Beta-limiting Instabilities and Global Mode Stabilization in NSTX

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Research on the stability of spherical torus plasmas at and above the no-wall beta limit is being addressed on NSTX, which has produced low aspect ratio plasmas, R/a ~ 1.27 at plasma current exceeding 1.4 MA with high energy confinement (Taur/TauE_ITER89P > 2). Toroidal and normalized beta have exceeded 25%, and 4.3, respectively in q ~ 7 plasmas. The beta limit is observed to increase and then saturate with increasing l_i. The stability factor \( \beta_N/\lambda \) has reached 6, limited by sudden beta collapses. Increased pressure peaking leads to a decrease in \( \beta_N \). Ideal stability analysis of equilibria reconstructed with EFIT show that the plasmas are at the no-wall beta limit for the \( n = 1 \) kink / ballooning mode. Low aspect ratio and high edge \( q \) theoretically alter the plasma stability and mode structure compared to standard tokamak configurations. Below the no-wall limit, stability calculations show the perturbed radial field is maximized near the center column and mode stability is not highly affected by a nearby conducting wall due to the short poloidal wavelength in this region. In contrast, as beta reaches and exceeds the no-wall limit, the mode becomes strongly ballooning with long poloidal wavelength at large major radius and is highly wall stabilized. In this way, wall stabilization is more effective at higher beta in low aspect ratio geometry.
The resistive wall mode has been observed in plasmas exceeding the ideal no-wall beta limit and leads to rapid toroidal rotation damping across the plasma core.

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I. INTRODUCTION

Plasma stability at high ratio of plasma energy to magnetic field energy is required for economically attractive operation of a thermonuclear fusion reactor based on magnetic confinement. A figure of merit typically used for tokamak devices is the toroidal beta, \( \beta_t \equiv 2\mu_0 <p> / B_0^2 \), of the system where \(<p>\) is the volume-averaged plasma pressure, and \(B_0\) is the vacuum toroidal field at the plasma geometric center. Development toward greater efficiency in advanced tokamak and spherical torus (ST) reactor designs has defined additional criteria, including a large fraction of bootstrap current to minimize power requirements for auxiliary systems. Plasma current profiles in largely bootstrap driven equilibria are generally broad (have low plasma internal inductance, \( l_i \)). However, tokamak experiments have shown that low \( l_i \) plasmas yield reduced \( \beta_t \) limits caused by the destabilization of magnetohydrodynamic (MHD) instabilities. This contradiction has motivated both theoretical and experimental investigation of the stabilization of low \( l_i \) plasmas. Advanced tokamak plasmas in DIII-D have been stabilized utilizing conducting structure (wall stabilization) and feedback systems at values of \( \beta_t \) significantly above the level possible without stabilizing systems. In contrast, stabilization of the spherical torus using similar tools is not yet established. While the START\(^8\) spherical torus was successful in reaching high \( \beta_t \) at plasma current, \( I_p \), up to 0.3 MA, determination of beta-limiting instabilities and the characteristics of these modes in high current (\( I_p > 1 \) MA) ST plasmas remains to be investigated. Dependence of stability limits on equilibrium parameters for low aspect ratio plasmas has been examined theoretically. Details of the instabilities and their stabilization such as mode structure and related coupling to conducting walls can be significantly different in an ST compared to the advanced tokamak, due to the low aspect ratio and relatively high edge safety factor.

Research in the National Spherical Torus Experiment (NSTX) has been conducted to establish the stable high \( \beta_t \) operating space of an \( I_p > 1 \) MA device, to identify and study the instabilities that limit \( \beta_t \), and to initiate wall-stabilized plasma experiments. The device has a
major radius, $R_0 = 0.86$ m, and a midplane half-width of 0.7 m. The plasma current has exceeded 1.4 MA, and the on-axis vacuum toroidal field, $B_0$, is typically produced in the range 0.3 - 0.45 T. Auxiliary heating and current drive systems include 5 MW of neutral beam injection (NBI) and 6 MW of high-harmonic fast wave (HHFW) power. Plasma elongation, $\kappa$, and triangularity, $\delta$, have reached 2.5 and 0.7, respectively. Operation of limiter, and both double and single-null divertor configurations have been established.$^{13}$ To provide passive stabilization of gross plasma modes, the device has a set of stabilizing conducting copper plates, arranged as four segmented toroidal rings (FIG. 1). The plates are indirectly connected electrically through high resistance supports that mount the plates to the vacuum vessel. For diagnosis of MHD instabilities, the machine has both toroidal and poloidal arrays of magnetic pickup coils, horizontal and vertical fans of ultra soft X-ray detectors, and a set of six locked mode detectors that surround the device at the midplane. Toroidal rotation profiles are measured with 20 ms time resolution by a charge exchange recombination spectroscopy diagnostic.

