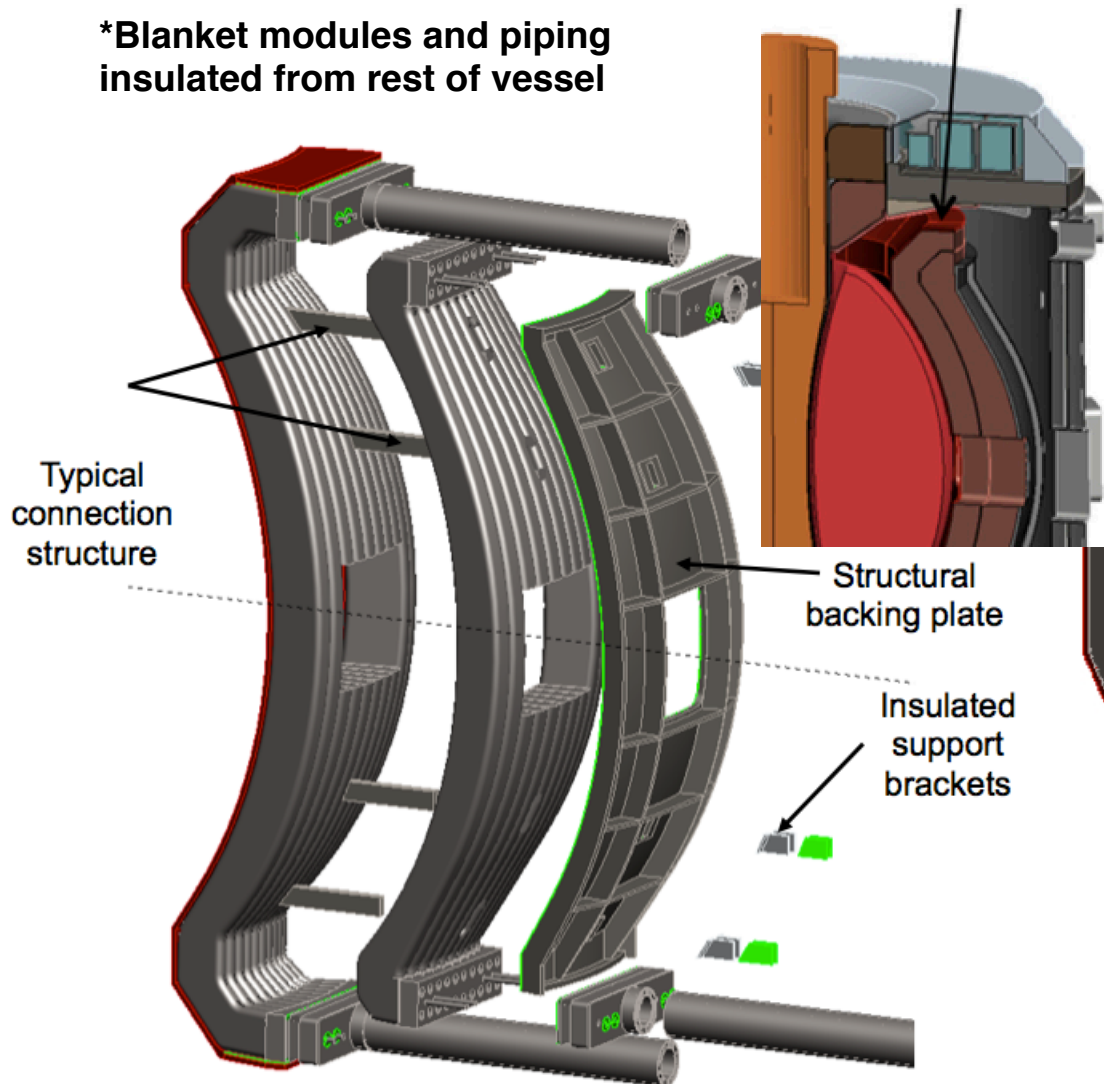


\*Insulator dose:  
 $\sim 6 \times 10^9 \text{ Gy @ 6FPY} < 10^{11} \text{ Gy limit}$

# CHI Design Studies for ST-FNSF have Identified Two Designs with $> 2$ MA Start-up Current Generation Potential

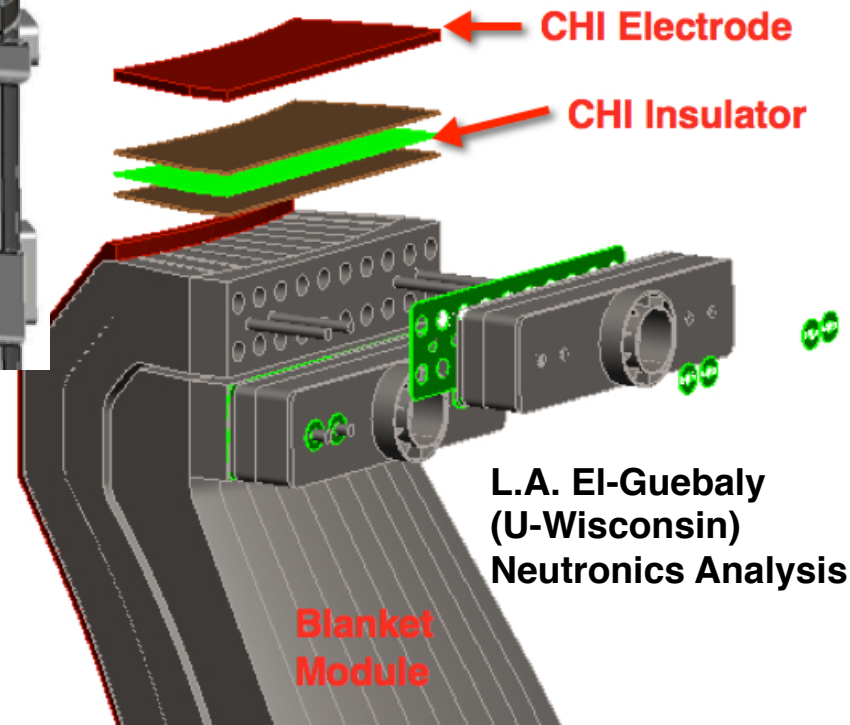
## Concept – I (NSTX-like)

\*Blanket modules and piping insulated from rest of vessel



## Concept – II (QUEST-like)

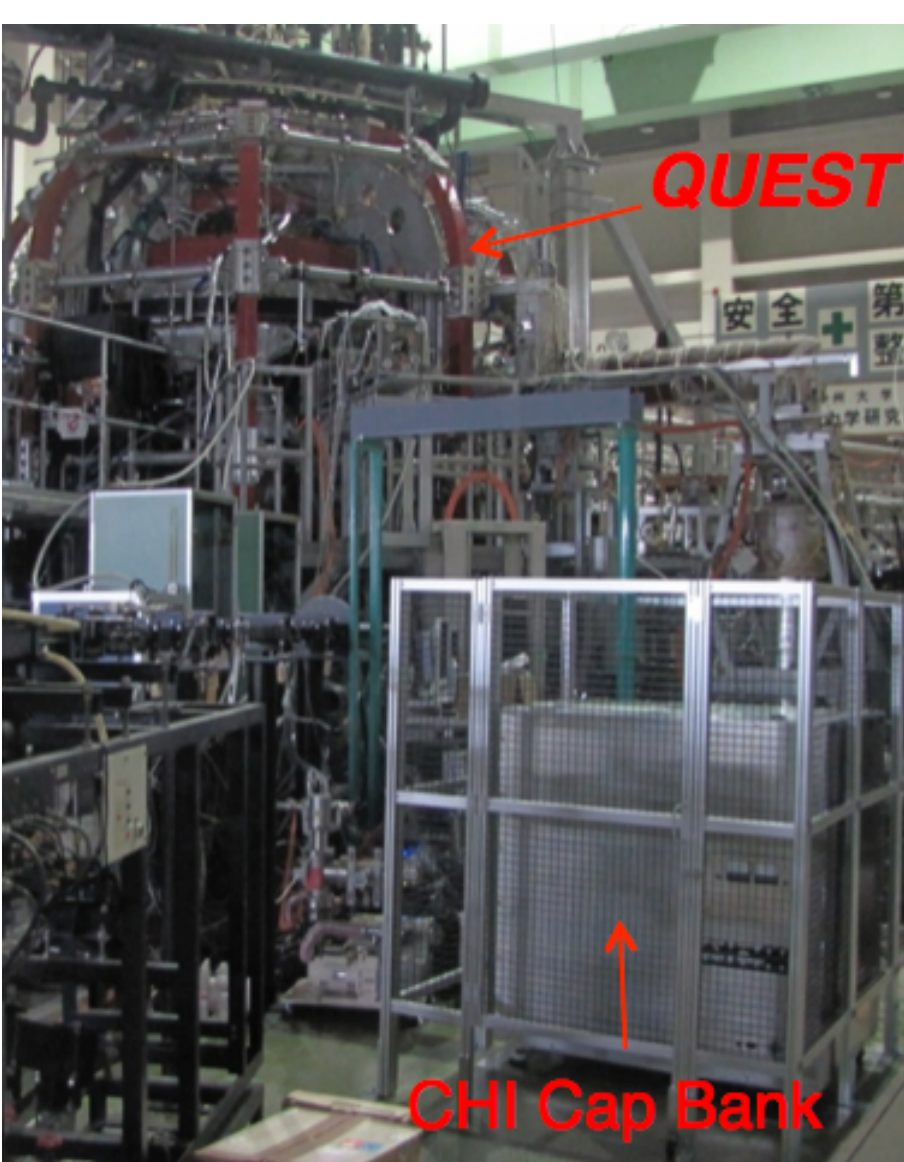
Toroidal electrode on top of blanket structure, analogous to CHI ring electrode previously used on DIII-D