Computed ideal MHD stability limits determined during the conceptual design of NSTX ranged from $\beta_t \sim 25\%$ without the aid of a conducting wall (no-wall $\beta_t$ limit), to $\beta_t$ exceeding $40\%$ in wall stabilized configurations with optimized equilibrium profiles.$^{14}$ Recent experiments in the device have produced plasmas with $\beta_t$ values reaching the no-wall limit as shown in FIG. 2 where $\beta_t$ at maximum plasma stored energy as determined by NSTX EFIT reconstructions using external magnetics is plotted against the Troyon scaling parameter, $I_p/aB_0$, where $a$ is the plasma minor radius. The instabilities that set the present $\beta_t$ limit and the behavior of this limit as a function of equilibrium profiles are described in Section II. Stabilization of low toroidal mode number kink/ballooning instabilities are theoretically investigated in Section III. Here, we find that relative to the advanced tokamak, mode coupling to conducting structure is relatively weak until the instability becomes strongly ballooning. Section IV describes the initial experimental investigation of global mode coupling to passive conducting structure in the spherical torus, and the identification of the resistive wall mode in the device. A summary and discussion of accessing $\beta_N$ beyond the no-wall ideal limit based on the present results is given in
II. BETA LIMITING INSTABILITIES AND OPERATING SPACE

Several plasma instabilities identified in tokamak experiments have now been observed in NSTX. These results have enabled initial studies of the physical similarities and differences of these modes in ST magnetic field geometry. In this paper, two classes of beta-limiting modes in NSTX are studied - ideal low-$n$ kink/ballooning modes and resistive wall modes. These instabilities lead to relatively fast and large reductions in plasma stored energy at large normalized beta, $\beta_n \equiv 10^8 \langle \beta_t \rangle a B_0 / I_p$, but rarely lead to a full current quench. Other beta limiting instabilities include neoclassical tearing modes (NTMs) \cite{15}, current-driven kinks, \cite{16,17}, and locked modes. NTMs lead to beta saturation, rather than fast beta collapses. Current-driven kinks have been studied in specific low edge safety factor, $q_a$, experiments and can typically be avoided in standard machine operation. Locked modes can be beta-limiting, but are typically eliminated through alteration of the plasma startup phase or gas puffing. Sawteeth with small inversion radii created by slowed minor radial growth during startup are observed and are benign except at sufficiently high poloidal beta when they can trigger NTMs. In general, however, operation with EFIT reconstructed central safety factor greater than unity is required to avoid strong toroidal mode number, $n = 1$ mode activity that typically precedes beta collapse. Compressional Alfvén eigenmodes have also been identified but are not observed to be beta-limiting.\cite{18}

Elements of establishing the fundamental plasma operating space in NSTX including density limits,\cite{16} flux consumption,\cite{19} and MHD equilibrium parameters and configurations\cite{13} have been reported. The present aim is to study instabilities limit $\beta_t$ in NSTX. Once determined, plasma stability can be approached in two ways, (i) determine how beta limits vary with equilibrium profiles and boundary shape so that optimal parameters can be chosen to avoid instability, and (ii) examine how systems can be effectively applied to stabilize modes if instability cannot be avoided. The latter approach is important since in an actual experiment, optimizations are normally limited by practical considerations. Also, advanced tokamak research
has shown that significant increases in $\beta_t$ can be realized for global MHD instabilities by conducting wall stabilization and active feedback once the no-wall $\beta_t$ limit has been violated.\textsuperscript{20,21} Recently, stabilization of NTMs has also been demonstrated,\textsuperscript{22} with some experiments reaching maximum $\beta_t$ after mode suppression.\textsuperscript{23}