R. Raman, T. Brown, L.A. El-Guebaly, et al.,  
Fusion Science & Technology (2015)



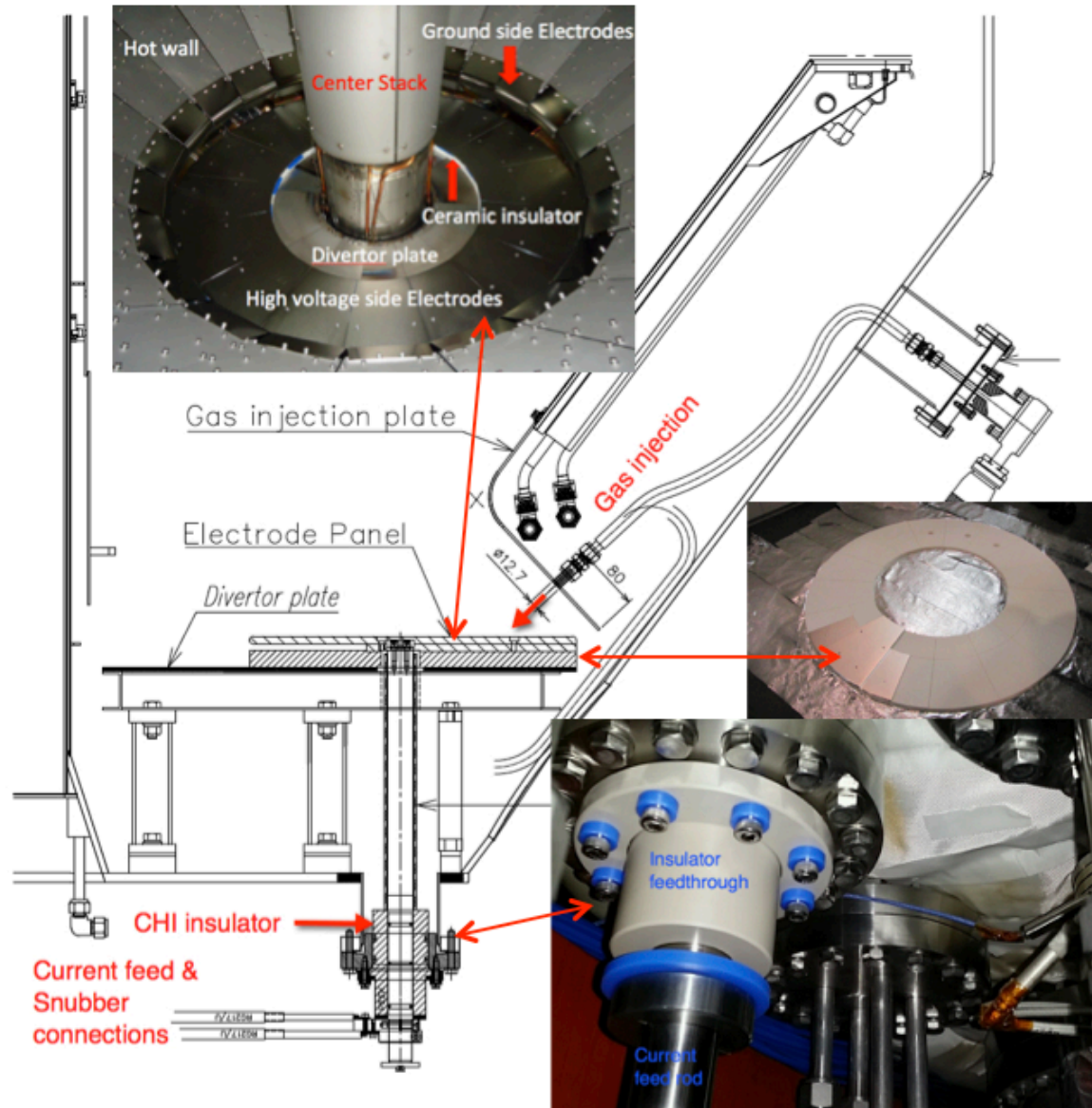
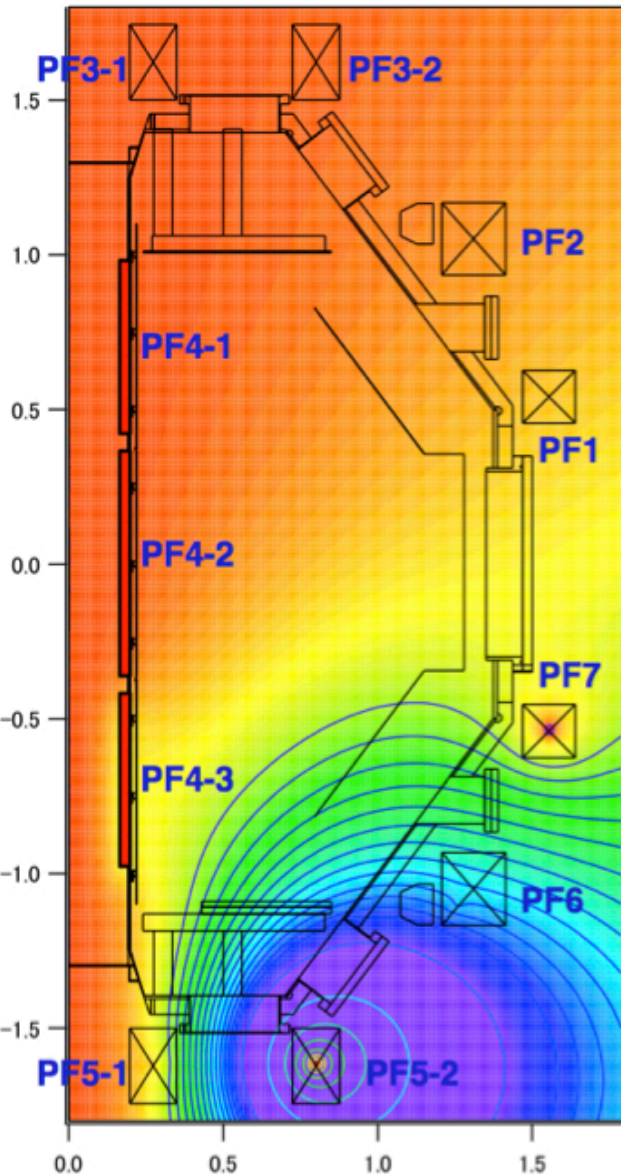
# CHI Research on QUEST in Support of NSTX-U and ST-FNSF