Experimentally, the maximum $\beta_N$ increases with increasing current profile peaking in NSTX until $l_i$ reaches 0.7, while at higher $l_i$, the maximum $\beta_N$ saturates with increasing $l_i$ (FIG. 3). The increase of $\beta_N$ with $l_i$ is well-known in advanced tokamak research and correlates with maintaining ideal MHD stability.\textsuperscript{2,3} In DIII-D (Ref. 2), a reduction of $\beta_N$ with increasing $l_i$ at high values of $l_i$ was reported due to the onset of internal instabilities. However, using specially tailored current profiles through negative plasma current ramping, this reduction can be avoided. Instead, a saturation of $\beta_N$ at higher $l_i < 1.3$ is shown in FIG. 3. Another significant difference in NSTX is that a substantial portion of the present database has exceeded the DIII-D $\beta_N$ limit of $4l_i$ with plasmas reaching $6l_i$. Fast beta collapses are observed at all values of $l_i$. Beta saturation coincident with NTM activity typically occurs in high current plasmas with poloidal beta greater than 0.4. A clear reduction of the maximum $\beta_N$ with increasing pressure profile peaking, $F_{p\_mag} \equiv p_{mag}(0) / \langle p_{mag} \rangle$, where $p_{mag}$ is the EFIT reconstructed (using external magnetics alone) total plasma pressure, is also observed (FIG. 4). The significant quantitative decrease of $\beta_N$ with increasing $F_{p\_mag}$ illustrates the importance of reduced pressure peaking in attaining maximum $\beta_N$ in NSTX. The figure illustrates that by increasing $l_i$ at fixed $F_{p\_mag}$, $\beta_N$ can be increased, but even at increased $l_i$, a reduction in $\beta_N$ with increasing $F_{p\_mag}$ is evident. Dependence of the experimental beta limit on plasma boundary shape is presently under investigation.\textsuperscript{24}

Agreement between the experimentally observed $\beta_N$ limit due to fast beta collapses and the theoretically computed ideal MHD stability to low toroidal mode number kink/ballooning modes can be tested using the time evolution of equilibrium reconstructions. Ideal MHD stability analysis of NSTX EFIT reconstructions using external magnetic measurements qualitatively reproduce the experimental behavior of the $\beta_N$ limit shown in Section II. However, to obtain quantitative agreement, equilibrium reconstructions must be refined by also including at least
partial kinetic pressure profile information and diamagnetic loop measurement to allow more accurate determination of the pressure peaking factor, $F_p$ and plasma stored energy, $W_{tot}$. It is found that $F_p$ is typically 50% larger than $F_{p\text{ mag}}$, and $W_{tot}$ typically increases by about 10% in partial kinetic versus magnetics-only reconstructions. For example, the largest $\beta_t$ shown in FIG. 2 is 24.8%, while partial kinetic reconstruction of the same discharge yields a maximum $\beta_N = 26.9\%$. The plasmas are strongly paramagnetic, and remain so at maximum $\beta_t$ with a toroidal field increase of 41% at the magnetic axis. Regardless of this increase in the local magnetic field, the local $\beta$ at the magnetic axis is 48%. As in magnetics-only fits, a single set of EFIT constraints has been determined for partial kinetic reconstructions to model all plasmas. Adhering to this set without varying constraints for specific equilibria allows a quantitative stability evaluation of the time evolution of the plasma equilibria in a single discharge, as well as a direct comparison of the stability of plasmas with significantly different pressure peaking factors and beta limits. Such a comparison is shown in FIG. 5, in which time-evolved ideal, no-wall MHD stability is computed using the DCON$^{25}$ code for two plasmas exhibiting fast beta collapses. Stability calculations begin at $t = 0.15s$, and continue with increasing time resolution (down to 2 ms) as the fast beta collapse time is reached. The pressure peaking factor evolves slowly in both discharges, with $F_p = 3.7$ in the discharge shown in FIG. 5(a) at the time of the beta collapse, and $F_p = 2.9$ in the discharge shown in FIG. 5(b) at the analogous time. In the plasma with larger $F_p$, the experimental $\beta_N$ limit is 2.6, while the computed $n = 1$ ideal kink/ballooning mode becomes unstable at $\beta_N = 2.4$. In the plasma with smaller $F_p$, the experimental $\beta_N$ limit is 4.2 while the computed $n = 1$ ideal kink/ballooning mode becomes unstable at $\beta_N = 4.1$. In both cases, high-$n$ ballooning modes become unstable shortly before the $n = 1$ kink. Stability to the Mercier criterion is violated either shortly before or after the $n = 1$ mode becomes unstable.