- Test ECH heating of a CHI Target
  - QUEST is equipped with ECH
- Test CHI start-up using metal electrodes
  - Clean metal electrodes should reduce low-Z impurity influx
- Test CHI start-up in an alternate electrode configuration that may be more suitable for a ST-FNSF installation
  - CHI insulator is not part of the vacuum vessel

Collaboration with Kyushu University:  
K. Kuroda, K. Hanada, M. Hasegawa, T. Onchi, et al.,

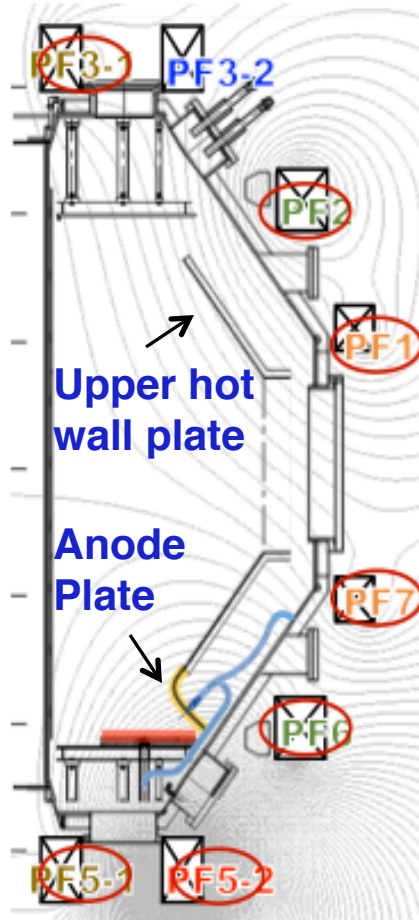
# CHI Configuration on QUEST is Developing ST-FNSF Relevant Single Biased Electrode Design