**III. KINK/BALLOONING MODE STABILIZATION IN ST GEOMETRY**

Stabilization of global kink/ballooning instabilities in tokamaks relies on the presence of
a conducting wall to either stabilize rapidly rotating plasma modes (mode frequency, $\Omega_m \gg 1/\tau_w$) where $\tau_w$ is the resistive decay time of the wall, or to slow the growth of slowly rotating or stationary modes, $\Omega_m \sim 1/\tau_w$, such as the resistive wall mode (RWM) in plasmas rotating below the RWM critical rotation frequency, $\Omega_c$. In order for either scenario to succeed, the mode structure must allow coupling of the perturbed field to the conducting wall. However, ST magnetic field geometry yields mode structures that are significantly different than advanced tokamak counterparts and at similar $\beta_N$, lead to relatively weak wall coupling. This is illustrated in FIG. 6 that compares the theoretically computed poloidal variation of the normal field perturbation, $\delta B_r$, at the plasma edge between NSTX and DIII-D plasmas of similar $\beta_N \sim 2.3$. The normalized equal-arc length poloidal angle, $\theta/2\pi$ equals 0 and 1 at the outboard midplane, $R_0 + a$, where $R_0$ is the major radius of the device, and 0.5 at the inboard midplane, $R_0 - a$. The mode in the NSTX case lacks coupling to outboard conducting structure due to the near zero amplitude in this region. Also, the short poloidal wavelength of the mode on the inboard side causes a rapid amplitude reduction of the perturbed field away from the plasma surface. In contrast, the mode in DIII-D has maximum amplitude and relatively long poloidal wavelength on the outboard side. These characteristics lead to stronger coupling of the DIII-D mode to outboard conducting structure. In order for the NSTX case to couple well, the underlying equilibrium must have sufficient pressure drive to produce a mode that is ballooning. The short connection length in ST geometry will insure that the mode will have long poloidal wavelength on the outboard side.

The lack of wall stabilization due to weak mode coupling to the wall in the low $\beta_N$ ST plasma can be shown by comparing no-wall to with-wall ideal MHD stability calculations of the potential energy functional, $\delta W$, computed by DCON for the NSTX plasma used in the previous comparison. The variation of stability with $\beta_N$ is examined by scaling the pressure profile self-similarly from the original equilibrium. The lower pressure peaking, $F_{p,mag} = 2.4$ was used for this illustration as it leads to a higher no-wall $\beta_N$ limit and a wider gap in $\beta_N$ between the no-wall and with-wall $\beta_N$ limits. The results are shown in FIG. 7, the solid and dashed curves representing the with-wall and no-wall configurations, respectively. These equilibria generally
require finite edge current density to allow reliable reconstruction of the entire discharge. The edge current can drive localized, or peeling modes that are well-known to appear at $n^*q_a$ slightly below integer values. The $\delta W$ is therefore computed at approximate minimum and maximum values by varying $q_a$ and both solutions are shown. The localized / peeling mode is typically unstable down to zero $\beta_N$, however this mode is not observed to be disruptive in NSTX. The no-wall limit, as compared to the experimental onset of fast beta collapse in FIG. 5 is therefore defined as the $\beta_N$ value at which the maximum computed value of $\delta W$ becomes negative. Thepoloidal variation of $\delta B_r$ for the localized / peeling mode at $\beta_N$ below the no-wall limit is similar to that shown for the NSTX case in FIG. 6, and as expected, the conducting wall has no effect on the stability of this mode until the no-wall limit is reached due to the lack of mode coupling to the wall. However, as $\beta_N$ increases past the no-wall limit, the mode structure becomes more ballooning and couples to the conducting plates, allowing the mode to be wall stabilized. In this way, wall stabilization becomes more effective as $\beta_N$ is increased. The maximum value of $\delta W$ is affected by the conducting wall at lower $\beta_N \sim 3.5$, and the wall allows an increase of the stable operating $\beta_N$ from 5.5 to 6.5 until the with-wall limit is reached, set by internal mode instability. The range of wall stabilized $\beta_N$ is dependent upon $l_i$ and $F_p$, however this range increases in size at higher $\beta_N$ in the ST since the increased pressure drive provides the ballooning character of the mode that leads to greater wall coupling.