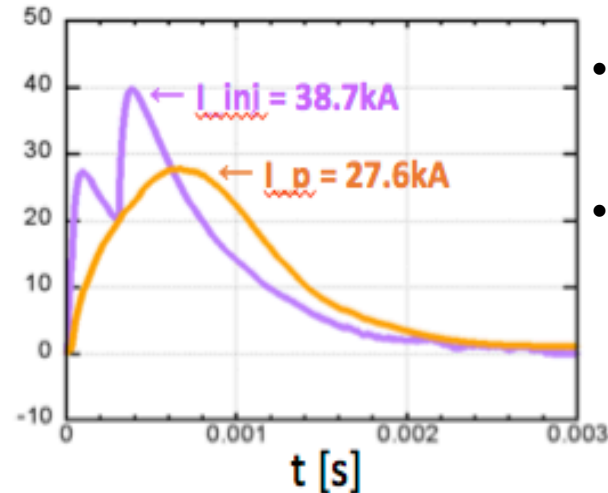


# Reliable Discharge Initiation & Plasma Growth Obtained in the Single Biased Electrode Configuration on QUEST

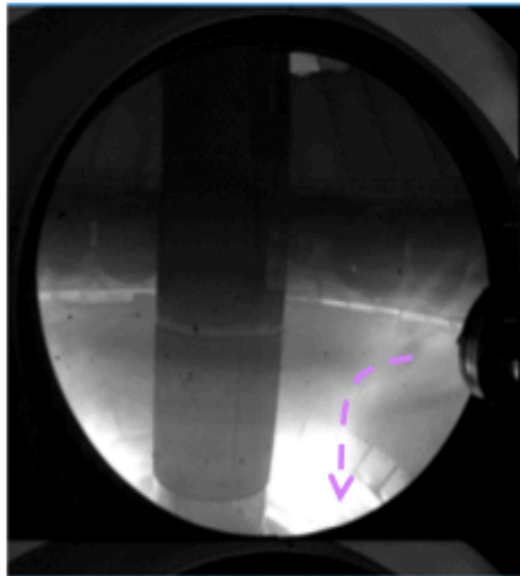
## Injector Flux Configuration on QUEST to reduce flux footprint width



# 035029

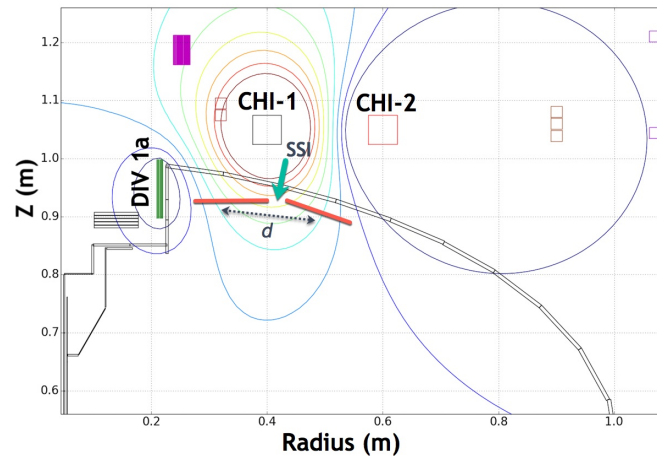
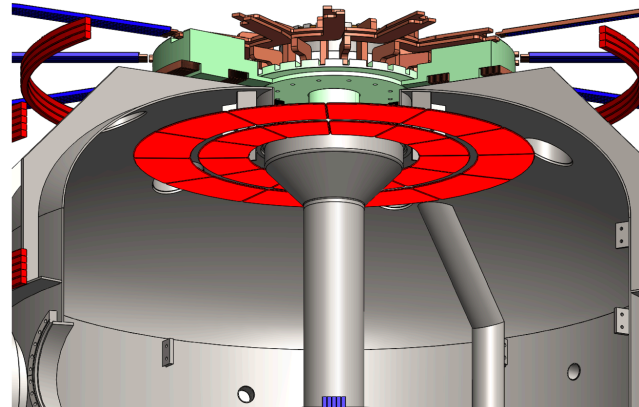
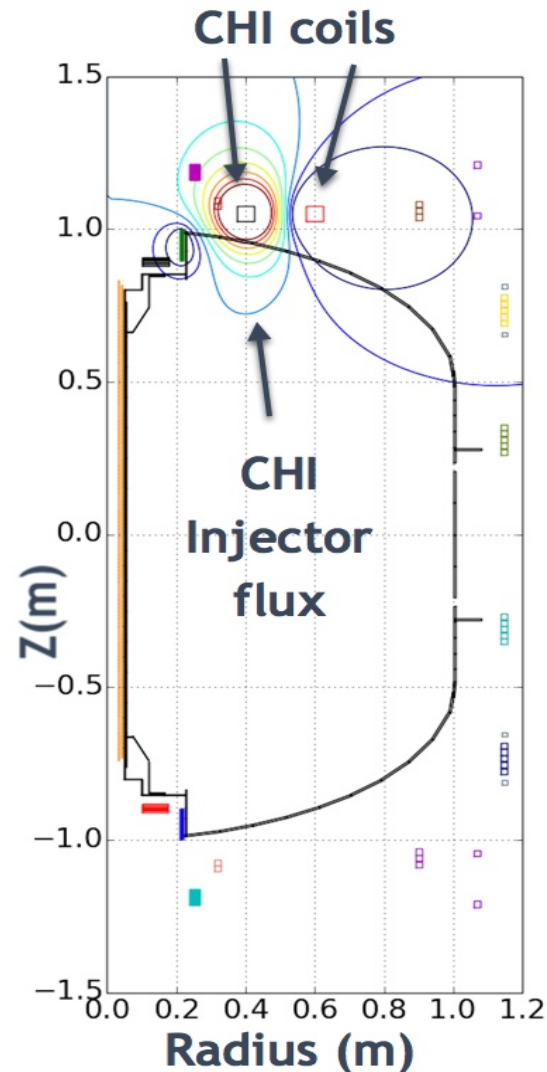


- At low  $I_p$ , current path is to the outer anode plate
- As current increases, and plasma fills the vessel, (not shown here) the discharge appears to contact the upper hot wall plates
- Improved diagnostics, plasma shaping, and capacitor bank programming to be implemented in future to improve discharge performance