One could imagine that stabilization of the short poloidal wavelength mode might be possible using close conducting structure at $R_0 - a$. To check this, a conformal wall is considered in the calculation of $\delta W$. However, a conformal wall with a 1 cm gap to the plasma surface is required stabilize the mode at all values of $\beta_N$ (FIG. 8). Since relatively high resistance plasma facing components of greater than 1 cm thickness are typically used in actual devices, inner wall stabilization is impractical in the ST.
IV. MODE COUPLING TO CONDUCTING WALL AND RESISTIVE WALL MODES

The relatively weak mode coupling to conducting structure in the ST expected from theory has guided experiments in NSTX to investigate mode coupling and generation of the resistive wall mode. Inboard limited plasmas were created that minimized the gap between the plasma boundary and the primary stabilizing plates in the device (the plates closest to the midplane). Since the present control system in NSTX allows steady plasma elongation of about 2, the minimal plasma / plate gap is approximately 11 cm when the plasma / limiter gap at the midplane is 1 cm. In this configuration, plasmas with sufficient NBI power either developed NTMs leading to beta saturation, or fast beta collapses. A comparison of these two cases are shown in FIG. 9. In the latter case, the resistive wall mode (RWM) was observed on the locked mode detector while the plasma stored energy increased. Characteristics of the RWM observed in these experiments are similar to those found in tokamaks. The mode was observed when the ideal \( n = 1 \) no-wall \( \beta_N \) limit was violated through high power NBI heating (4.6 MW). The mode was not observed in control experiments in which lower NBI power (1.7 MW) was used. Calculation of the stability and eigenmode evolution show that the RWM is observed when the computed eigenfunction couples to the conducting wall. This is shown in FIG. 10, where the evolution of ideal \( n = 1 \) stability is computed for equilibrium reconstructions of the experimental discharge. Before the ideal no-wall limit is violated and the RWM is observed \( (t = 0.18 \text{ s}) \), the eigenfunction has relatively small amplitude on the outboard side, closest to the stabilizing plates. However, as the ideal no-wall limit is violated and the RWM is observed, the eigenfunction balloons and couples to the stabilizing plates. As expected from the analysis given in Section III, the wall stabilized range of \( \beta_N \) is small \( (\Delta \beta_N = 0.2) \) as the plasma rapidly becomes internal mode unstable. The margin in \( \beta_N \) over the no-wall limit, or enhancement factor, \( E_w = \beta_N / \beta_N^{\text{no-wall}} = 1.08 \). The growth rate of the RWM observed determined from the growth of the locked mode detector signal is 5 ms. This agrees well with VALEN code calculation of the growth time of 4.6 ms for the computed \( n = 1 \) mode in the presence of a detailed 3D model of the NSTX stabilizing plates, vacuum vessel, and center stack. Computed image currents are
maximum in the primary passive plates (FIG. 11). Based on this calculation, the RWM persists for 3.5 $\tau_w$ before termination at the beta collapse.

Evidence from additional diagnostics support the identification of the resistive wall mode. In contrast to a rotating plasma mode, the RWM is nearly stationary in the lab frame. RWM growth in the locked mode detector was observed while the plasma was rotating, eliminating the possibility that the mode was a locked tearing mode. No precursors were observed in the magnetic pickup coils before the onset of the RWM. In contrast, clear $n = 2$ and $n = 3$ rotating modes were detected by these coils in the comparison plasma in which beta saturation was observed (FIG. 12). Soft X-ray emission shows a mode structure resembling a global kink in RWM plasmas leading up to the beta collapse. No core or edge islands were clearly observed, and the termination resembled a kinking of the plasma core. In contrast, a radially symmetric reconnection event was observed leading to the termination of the comparison plasma. RWM plasmas also exhibit a unique, rapid rotation decrease across the entire plasma core (FIG. 13a). Rotation damping rates of -300 kHz/s were observed while the RWM was present. The rotation damping occurred in spite of maximum neutral beam momentum input in these plasmas. In contrast, the comparison plasma with an $n = 2$ mode showed a core toroidal rotation that increased monotonically in time (FIG. 13b). The pickup coils showed the $n = 2$ mode with a frequency decreasing from approximately 6 to 3 kHz (FIG. 12). This reduction in frequency was consistent with the observed toroidal rotation damping in the edge region. The observed rotation damping rate was -75 kHz/s, significantly less rapid than that observed during RWM activity. Computation of the radial mode structure showed that the mode amplitude was greatest in the plasma core, where the observed toroidal rotation damping was strongest. This is consistent with RWM theory which predicts that rotation damping should scale as the square of the perturbed field caused by the mode.
V. SUMMARY AND DISCUSSION