# CHI research on Pegasus plans to develop a double biased electrode configuration to better define the current path

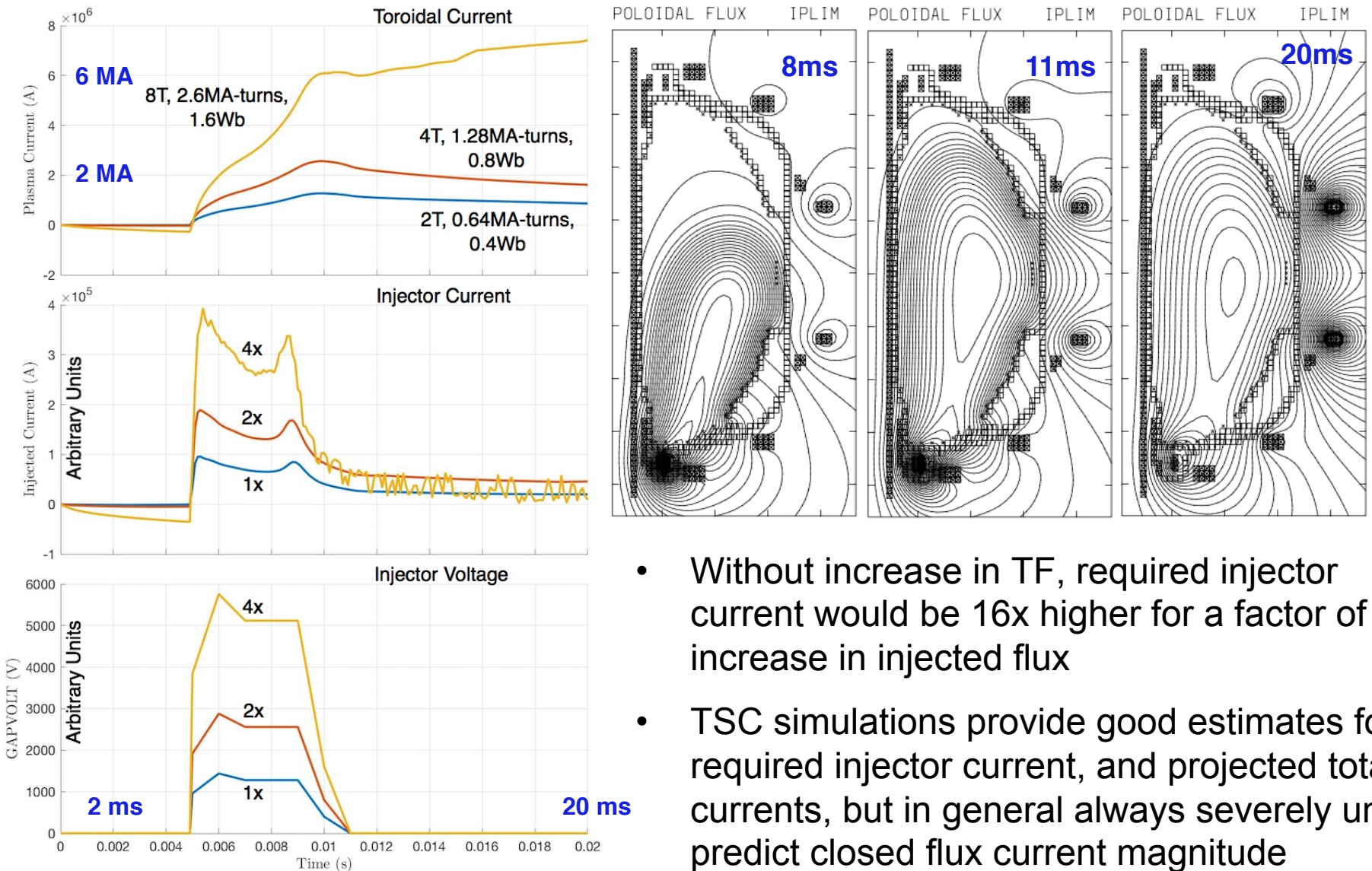


## Goals on Pegasus:

- High  $I_p \sim 300$  kA (@ PF coil limits for  $I_p$ )
- Flux footprint width characterization
- Role of impurities
- Influence of current channel shape on reconnection
- Dynamo current drive enhancement
- ECH heating

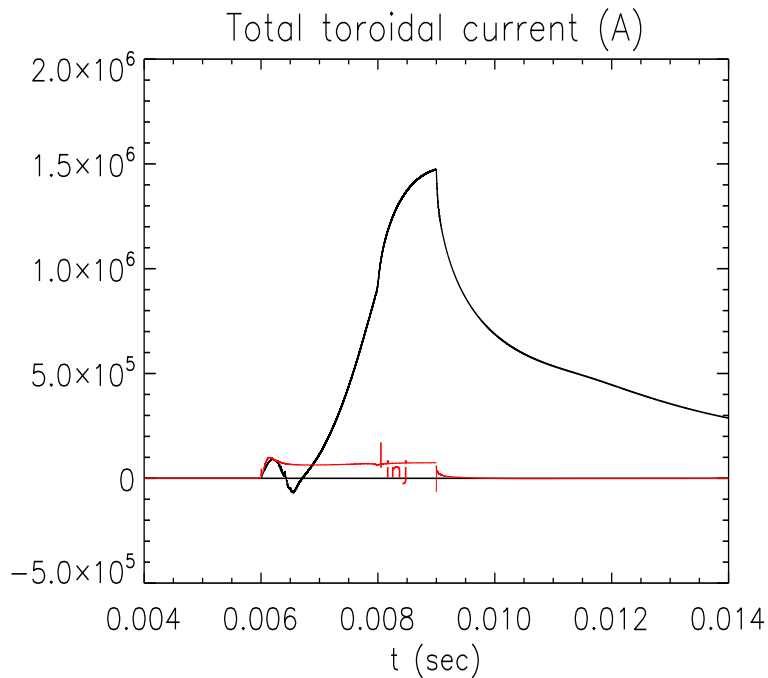
Collaboration with Univ. of Wisconsin:  
J. Reusch, R. Fonck, M. Bongard

# TSC Simulations in NSTX-U Geometry Show Toroidal Current Continuing to Increase with Injected Flux

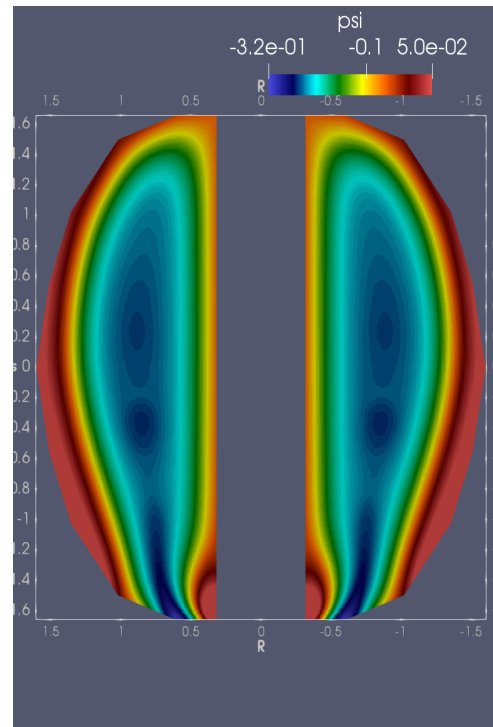


- Without increase in TF, required injector current would be 16x higher for a factor of 4 increase in injected flux
- TSC simulations provide good estimates for required injector current, and projected total currents, but in general always severely under predict closed flux current magnitude

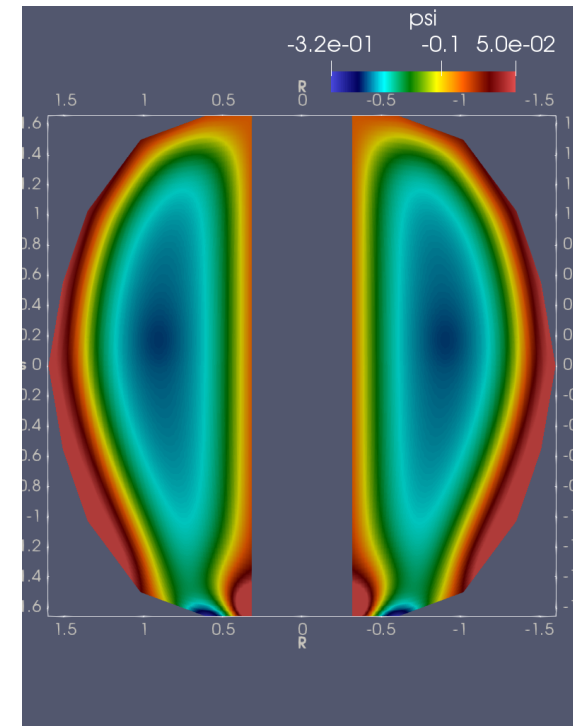
# First High-Flux NIMROD Simulations Show Peak Current Generation to Over 1 MA, Similar to TSC Results



**t = 8 ms**



**t = 9.3 ms**



- Peak toroidal current  $\sim 1.5$  MA
- Simulations are performed at high poloidal flux of 0.32 Wb and toroidal field of about 4 T
- $T_e$  limited to  $\sim 15$  eV, will be increased to 100 eV in future
- Poloidal fluxes during injection 8 ms and decay phase 9.3 ms.
- 0.5 MA closed flux (un-optimized run)

# Representative Parameters for Transient CHI in STs

Parameters	HIT-II	NSTX	QUEST	Pegasus
Major radius [m]	0.3	0.86	0.68	0.45
Minor radius [m]	0.2	0.66	0.4	~0.3
$B_T$ [T]	0.5	0.55	0.25 - 0.5	0.15 - 0.6
Injector flux (mWb)	16	50	28	~60
Projected Start-up current (kA)	100	200	<150	~300

# Transient CHI is being studied to assess its potential for full current generation in a ST/AT – based fusion reactor

- Transient CHI has been very successful on HIT-II and NSTX
- 200 kA current generation on NSTX, and ramp-up to 1 MW with record low flux consumption when coupled to induction demonstrated the high current start-up capability of transient CHI
- Transient CHI does not rely on dynamo mechanism for current generation, so the scaling to larger devices is simpler ( $I_p$  is proportional to Injector Flux)
- QUEST has successfully generated significant toroidal currents in a new single biased electrode geometry
- Design studies are in progress to implement a double biased electrode configuration on PEGASUS
- As a result of rapid improvements in HTSC technology, the design and injector current requirements for full magnitude current generation in STs is investigated using TSC and NIMROD codes
  - TSC simulations show the toroidal current continues to increase with Injector Flux
  - NIMROD simulations show high open to closed flux conversion efficiency and is being used investigate maximum flux injection limits in a given vessel size