Low aspect ratio, spherical torus plasmas with $I_p < 1.4$ MA and reaching the ideal no-wall beta limit have been created ($\beta_i > 25\%$). Experimentally, the $\beta_N$ limit increases, then saturates with increasing $l_i$ (current profile peaking), and decreases with increasing pressure profile peaking. Ideal low-$n$ stability of partial kinetic equilibrium reconstructions quantitatively agrees with the experimental $\beta_N$ threshold for fast beta collapses in the device. Theory predicts generally weak coupling to conducting structure in the range of $\beta_N$ and pressure peaking presently reached in the experiment. Strong coupling, and therefore strong stabilization occurs through ballooning of the mode, producing a mode with long poloidal wavelength on the outboard side of the device. Inner wall stabilization of global modes in spherical torus field geometry is ineffective. Dedicated experiments have produced adequate wall coupling in a fairly narrow region of $\beta_N$ space, and the resistive wall mode has been observed when the ideal no-wall limit was exceeded.

The present experimentation and analysis suggests specific routes to further increase $\beta_N$ and $\beta_i$ in NSTX. Operation with a broad pressure profile will lead to an increase of the no-wall beta limit, allowing stable access to increased $\beta_N$ without wall stabilization. Sufficiently high $l_i \sim 0.7$ will be required to stabilize global modes under these conditions (greater than $l_i \sim 3.5$ envisioned for optimized equilibrium targets). With $\beta_N$ sufficiently large, the increased pressure drive will cause global modes to balloon and create long poloidal wavelength modes on the outboard side of the device. These modes can then be effectively wall stabilized, and $l_i$ can be reduced through RF current drive, or more naturally by the increasing bootstrap current that will occur as $\beta_N$ and $\beta_i$ continue to increase. Alternatively, the plasma could be run at high $l_i$ without the aid of wall stabilization. However, this strategy is expected to yield a lower $\beta_N$ limit and would be prone to internal mode instability unless the central safety factor is maintained above unity.
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Figure Captions

FIG. 1. NSTX device cross-section. The position of the stabilizing plates and locked mode detector are shown.

FIG. 2. Toroidal beta vs. Troyon scaling parameter I/aB₀ for NSTX plasmas at maximum plasma stored energy.

FIG. 3. Maximum normalized beta vs. plasma internal inductance. \( \beta_N / l_i \) has significantly exceeded the well-known DIII-D scaling of 4, reaching a maximum value of 6 at \( l_i \sim 0.7 \).

FIG. 4. Maximum normalized beta vs. pressure peaking factor. \( \beta_N \) decreases with increasing pressure peaking. Plasmas indicated by solid points reach higher \( \beta_N \) at fixed \( F_p \) via current profile tailoring (increased \( l_i \)).

FIG. 5. Time evolution and computed ideal no-wall stability for discharges with different pressure peaking. At the time of the fast beta collapse, \( F_p = 3.7 \) for the discharge in frame (a), and \( F_p = 2.9 \) for the plasma in frame (b). The corresponding experimental \( \beta_N \) limits of 2.7 and 4.2 respectively are in quantitative agreement with the computed \( n = 1 \) ideal no-wall \( \beta_N \) limit for these plasmas. Stability calculations are performed from \( t = 0.15s \) in each discharge up to the time of the beta collapse.

FIG. 6. Comparison of the computed poloidal variation of the \( n = 1 \) radial field perturbation in NSTX and DIII-D plasmas at similar \( \beta_N \). ST field geometry leads to a perturbation with relatively weak wall coupling.

FIG. 7. Effect of stabilizing wall on ST equilibria. The potential energy functional \( \delta W \) vs. \( \beta_N \) is shown for configurations including an approximation of the NSTX conducting wall (solid line) and with no wall (dashed line) for an extrapolation of an NSTX plasma to high \( \beta_N \) with a pressure peaking factor of 2.4. The \( \delta W \) is not significantly different between no-wall and with-wall configurations until the no-wall \( \beta_N \) limit is approached.

FIG. 8. Effect of various conducting walls on modes lacking ballooning structure in the ST. Curves are shown for conformal walls with 1, 2, and 5 cm gap, the NSTX wall, and no wall for comparison.

FIG. 9. Time evolution of plasma current, normalized beta, \( n = 1 \) radial field perturbation from the plasma, and pressure peaking factor for a plasma exhibiting a resistive wall mode leading to a fast beta collapse, and a comparable plasma without the RWM leading to a saturation in beta. The latter case has lower pressure peaking.

FIG. 10. Time evolution of computed \( \delta W \) and poloidal variation of \( \delta B \), for \( n = 1 \) instability in a plasma developing a RWM. The computation is performed including an
approximation of the NSTX wall (solid line) and with no wall (dashed line). The $\delta B_r$ is shown at $t = 0.18s$ (weak, but finite perturbation on the outboard side) and $t = 0.192s$ (strong perturbation on the outboard side).

FIG. 11. VALEN calculation of image currents generated in NSTX conducting structure. Thicker arrows indicate regions of larger current.

FIG. 12. Mode frequency and toroidal mode number from toroidal pickup coil array for plasma exhibiting the RWM (frame (a)) compared to a plasma with rotating $n = 2$ and $n = 3$ modes (frame (b)). The RWM plasma shows no strong modes up to the fast beta collapse.

FIG. 13. Time evolution of toroidal rotation profiles in plasma exhibiting a RWM (frame (a)) compared to a plasma with an $n = 2$ rotating mode (frame (b)).

FIG. 14. Routes to high $\beta_N$ operation in NSTX suggested by analysis of conducting wall mode stabilization in ST magnetic geometry.
FIG. 1

Locked mode detector

Ceramic Insulator
Carbon Tiles

Passive Stabilizer Plates
Inner TF Center Stack Inner PFs & OH

Outer TF Outer PFs

High Harmonic Fastwave Coupler

2 m
FIG. 2

![Graph showing the relationship between $\beta_t$ (in %) and $I/aB_0_{\text{mag}}$ (in MA/mT). The graph includes two lines representing $\beta_N = 4$ and $\beta_N = 5$. The distribution of data points indicates a trend consistent with these lines.]
\[ F_p = \frac{p(0)}{DIII-D \text{ scaling}} \]

\[ \beta_N = 4 \]

\[ \beta_N = 6 l_i \]

FIG 3.

FIG 4.
FIG 5.

High-n ballooning
Mercier
n = 1 kink

(a) (b)
FIG 6.

\[ \delta B_r \]

\[ \theta / 2\pi \]

104403 \[ \beta_N = 2.4 \]

DIII-D 92544 \[ \beta_N = 2.2 \]
FIG 7.

Wall stabilized

$\delta W$ (arb)

$kink$

Localized / "peeling" mode

104403 extrapolation, $F_p \sim 2.4$

No wall (dashed)
NSTX wall (solid)

No-wall limit
With-wall limit
FIG 9.

The graph shows the time evolution of various plasma parameters during a 4.6 MW NBI event. The parameters include:

- $I_p$ (MA): Plasma current
- $\beta_N$: Beta parameter
- $\Delta B_r$: Radial magnetic field excursion
- $F_p$: A parameter related to the plasma edge

Key observations include:

- The $I_p$ curve peaks just before the $\beta_N$ and $\Delta B_r$ curves show indications of a disruption.
- The $3.5 \times \tau_{wall}$ mark is significant, indicating a time at which the wall effect becomes dominant.
- The yellow highlighted area suggests a critical time frame, possibly indicating the onset of a serious event.
FIG 10.

No-wall limit

With-wall limit

\[ \delta W \, (arb) \]

\[ \beta_N = 2.25 \, t = 0.18s \]

\[ \beta_N = 2.80 \, t = 0.192s \]

NSTX wall (solid)

no wall (dashed)

106165 time evolution

$\theta / 2\pi$

$\beta_N$

No-wall limit  With-wall limit
FIG 12.
FIG 13.

\( \frac{\Delta f}{\Delta t} = -300 \text{ kHz / s} \) (n = 2 mode)

\( \frac{\Delta f}{\Delta t} = -75 \text{ kHz / s} \)
$\beta_N = 6 I_i$

Low $\beta_N$ kink (no wall coupling)

Wall stabilized

n = 1 internal mode (no wall coupling)